CITY OF GREENVILLE

FORK SWAMP WATERSHED MASTER PLAN

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Prepared for

City of Greenville 1500 Beatty Street Greenville, NC 27834

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EXECUTIVE SUMMARY

The City of Greenville retained WK Dickson to complete a Master Plan for the Fork Swamp watershed. The goals of this master plan include: (1) evaluate the existing flooding, water quality and erosion problems, (2) recommend and prioritize capital improvements to control existing flooding by reducing the frequency and severity of flooding for property owners, and (3) identify stream stabilization projects to reduce the risk of property loss along streams and reduce sediment loads as a result of erosion. To assist in achieving the goals listed above, WK Dickson completed a stormwater drainage infrastructure inventory for drainage structures and features within the Fork Swamp watershed. Over 2,350 drainage structures and approximately 40 miles of drainage pipes was located and incorporated into a GIS database as part of this effort.

The project included a broad range of stakeholders to collect as much data, information, and tacit knowledge of the watershed as feasible. The general public was solicited through questionnaires mailed to all property owners in the watershed and through an open house public meeting where residents and business owners were encouraged to provide feedback on stormwater issues in the watershed. Information collected from the questionnaires and public meeting can be found in Section 2.1 and Appendix D. City staff served as a critical stakeholder by providing valuable information regarding historical flooding and erosion problems in the watershed as well as providing feedback on potential capital improvements and their prioritization.

The project watershed is approximately ten (10) square miles and is located in the south central portion of Greenville. Approximately 60% of the watershed is contained in the City limits, and it is 75% developed as predominantly residential land use. WK Dickson conducted an Existing Conditions Analysis in order to evaluate the existing hydrologic and hydraulic characteristics of the Fork Swamp watershed. Noted in this report as the Primary System are the following:

- Fork Swamp Main Branch;
- Unnamed Tributary 1 to Fork Swamp (referred to as FSUT1);
- Unnamed Tributary 2 to Fork Swamp Reach 1(referred to as FSUT2R1);
- Unnamed Tributary 2 to Fork Swamp Reach 2(referred to as FSUT2R2); and
- Unnamed Tributary 3 to Fork Swamp (referred to as FSUT3).

These Primary Systems were hydraulically studied in detail and were selected based on historical flooding of residential areas and roadways. Furthermore, high storm flows have eroded channel banks over time causing impacts to private yards, fences, and other property enhancements. In addition to the Primary Systems, select conveyance systems (referred to as secondary systems) in the Fork Swamp watershed were analyzed to determine if they meet the desired City design requirements outlined in Section 1.2. These secondary systems were identified based on feedback from City residents and staff.

As a result of the Existing Conditions Analysis, multiple capital improvement and maintenance projects were identified to reduce the severity and frequency of flooding, stabilize stream banks, and improve water quality through stormwater treatment practices. Additionally, the identified projects meet the City's design requirements outlined in Section 1.2 for future conditions.

The proposed capital projects are as follows with the locations of each project shown on Figure ES-1.

Flood Control Projects

Fork Swamp Main Branch Primary System

<u>East Baywood Lane</u> – The existing twin 72" corrugated metal pipes (CMPs) at this crossing are currently providing a 2-year level of service. The water surface elevations (WSELs) at East Baywood Lane are controlled by the backwater from the downstream railroad crossing. With the proposed downstream improvements, the resultant 25-year WSEL is reduced by over 2 feet. However, East Baywood Lane still does not meet the required 25-year level of service and will operate just below a 10-year level of service. Increasing the capacity at the crossing does not impact the WSEL since the culvert is in outlet control. Furthermore, there is no room available to incorporate floodplain benching immediately downstream of the crossing to try to lower the tailwater. Therefore, no capital improvements are proposed at this location. Reductions in flooding in the vicinity of East Baywood Lane will occur as a result of the railroad crossing and Evans Street projects described below.

Railroad Crossing - The existing twin 84" CMPs at this crossing are currently operating at a 25year level of service. In order to aid in lowering the tailwater at East Baywood Lane, floodplain benches downstream of the railroad crossing in the left overbank are proposed for approximately 770 linear feet. The floodplain benching will improve the performance of the existing CMPs at the railroad crossing and bring it up to the desired 100-year level of service while also reducing water surface elevations in the Westhaven neighborhood upstream by increasing the cross-sectional area of flow. The proposed improvements would result in up to a 2.3-foot decrease in WSEL for the 25-year event. Lowering the tailwater at the railroad by installing floodplain benching is the only feasible alternative for reducing the water surface elevations in the upstream Westhaven neighborhood. Based on the model results 121 properties are at risk for lowest adjacent grade (LAG) flooding during the 25-year storm upstream of the railroad crossing. The combination of the Evans Street project and the railroad project will remove 15 of these properties from the 25-year floodplain. Approximately 25% of the proposed floodplain bench appears to be located within a Pitt County Drainage District easement based on the Pitt County OPIS website. Coordination with the Drainage District will be required to implement the proposed project. Additionally, the floodplain benching could be

coordinated with the proposed Fork Swamp Greenway referenced in the 2004 Greenway Master Plan. Economy of savings could be provided if both projects are constructed at the same time.

Evans Street - The existing twin 84" CMPs at this crossing are currently providing a 25-year level of service. Since Evans Street is classified as a major thoroughfare, the desired level of service is the 50-year storm. This alternative entails replacing the existing CMPs with twin 7' x 7' RCBCs coupled with floodplain benching downstream of the crossing to lower the tailwater. The floodplain benching is proposed in the left overbank for approximately 1,200 linear feet. The improvements proposed will bring Evans Street up to the desired 50-year level of service. It should be noted that NCDOT has an upcoming widening project planned for Evans Street. In order to implement the culvert improvements with this planned roadway widening project, coordination with NCDOT will be required. Depending upon the timing, another option would be to complete this project in phases. Phase 1 would be the installation of the proposed floodplain benching followed by Phase 2, the culvert upgrades. The proposed improvements would result in up to a 2.9-foot decrease in WSEL for the 25-year event. As noted above, 15 out of the 121 properties are expected to be removed from the 25-year floodplain as a result of implementing the railroad and Evans Street improvements. The majority of the proposed floodplain bench appears to be located within a Pitt County Drainage District easement based on the Pitt County OPIS website. Coordination with the Drainage District will be required to implement the proposed project. Additionally, the floodplain benching could be coordinated with the proposed Fork Swamp Greenway referenced in the 2004 Greenway Master Plan. Economy of savings could be provided if both projects are constructed at the same time.

<u>East Fire Tower Road</u> – The existing bridge at this crossing is in good condition and currently performs at a 25-year level or service. Since East Fire Tower Road is a major thoroughfare, the desired level of service is the 50-year storm. In order to provide a 50-year level of service at this crossing, the recommended alternative is to reduce the tailwater by grading floodplain benches downstream of East Fire Tower Road. This alternative entails proposed floodplain benching in the right overbank for approximately 2,000 linear feet. The proposed improvements will bring East Fire Tower Road up to the desired 50-year level of service and provide a reduction in the severity, frequency, and duration of flooding for several properties along Treetops Circle. The proposed improvements would result in up to a 2.3-foot reduction in WSEL for the 25-year event. Additionally, four (4) out of six (6) properties may expect to be removed from the 25-year floodplain and twelve (12) properties from the 100-year floodplain. The majority of the proposed floodplain bench appears to be located within a Pitt County Drainage District easement based on the Pitt County OPIS website. Coordination with the Drainage District will be required to implement the proposed project. The floodplain benching could be coordinated with the proposed Fork Swamp Greenway referenced in the 2004 Greenway Master Plan. Economy of savings could be provided if both projects are constructed at the same time.

<u>Fork Swamp Main Branch Floodplain Benching</u> – In addition to the improvements proposed at and near the individual road crossings, there is a proposed floodplain bench and stream stabilization project located along the main branch of Fork Swamp downstream of FSUT1 and

FSUT2. Approximately 2,670 linear feet of floodplain benching is proposed in the left and right overbank. The proposed project will reduce tailwater for FSUT1 and FSUT2, provide additional floodplain storage and remove four (4) and one (1) properties from the 25-year and 100-year floodplains, respectively. The majority of the proposed floodplain bench appears to be located within a Pitt County Drainage District easement based on the Pitt County OPIS website. Coordination with the Drainage District will be required to implement the proposed project. The floodplain benching could be coordinated with the proposed Fork Swamp Greenway referenced in the 2004 Greenway Master Plan. Economy of savings could be provided if both projects are constructed at the same time.

The total length of the proposed Fork Swamp Greenway is 3.3 miles. Approximately 1.25 miles of the proposed greenway overlaps with the floodplain benching limits. If possible construction of the benching and greenway should be coordinated.

Fork Swamp UT1 (FSUT1) Primary System

<u>Trafalgar Drive – South</u> – The twin 60" CMPs at this crossing are currently providing a 2-year level of service. In order to meet a 25-year level of service, the twin 60" CMPs will remain in place and an additional 60" floodplain culvert will be required along with a new headwall. The proposed improvements will WSEL for the 25-year storm by up to 0.67 feet upstream of Trafalgar Drive-South and remove one property from the 25-year floodplain.

<u>Trafalgar Drive – North</u> – The 60'' and 66'' CMPs at this crossing are operating at a 2-year level of service. To meet the desired 25-year level of service, it is proposed that the existing CMPs be removed and replaced with twin $8' \times 5'$ RCBCs. The resulting upstream WSEL will be reduced by as much as 0.95 feet in the 25-year if improvements are completed in conjunction with those proposed at Corey Road as described below. This will bring two (2) properties out of the 25-year floodplain and two (2) additional properties out of the 100-year floodplain.

Corey Road – The existing twin 13′ x 4.5′ corrugated metal arch pipes at this crossing are relatively new and meet the desired 25-year level of service. However, the WSEL at the upstream Trafalgar Drive – North is impacted by the tailwater from Corey Road. In order to lower the tailwater, it is proposed that twin 48″ floodplain culverts be installed along with approximately 2,300 linear feet of floodplain benching in the left and right overbanks downstream of Corey Road. The Corey Road improvements should be constructed prior to culvert upgrades at Trafalgar Drive to provide the desired level of service noted above. The proposed improvements would result in up to 2-foot reduction in WSEL for the 25-year event. This will bring one property out of the 25-year floodplain and an additional property out of the 100-year floodplain.

Fork Swamp UT2 Reach 1 (FSUT2R1) Primary System

<u>Old Tar Road</u> – The existing 72" CMP at this crossing is currently operating at a 2-year level of service. In order to meet the desired 50-year level of service, the existing CMP will need to be replaced with twin 7' x 8' RCBCs with 230 linear feet of floodplain benching in the left and right overbanks proposed downstream of Old Tar Road. The NCDOT maintained Old Tar Road is located immediately west of the existing City limits and the City's ETJ. A portion of the proposed floodplain benching along the left bank would be inside the City limits. Based on the location of the road crossing outside the City limits, the Old Tar Road project is not included as a capital project for the City of Greenville.

Fork Swamp UT2 Reach 2 (FSUT2R2) Primary System

<u>West Fire Tower Road</u> – The existing 10′ x 8′ reinforced concrete box culvert (RCBC) at this crossing is in good condition and is currently exceeding a 100-year level of service. Therefore, no capital improvements are proposed for West Fire Tower Road.

Fork Swamp UT3 (FSUT3) Primary System

<u>Coleman Drive</u> – The existing triple 10′ x 4′ RCBCs at this crossing are in good condition and currently meet the desired 25-year level of service. With the downstream improvements recommended along FSUT3, the RCBCs will continue to pass the 25-year storm. Therefore, no capital improvements are proposed at this location.

<u>County Home Road</u> – The twin 48" reinforced concrete pipes (RCPs) at this crossing currently pass a 10-year storm event. Based on its classification as a major thoroughfare, it is required to meet a 50-year level of service. It is proposed that the twin 48" RCPs remain in place and an additional 42" floodplain culvert be installed with approximately 240 linear feet of floodplain benching in the left overbank downstream of Country Home Road. The proposed improvements will bring the crossing up to a 50-year level of service and result in up to a 1.3-foot reduction in WSEL for the 25-year event. This will bring two (2) properties out of the 25-year floodplain and two (2) additional properties out of the 100-year floodplain.

<u>East Fire Tower Road – U/S</u> – The existing twin 54" RCPs at this crossing are currently providing a 2-year level of service. In order to meet the desired 50-year level of service, the twin 54" RCPs under East Fire Tower Road will be replaced with twin 6'x 6' RCBCs. The proposed improvements would result in up to a 1.5-foot reduction in WSEL for the 25-year event and one (1) property being removed from the 25-year floodplain.

<u>Wimbledon Drive</u> – The twin 60" CMPs at this crossing are currently providing a 2-year level of service. In order to meet a 25-year level of service, the twin 60" CMPs will be replaced with twin $10' \times 5'$ RCBCs. Additionally, 245 linear feet of floodplain benching is proposed in the right overbank downstream of Wimbledon Drive. Final limits of the proposed benching may

change to minimize impacts to private property owners. The proposed improvements would result in up to a 1.2-foot reduction in WSEL for the 25-year event and removal of one property from the 25-year floodplain.

<u>Tower Place</u> – The twin 66" CMPs at this crossing are currently operating at a 2-year level of service. In order to meet a 25-year level of service, the twin 66" CMPs will be replaced with twin 10' x 5' RCBCs. The proposed improvements would result in up to a 1.0-foot reduction in WSEL for the 25-year event. This will bring two (2) properties out of the 25-year floodplain and one additional property out of the 100-year floodplain.

<u>Summerhaven Drive</u> – Currently, the twin 66" CMPs at this crossing provides a 2-year level of service. To meet a 25-year level of service, the twin 66" CMPs will be replaced with quad 6' x 6' RCBCs. It is proposed that 115 linear feet of floodplain benching be graded downstream of Summerhaven Drive to help lower the tailwater. The proposed improvements would result in up to a 1.2-foot reduction in WSEL for the 25-year event and seven (7) properties being removed from the 25-year floodplain.

<u>East Fire Tower Road – D/S</u> – The existing twin $10' \times 7'$ corrugated metal ellipse pipes only pass the 2-year storm. To meet a 50-year level of service, it is proposed that the existing culverts be removed and replaced with quad $6' \times 7'$ RCBCs. In addition to the culvert upgrade, a total of 3,240 linear feet of floodplain benching is proposed (990 linear feet upstream of the crossing in the left overbank and 2,250 linear feet downstream of the crossing in the left and right overbanks). The proposed improvements would result in up to 1.9 feet reduction in WSEL for the 25-year event. Additionally, forty-two (42) properties will be removed from the 25- and 100-year floodplain.

The floodplain benching could be coordinated with the proposed Fire Tower to Hub - Connector Greenway referenced in the 2004 Greenway Master Plan. Economy of savings could be provided if both projects are constructed at the same time.

Secondary Systems

<u>Corey Road Closed System</u> – The majority of the system is operating at or above the required 10-year level or service. Therefore, the proposed improvements consist of minimal upgrades including upsizing the downstream discharge pipes along Southlea Drive. The proposed pipe improvements range in size from 24" to 48" RCP. The proposed improvements are expected to decrease WSELs by up to 1.7 feet for the 25-year event.

<u>Trafalgar Drive Closed System</u> – All segments of this system located in the Farrington subdivision are operating above the required 10-year level of service. Therefore, no capital improvements are proposed at this location.

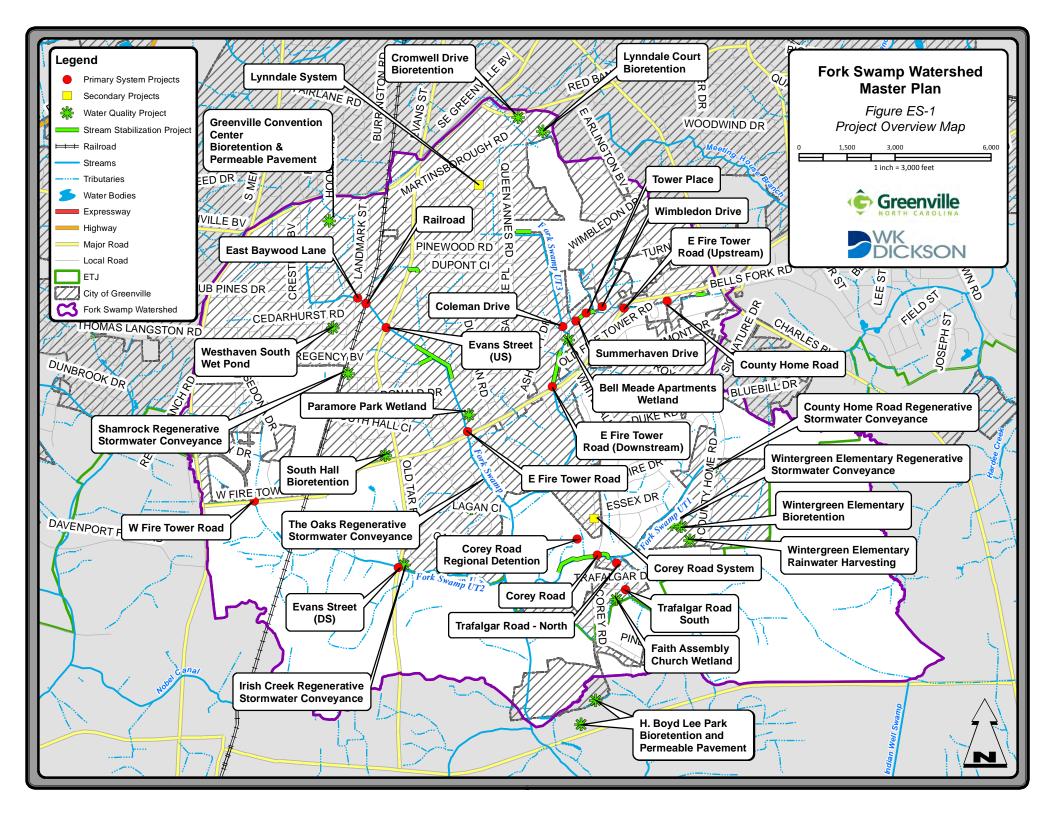
<u>Lynndale System</u> – Seven (7) questionnaires were received from the residents in the Lynndale subdivision reporting yard and street flooding. A study for this area has been completed with

proposed recommendations by River & Associates. The proposed design is included as part of this report. Due to the size of the project, it is recommended that the Lynndale system be completed in three (3) separate phases.

<u>Evans Street Channels</u> – Two (2) channel sections east of Evans Street and south of Pinewood Drive were reported by City staff as being eroded. The channel velocities calculated by the model range between 0.2 and 3.3 feet per second in the 10-year storm event. These channel sections were walked and evaluated by WK Dickson personnel. Based on this evaluation, a stream stabilization project (Project #7) is proposed along the upstream segment.

Regional Detention

A Corey Road facility is proposed in the southern part of the Fork Swamp watershed along FSUT1 adjacent to Corey Road. It is recommended to help offset peak flow increases that will be created as a result of the proposed upstream culvert upgrades. Based on the development of a cursory model, the proposed 20-acre detention pond would lower the flows in the 2-, 10-, 25-, 50-, and 100-year storms by 20 to 25 percent at the confluence of FSUT1 with Fork Swamp. These flow reductions continue through the downstream modeling limits of the Fork Swamp watershed. The regional detention facility will not impact the size of culverts along FSUT1 but will reduce the downstream flows (and therefore the water surface elevations) along the main branch of Fork Swamp. The location of this facility is close to the border of Winterville and outside of the existing City limits, although City residents upstream and downstream of this facility would benefit from the project. The proposed detention facility would be an opportunity to partner with this Winterville and potentially Pitt County. If 25-year detention is required in the areas shown in Section 4.3, then the size of the regional detention area can be substantially reduced to maintain no net increase in the 25-year storm at the study area limits for the future conditions.



Flood Control Prioritization

To appropriately allocate City resources, the flood control projects listed above were prioritized based on the following categories as described in Appendix L:

- Public health and safety
- Severity of street flooding
- Cost effectiveness
- Effect of improvements
- Water quality BMP
- Open channel erosion control
- Implementation constraints
- Grant funding
- Constructability

Scores were assigned to each project for the factors listed above to determine the priority list. In some instances, project prioritization will be impacted by the required sequencing of projects to provide the highest possible flood reduction benefits and to reduce or negate any downstream impacts from the proposed projects. Tables ES-1 and ES-2 show the proposed prioritizations and conceptual cost estimates for the Flood Control Improvements. The City should re-visit the prioritization lists annually to determine if priorities should shift. The prioritization scoring for each project and a description of the aforementioned categories is included in Appendix L. The total cost for all of the recommended primary and secondary system improvements in the Fork Swamp watershed is approximately \$31,730,000.

Table ES-1: Flood Control Project Prioritization – Primary Systems

Prioritization	Project	Cost
1	Railroad Crossing (Fork Swamp) \$1,000,000	
2	Summerhaven Drive (FSUT3)	\$650,000
3	Evans Street (Fork Swamp)	\$1,920,000
4	Trafalgar Drive - South (FSUT1)	\$180,000
5	County Home Road (FSUT3)	\$210,000
6	6 Tower Place (FSUT3) \$640,000	
7	7 East Fire Tower Road (Fork Swamp) \$1,740,000	
8	8 Trafalgar Drive - North (FSUT1) \$440,000	
9	Corey Road (FSUT1)	\$6,870,000
10	Wimbledon Drive (FSUT3)	\$610,000
11	Fork Swamp Main Branch Floodplain Benching	\$5,240,000
12 East Fire Tower Road - Downstream (FSUT3) \$4,000,000		\$4,000,000
13	13 East Fire Tower Road - Upstream (FSUT3) \$680,000	
	Total	\$24,180,000

See Appendix L for prioritization details.

Table ES-2: Flood Control Project Prioritization – Secondary Systems

Prioritization	Project Cost			
1	Lynndale Closed System Phase I	\$1,010,000		
2	Lynndale Closed System Phase II	\$3,420,000		
3	Lynndale Closed System Phase III	\$2,750,000		
4	Corey Road Closed System	\$370,000		
	Total	\$7,550,000		

See Appendix L for prioritization details.

The additional cost to construct the Corey Road Regional Detention Facility would be \$9,500,000 which would include anticipated land acquisition costs.

Stream Stabilization and Water Quality Projects

During the Existing Conditions Analysis, the majority of the streams were quantitatively assessed for stability. Based on this assessment, seven (7) stream stabilization projects were identified as shown on Figure ES-1. Potential components of the stabilization project include, flattening the slope of the channel banks, installing erosion control matting and plantings, rock grade control structures, retaining walls, and rip-rap. The stabilization project will protect residential yards, fences, and structures from further erosion, and substantially decrease the instream sediment loads to downstream receiving waters.

In additions to the stream stability projects, eighteen (18) water quality BMP retrofit projects were recommended. Potential project locations were initially identified using available GIS data by focusing on locations with contributing drainage areas that are highly impervious and preferably on publically-owned land. Impervious areas typically generate the highest concentration of pollutants, so treating the runoff from these areas would provide more pollutant material than treating water that carried fewer pollutants. Publically-owned land is ideal for BMP retrofits to reduce or eliminate potential land acquisition costs. See Section 5.2 for additional evaluation criteria for BMP retrofit sites. Potential locations that were identified using GIS were then presented to the City. Following concurrence with the City, the final list of BMPs were field inspected to determine any project constraints present that may not be discernible from GIS data, such as utility conflicts, limited access to the site, or private property conflicts.

The stream stabilization and water quality projects were prioritized using categories similar to those used to prioritize the flood control projects described above (See Appendix L). Cost effectiveness for the stream stabilization project was calculated based on a cost per linear foot of stabilized stream while for water quality projects, it was calculated based on a cost per impervious acre treated. Tables ES-3 and ES-4 show the prioritization of the stream stabilization and water quality projects along with estimates of their preliminary cost.

Table ES-3: Stream Stabilization Prioritization

Prioritization	Project	Cost
1	Evans Street	\$130,000
2	Live Oak Lane	\$280,000
3	Tower Place	\$140,000
4	Charles Boulevard \$90,000	
5	East Fire Tower Road \$230,000	
6	Queen Annes Road \$220,000	
N/A*	Corey Road* \$590,000	
	Total	\$1,090,000*

^{*}The Corey Road Stream Project is located outside City Limits and therefore was not ranked or included in the total cost. However, improvements will benefit residents in the City limits. See Appendix L for prioritization details.

Table ES-4: Water Quality Project Prioritization

Prioritization	Project	Cost
1	WGP Properties Regenerative Stormwater Conveyance	\$60,000
2	H. Boyd Lee Park Bioretention	\$340,000
3	Wintergreen Elementary Rainwater Harvesting	\$20,000
4	Wintergreen Elementary Bioretention	\$310,000
5	South Hall Bioretention	\$240,000
6	Lynndale Court Bioretention	\$150,000
7	Shamrock Regenerative Stormwater Conveyance	\$130,000
8	Paramore Park Wetland	\$210,000
9	H. Boyd Lee Park Permeable Pavement	\$970,000
10	County Home Road Regenerative Stormwater Conveyance \$490,000	
11	The Oaks Regenerative Stormwater Conveyance \$200,000	
12	Wintergreen Elementary Regenerative Stormwater \$180,000 Conveyance	
13	Cromwell Drive Bioretention	\$350,000
14	Belle Meade Apartments Wetland	\$570,000
15 Faith Assembly Church Pond Retrofit \$270,000		\$270,000
16		
17	Irish Creek Regenerative Stormwater Conveyance	\$250,000
18	Greenville Convention Center Permeable Pavement	\$2,870,000
	Total	\$8,430,000

See Appendix L for prioritization details.

25-Year Detention Analysis

As part of the Fork Swamp Master Plan, an analysis was completed to determine if there are areas within the watershed that should be considered "well documented water quantity problems" requiring detention for the 25-year, 24-hour storm event. As noted in Section 3.1, documented flooding issues are located along Fork Swamp Main Branch, Unnamed Tributary 3, and Unnamed Tributary 1 including the area between Baywood Lane and Treetops Circle along Fork Swamp Main Branch, the area between Corey Road and Trafalgar Drive along Unnamed Tributary 1, and the area between East Fire Tower Road and County Home Road along Unnamed Tributary 3. Large portions of the Fork Swamp watershed are already fully developed, however there are some areas of the watershed where the future conditions 25-year flows could be greater than 10% higher than the current existing flows. These areas are outlined in Section 4.3.

If 25-year detention is required in the proposed areas, the need for culvert improvements will not be eliminated but the recommended culvert sizes could be decreased. Although the cost savings to the City would not be substantial, the severity, frequency, and duration of flooding would be reduced, which would in return provide savings to the property owners.

The Corey Road Regional Detention area is the largest portion of the overall cost for flood control projects in the Fork Swamp watershed (\$9,500,000). As previously noted, this project is proposed to address increases in the 25-year flows as a result of increasing upstream capacity and proposed future development. If the City requires 25-year detention for portions of the watershed as shown in Section 4.3, the size of the Corey Road regional detention area can be reduced, which would substantially lower the cost of the proposed detention area by approximately \$5 million.

INTRODUCTION

1.1 Project Description

The City of Greenville retained WK Dickson to complete a Watershed Master Plan for the Fork Swamp watershed. As shown in Figure 1-1, the Fork Swamp watershed is located in the south central portion of Greenville and generally drains north to south ultimately discharging to the Neuse River. As noted in the Executive Summary, the goals of the Master Plan include: (1) evaluate the existing flooding, water quality and erosion problems, (2) recommend and prioritize capital improvements to control existing flooding by reducing the frequency and severity of flooding for property owners, and (3) identify stream stabilization projects to reduce the risk of property loss along streams and reduce sediment loads as a result of erosion. To assist in achieving the goals listed above, WK Dickson completed a stormwater drainage infrastructure inventory for drainage structures and features within the Fork Swamp watershed.

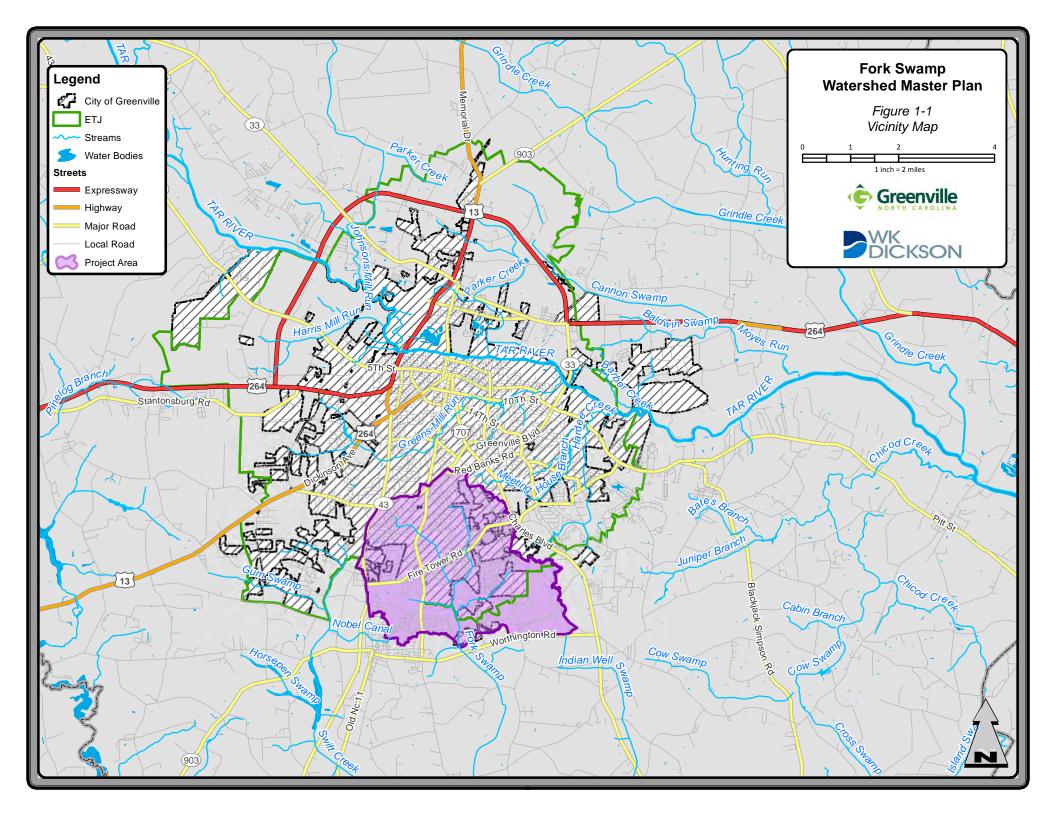
The Master Plan includes an evaluation of the segment of Fork Swamp from East Baywood Lane at the upstream end to approximately 900 feet upstream of the Worthington Road crossing at the existing City limits. The following tributaries were evaluated as part of this Master Plan:

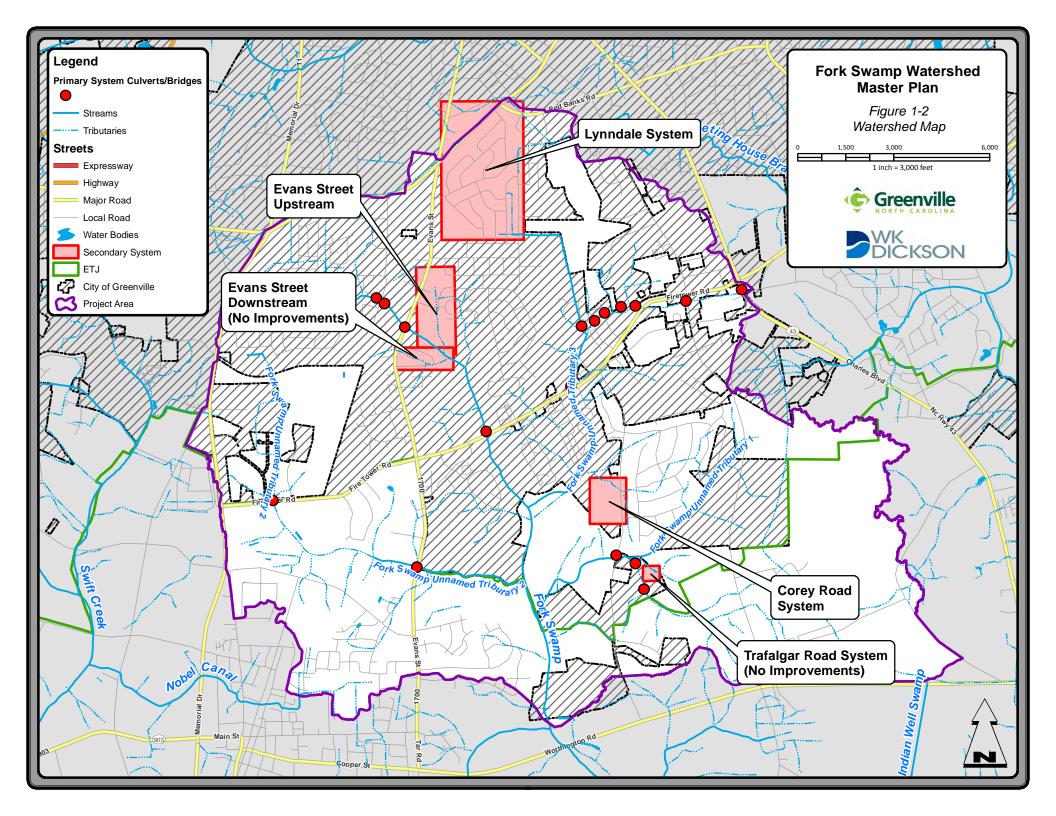
- Fork Swamp UT1 from approximately 250 feet upstream of the Trafalgar Drive South crossing at the upstream end to its confluence with Fork Swamp at the downstream end;
- Fork Swamp UT2R1 from the Old Tar Toad crossing at the upstream end to its confluence with Fork Swamp at the downstream end;
- Fork Swamp UT2R2 from approximately 300 feet downstream of the Regency Boulevard crossing at the upstream end to the West Fire Tower Road crossing at the downstream end; and
- Fork Swamp UT3 from the Queen Annes Road crossing and Charles Boulevard at the upstream end to its confluence with Fork Swamp at the downstream end.

Additionally, four (4) conveyance systems that drain to the primary systems were evaluated. For the purposes of this report, Fork Swamp and its tributaries (FSUT1, FSUT2R1, FSUT2R2, and FSUT3) will be noted as primary systems and the conveyance systems will be noted as secondary systems. A project area map showing the Fork Swamp watershed and the conveyance systems evaluated as part of this Master Plan is included as Figure 1-2. Detailed hydraulic analysis included the following:

- Primary System Fork Swamp
 - o East Baywood Lane Culvert
 - Railroad Crossing Culvert
 - o Evans Street Culvert
 - o East Fire Tower Road Bridge

- Primary System FSUT1
 - o Trafalgar Drive South Culvert
 - o Trafalgar Drive North Culvert
 - o Corey Road Culvert
- Primary System FSUT2R1
 - o Old Tar Road Culvert
- Primary System FSUT2R2
 - o West Fire Tower Road Culvert
- Primary System FSUT3
 - o Coleman Drive Culvert
 - o County Home Culvert
 - o East Fire Tower Road Upstream Culvert
 - o Wimbledon Drive Culvert
 - o Tower Place Culvert
 - o Summerhaven Drive Culvert
 - o East Fire Tower Road Downstream Culvert
- Secondary Systems
 - o Corey Road System
 - o Trafalgar System
 - o Lynndale System
 - o Evans Street Channel System





1.2 Design Standards and Criteria

The following design storms were used to evaluate the performance of the primary and secondary systems in this Master Plan:

- 10-year storm event piped collection systems;
- 25-year storm event minor thoroughfare roadway bridges and culverts;
- 50-year storm event major thoroughfare roadway bridges and culverts;
- 100-year storm event structural flooding of homes; and
- 100-year storm event overtopping of railroad.

Table 1-1 shows the applicable storm for the project areas evaluated as part of this Master Plan. The corresponding rainfall depths for the design storms are included in Appendix A.

Table 1-1: Project Area Design Standards and Criteria

Drainage Type	Design Storm (years)	Project Area	
Piped Collection Systems	10	Corey Road SystemTrafalgar SystemLynndale System	
Minor Thoroughfare Roadway Crossings	25	 East Baywood Lane Culvert (Fork Swamp) East Fire Tower Road Bridge (Fork Swamp) Trafalgar Drive – South Culvert (FSUT1) Trafalgar Drive – North Culvert (FSUT1) Corey Road Culvert (FSUT1) Old Tar Road Culvert (FSUT2R1) Coleman Drive Culvert (FSUT3) Wimbledon Drive Culvert (FSUT3) Tower Place Culvert (FSUT3) Summerhaven Drive Culvert (FSUT3) 	
Major Thoroughfare Roadway Crossings	50	 Evans Street Culvert (Fork Swamp) West Fire Tower Road Culvert(FSUT2R2) County Home Road Culvert (FSUT3) East Fire Tower Road – U/S Culvert (FSUT3) East Fire Tower Road – D/S Culvert (FSUT3) 	
Railroad Crossing	100	Fork Swamp – Culvert	

EXISTING WATERSHED CONDITIONS

2.1 CITIZEN INPUT

The Master Plan included a citizen input component to solicit feedback and information regarding stormwater impacts and future stormwater management in the City. In August of 2014, the City began distribution of questionnaires related to stormwater management property owners in the Fork Swamp watershed. Thirty-six (36) questionnaires were completed and returned to the City for consideration from Fork Swamp watershed property owners. The questionnaire results were georeferenced according to the address of the questionnaire respondent (See Figure 2-1). There was one response that was located outside of the City limits. Seven (7) of the respondents indicated some level of property flooding, with one (1) property owners experiencing living space flooding, (4) four crawl space flooding, and 2 (two) AC/storage at least once per year. Twenty-four (24) respondents identified locations where street flooding occurs while another ten (10) residents reported yard flooding. A total of five (5) residents reported erosion threatening streets, yards, garages, or fences. See Figure 2-2 for locations of reported erosion. A sample questionnaire and the tabulated results are provided in Appendix D.

On November 4, 2014, the City provided another avenue for obtaining citizen input by holding a public meeting. An open house format allowed property owners to attend at their convenience and speak to City staff or representatives from WK Dickson. Nine (9) residents from the watershed provided feedback at the meeting. All of these residents were located within the City limits. Minutes from this meeting are included in Appendix D. The results and comments from the citizen's input contributed significantly to the identification and prioritization of problem areas, and validation of model results.

2.2 WATERSHED CHARACTERISTICS

The Fork Swamp watershed is approximately 6,800 acres (10.6 square miles) between its downstream boundary in the vicinity of Worthington Road and its upstream boundary along SE Greenville Boulevard. Approximately 60% of this total watershed area is located within the City limits. Land use in the watershed is approximately 75 percent built out as shown on the Existing Conditions Land Use Map included in Appendix C. The existing land use in the watershed is mostly residential and smaller percentages of commercial, office, and institutional (See Table 2-1a). The soils within the watershed are predominately NRCS hydrologic groups B/D and C as shown on the Soils Map included in Appendix C. More detailed information about the land use and soils in the Fork Swamp watershed is provided in Appendix A.

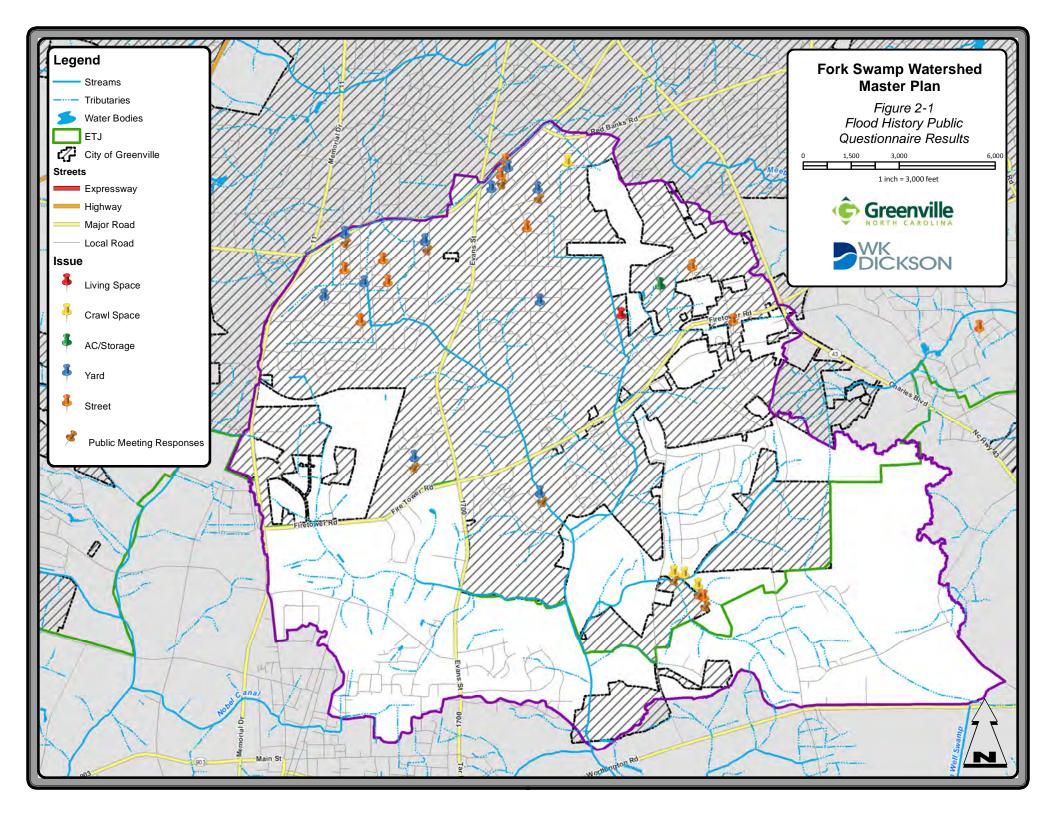
SECTION 2: EXISTING WATERSHED CONDITIONS

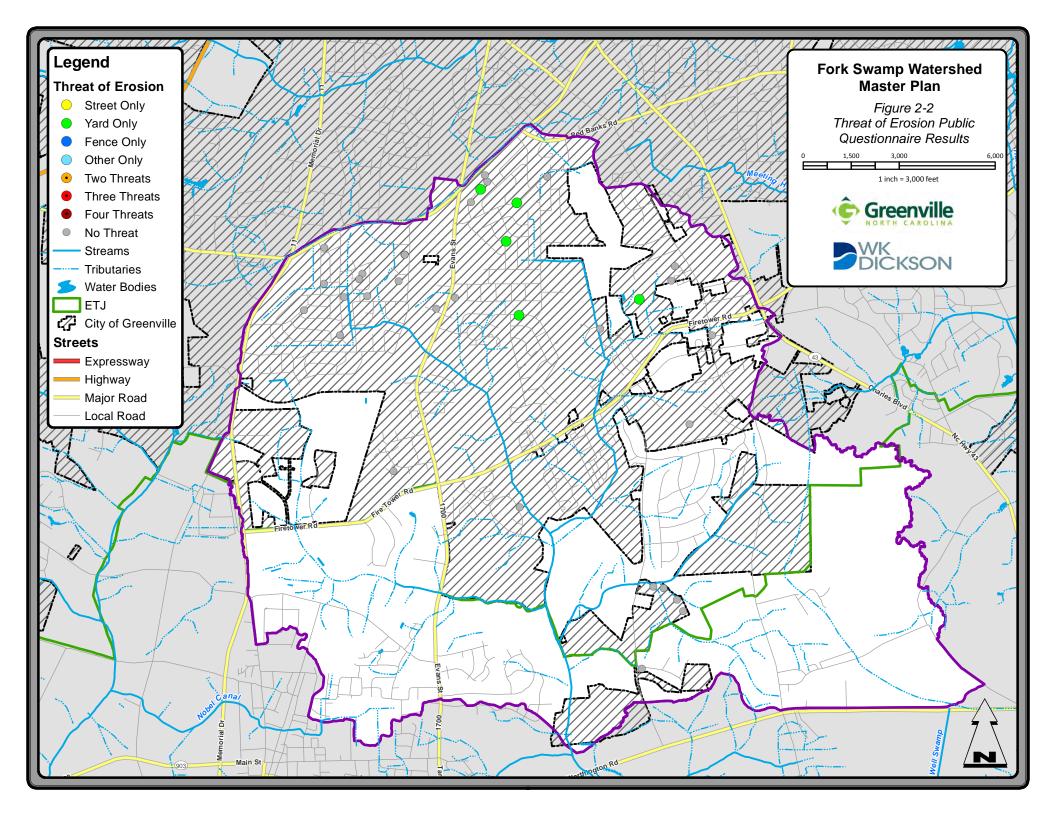
Table 2-1a: Fork Swamp Watershed Existing Land Use

Land Use Category	Area (acres)
Commercial	452
Mixed Use/Office/Institutional	29
Office/Institutional/Multi-Family	293
Office/Institutional/Medical	67
High Density Residential	508
Medium Density Residential	1,149
Low Density Residential	572
Very Low Density Residential	905
Conservation/Open Space	2,067
Right-of-Way	733
Industrial	32

Table 2-1b: Fork Swamp Watershed Future Land Use

Land Use Category	Area (acres)
Commercial	617
Mixed Use/Office/Institutional	33
Office/Institutional/Multi-Family	381
Office/Institutional/Medical	67
High Density Residential	623
Medium Density Residential	2,074
Low Density Residential	576
Very Low Density Residential	1,146
Conservation/Open Space	628
Right-of-Way	733
Industrial	32





2.3 Existing Conditions Survey and Field Data Collection

For the Fork Swamp Watershed Master Plan, stormwater utility infrastructure throughout the watershed was collected by WK Dickson and River & Associates personnel to compile a Geographic Information System (GIS) stormwater inventory database for the City. This was accomplished by using Global Positioning Systems (GPS) at the primary means of data capture. Survey grade employed GPS to locate the x, y, and z coordinates of each visible stormwater system structure and conventional surveying techniques to obtain attributes including but not limited to size, material, slope, and length. The data was collected using horizontal datum NAD 1983 and vertical datum NAVD 1988. A total of 2,379 closed system structures and 208,261 linear feet of pipe were collected as part of the inventory. Tables 2-2 and 2-3 summarize the inventory collected in the Fork Swamp watershed.

Table 2-2: Inventory Summary – Closed System Structures

Structure Type	Number Surveyed		
Yard Inlet	220		
Drop Inlet	65		
Junction Box	103		
Pipe End	533		
Pond Structure	8		
Slab Top Inlet	8		
Catch Basin	1,416		
Underground Pipe Junction	26		

Table 2-3: Inventory Summary – Pipes

Size	Length (Linear Feet)			
12" Diameter	152			
15" Diameter	35,292			
18" Diameter	40,753			
24" Diameter	47,174			
30" Diameter	27,939			
36" Diameter	23,640			
42" Diameter	10,895			
48" Diameter	9,458			
54" Diameter	2,647			
60" Diameter	2,036			
66" Diameter	799			
72" Diameter	525			
84" Diameter	382			

SECTION 2: EXISTING WATERSHED CONDITIONS

Data was obtained for those open channels required to complete connectivity for modeling purposed. Attributes such as shape, lining type, bed type, flow, bottom width, top width, and bank heights were collected for 160 open channel sections totaling over 24 miles in length. For those sections of open channel where more detailed information was required for model input, cross sections were surveyed. Data including elevations for the top of the back, bottom of bank, and channel centerline was obtained for eighty-nine (89) cross sections to supplement the existing FEMA Cross section data. One (1) bridge was also included in the inventory. Refer to the City of Greenville's Storm Water System Inventory Standard Operating Procedures for additional information about the processes and details of the inventory database.

EXISTING WATERSHED ANALYSIS

3.1 Primary System Hydrologic and Hydraulic Analyses

3.1.1 Hydrology

The purpose of the hydrologic analysis is to estimate the magnitude of selected frequency floods for the Fork Swamp Watershed. The United States Army Corps of Engineers (USACE) HEC-HMS was selected to model the primary systems. HEC-HMS simulates the surface runoff response to precipitation for an interconnected system of surfaces, channels, and ponds. Input data for the HEC-HMS model was developed using topographic, land use, and soils maps in GIS to delineate and calculate the basin areas and Natural Resources Conservation Service (NRCS) hydrologic parameters. Detailed descriptions of the model parameters can be found in Appendices A and B.

The HEC-HMS model offers a variety of methods for simulating the rainfall-runoff response, hydrograph development, channel and pond routing. The selection of methods for the analyses is based on the study objectives, data availability, and watershed characteristics. The precipitation data for the 24-hour duration, Type III storm was used to represent the synthetic rainfall event. The Type III storm was selected based on the location of the City of Greenville. The geographic boundaries for the different NRCS rainfall distributions are shown on Figure B-2 of NRCS document <u>Urban Hydrology for Small Watersheds</u>, dated June 1986 and commonly referred to as TR-55 (See Appendix A). As shown in TR-55 for the coastal regions of North Carolina including Greenville, a Type III storm is more characteristic. The NRCS curve number approach was selected to calculate runoff volumes from the precipitation data, and the subbasin unit hydrographs for these flood volumes were developed using the NRCS lag times.

Peak flows for the primary systems were developed for the 2-, 10-, 25-, 50- and 100-year storm events. The existing conditions flows were developed assuming attenuation occurs at the following locations:

- East Baywood Lane (Fork Swamp)
- Railroad Crossing (Fork Swamp)
- Evans Street (Fork Swamp)
- Corey Road (FSUT1)
- Trafalgar Drive North (FSUT1)
- Trafalgar Drive South (FSUT1)
- West Fire Tower Road (FSUT2R2)
- County Home Road (FSUT3)
- East Fire Tower Road Upstream (FSUT3)
- Wimbledon Drive (FSUT3)
- Tower Place (FSUT3)
- Coleman Drive (FSUT3)

Storage routing was modeled just upstream of the culverts listed above because of the large storage volume available behind the pipe's entrance. The culverts that have not been included provide little to no accessible storage volume in the area upstream of its respective crossing. The results of the hydrologic model used as input for HEC-RAS are summarized in Table 3-1. A hard copy of the HEC-HMS output is included as Appendix H. The CD found in Appendix J contains this digital information.

Table 3-1: Existing Conditions Flows from HEC-HMS for Fork Swamp Watershed

Dood Name /	HEC-	HEC- Storm Event				
	RAS	2-year	10-year	25-year	50-year	100-year
Location		<u> </u>	(cfs)	(cfs)	(cfs)	(cfs)
	FORK S	SWAMP	1			
_	55891	188	352	468	569	681
						916
	54609	256	486	642	784	937
	50168	438	844	1.138	1.395	1,681
				,	,	,
	46060	500	1.055	1,414	1,756	2,122
Swamp	46863	538	1,055			
Confluence of						
FSUT2 and Fork	44420	757	1,477	2,003	2,486	3,052
Swamp						
Confluence of						
FSUT1 and Fork	43230	963	1,937	2,637	3,288	4,025
Swamp						
	FORK SW	VAMP UT	1			
-						
O	5103	107	223	309	387	474
Trafalgar Drive – North	4235	111	231	319	399	490
Corey Road	3380	195	410	577	719	897
				377	717	071
			1			
		l .	1	604	752	914
U/S Limit Upstream Limit of Up						
_	4262	49	90	118	143	171
				-10	- 10	
	303	99	201	276	343	419
Road						
Upstream Limit of FSUT3	4360	108	213	290	358	434
	Confluence of FSUT2 and Fork Swamp Confluence of FSUT1 and Fork Swamp Upstream Limit of FSUT1/Trafalgar Drive – South Trafalgar Drive – North Corey Road Upstream Limit of FSUT2 West Fire Tower Road Upstream Limit of	RAS Station FORK S East Baywood Lane Railroad East Fire Tower Road Confluence of FSUT3 and Fork Swamp Confluence of FSUT2 and Fork Swamp Confluence of FSUT1 and Fork Swamp FORK SW Upstream Limit of FSUT1/Trafalgar Drive – South Trafalgar Drive – North Corey Road 3380 FORK SW Upstream Limit of FSUT2 West Fire Tower Road TORK SW Upstream Limit of FSUT2 West Fire Tower Road FORK SW Upstream Limit of FSUT2 FORK SW Upstream Limit of FSUT2 FORK SW Upstream Limit of FSUT2 FORK SW Upstream Limit of FSUT2	RAS Station Station Cfs	RAS Station C(fs) C(fs)	Road Name Location	RAS Station RAS Station C(fs) C(fs

HEC-HMS	Road Name /	HEC-		Storm Event			
Node	Location	RAS	2-year	10-year	25-year	50-year	100-year
		Station	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)
Coleman Drive	Coleman Drive	289	141	290	401	500	612
C + II	County Home	10420	62	113	148	178	211
County Home	Road						
East Fire Tower	East Fire Tower	8790	89	163	202	250	295
Road – North	Road – U/S						
Wimbledon	IA7:1-1- 1 Dui 00'	0220 142	200	221	400	407	
Drive	Wimbledon Drive	8238	142	260	331	409	486
Tower Pl_	Tower Place/	7(04/					
Summerhaven	Summerhaven	7694/ 7287	159	302	392	487	583
Dr	Drive	7287					
East Fire Tower	East Fire Tower	5065	308	610	810	1,012	1,220
Road - South	Road – D/S						

3.1.2 Hydraulics

The purpose of the hydraulic analysis is to determine an existing level of flooding for the storm drainage network and to develop proposed solutions to mitigate flooding. The USACE HECRAS was selected to model the primary systems to remain consistent the existing FEMA modeling. HEC-RAS calculates water surface profiles for steady, gradually varied flow in channels and floodplains. The standard backwater analysis for sub-critical flow was modeled for the Fork Swamp Watershed. The model calculates the effect of obstructions, such as culverts, and building structures in the channel and floodplain on the water surface profile. The hydraulic computations are based on the solution of a one-dimensional energy equation with energy loss due to friction evaluated by Manning's equation. Input data for HEC-RAS include the following:

- Cross-section geometry of the channel and floodplain;
- Roughness coefficients to describe characteristics of the channel and floodplain;
- Size, shape, and characteristics of culverts and roadways along the stream reach; and
- Energy loss coefficients for flow in the channel and at roadway crossings.

Channel cross sections utilized in the HEC-RAS model were based on the existing FEMA cross sections and WK Dickson surveyed cross sections. The channel cross sections were merged with State LiDAR data to develop cross sections spanning the entire floodplain area.

There were five (5) separate HEC-RAS models developed to analyze the stream reaches located in the Fork Swamp watershed. The starting water surface elevations for the HEC-RAS models were calculated using the slope-area method for three (3) of the models. The calculated normal depths are as follows:

0.0037 feet/feet for Fork Swamp Main Branch

- 0.0043 feet/feet for Fork Swamp UT2-R2
- 0.0035 feet/feet for Fork Swamp UT3

For the Fork Swamp UT1 (FSUT1) and Fork Swamp UT2-R1 (FSUT2R1) HEC-RAS models, the starting water surfaces elevations were set based on values calculated in the Fork Swamp Main Branch HEC-RAS model.

Hydraulic Performance

Sixteen (16) roadway crossings were analyzed for flooding potential for the primary system. Descriptions of the existing primary system crossings analyzed are summarized in Table 3-2. Pictures 3-1 through 3-14 of this report provide a visual image of the primary system crossings.

Table 3-2: Existing Condition of Primary System Crossings

Location	Size/Material	Condition
East Baywood Lane (Main Branch)	Twin 72" CMPs	Good
Railroad (Main Branch)	Twin 84" CMPs	Fair
Evans Street (Main Branch)	Twin 84" CMPs	Fair
East Fire Tower Road(Main Branch)	Bridge	Good
Trafalgar Drive – South (FSUT1)	Twin 60" CMPs	Good
Trafalgar Drive – North (FSUT1)	60" CMP and 66" CMP	Good
Corey Road (FSUT1)	Twin 13' x 4.5' CMP Arches	Good
Old Tar Toad (FSUT2-R1)	72" CMP	Poor – Rusted Bottom
West Fire Tower Road (FSUT2 – R2)	10′ x 8′ RCBC	Good
Coleman Drive (FSUT3)	Triple 10' x 4' RCBCs	Good
County Home Road (FSUT3)	Twin 48" RCPs	Good
East Fire Tower Road – U/S (FSUT3)	Twin 54" RCPs	Good
Wimbledon Drive (FSUT3)	Twin 60" CMPs	Fair
Tower Place (FSUT3)	Twin 66" CMPs	Fair
Summerhaven Drive (FSUT3)	Twin 66" CMPs	Fair
East Fire Tower Road – U/S (FSUT3)	Twin 10' x 7' CMP Ellipses	Good



Picture 3-1. East Baywood Lane Culvert – Upstream Face



Picture 3-2. Railroad Crossing Culvert – Upstream Face

SECTION 3: EXISTING WATERSHED ANALYSIS



Picture 3-3. Evans Street Culvert – Downstream Face



Picture 3-5. Trafalgar Drive – North Culvert – Downstream Face



Picture 3-7. West Fire Tower Road Culvert – Downstream Face



Picture 3-4. Trafalgar Drive – South Culvert – Downstream Face



Picture 3-6. Corey Road Culvert – Upstream Face



Picture 3-8. Coleman Drive Culvert – Downstream Face

SECTION 3: EXISTING WATERSHED ANALYSIS



Picture 3-9. County Home Road Culvert – Upstream Face



Picture 3-10. East Tower Road –U/S Culvert – Upstream Face



Picture 3-11. Wimbledon Drive Culvert – Upstream Face



Picture 3-12. Tower Place Culvert – Downstream Face



Picture 3-13. Summerhaven Drive Culvert – Upstream Face



Picture 3-14. East Tower Road –D/S Culvert – Upstream Face

SECTION 3: EXISTING WATERSHED ANALYSIS

The 2-, 10-, 25-, 50- and 100-year existing conditions flood elevations for the primary system crossings are identified in Table 3-3. The minimum elevations at the top of the road for each crossing are also listed in Table 3-3. Along Fork Swamp, none of the four crossings are meeting its desired level of service. East Baywood Lane is operating at a 2-year level of service while the railroad crossing, Evans Street, East Fire Tower Road have a 25-year level of service. The desired level of service for East Baywood Lane and the railroad crossing are the 25-year and 100-year storms, respectively. Evans Street and East Fire Tower Road are major thoroughfares with a desired 50-year level of service.

Along FSUT1, one out of the three crossings is meeting its desired level of service. The desired level of service for Trafalgar Drive – South, Trafalgar Drive – North, and Corey Road is the 25-year storm. As shown in Table 3-3, Trafalgar Drive – South is providing a 2-year level of service while Trafalgar Drive – North is providing a 10-year level of service. The new culvert at the Corey Road crossing is performing at the desired 25-year level of service.

There is only one roadway crossing along FSUT2R1, Old Tar Road. It is located on the edge of the City's limit and operating at a 2-year level of service. This is below the 25-year desired level of service. Along FSUT2R2 there is one roadway crossing, West Fire Tower Road. The desired level of service at this location is 50-year. Currently, West Fire Tower Road exceeds a 100-year storm with over 18 inches of freeboard.

Along FSUT3, one out of the seven crossings is meeting its desired level of service. As shown in Table 3-3, only Coleman Drive is providing the desired 25-year level of service while the remaining Wimbledon Drive, Tower Place, and Summerhaven Drive are performing at a 2-year level of service. The desired level of service for Coleman Drive, Wimbledon Drive, Tower Place, and Summerhaven Drive is the 25-year storm. County Home Road, East Fire Tower Road – U/S, and East Fire Tower Road – D/S are desired to meet a 50-year level of service. Currently, County Home Road provides a 10-year level of service while East Fire Tower Road – U/S and East Fire Tower Road – D/S only operate at a 2-year level or service.

Table 3-3: Hydraulic Performance for Existing Conditions Roadway Flooding

Table 3-3: Hydraulic I	Minimum Elevation at	Desired Level of	Calculated Water Surface Elevations (fee NAVD)			s (feet	
Location	Top of Road	Service	2-year	10-year	25-year	50-year	100-year
	(feet NAVD)	(Year)	flood	flood	flood	flood	flood
		FORK S	WAMP				
East Baywood Lane (Culvert)	66.01	25-year	63.88	66.27	68.77	70.98	71.36
Railroad (Culvert)	70.89	100-year	63.05	65.99	68.74	70.97	71.35
Evans Street (Culvert)	66.51	50-year	61.42	63.97	65.78	66.88	67.20
East Fire Tower Road (Bridge)	58.23	50-year	55.49	57.02	57.39	58.33	58.68
		FORK SWA	AMP UT1				
Trafalgar Drive – South (Culvert)	55.81	25-year	53.69	55.95	56.29	56.48	56.63
Trafalgar Drive – North (Culvert)	54.35	25-year	53.05	54.67	55.14	55.43	55.78
Corey Road (Culvert)	54.81	25-year	52.31	53.39	54.26	55.05	55.43
		FORK SWA	MP UT2R	1			
Old Tar Road (Culvert)	55.64	25-year	55.44	56.26	56.59	56.71	56.86
		FORK SWA	MP UT2R	2			
West Fire Tower Road (Culvert)	65.70	50-year	60.61	61.90	62.67	63.30	63.96
		FORK SWA	AMP UT3				
Coleman Drive (Culvert)	61.97	25-year	59.18	61.26	61.96	62.44	62.81
County Home Road (Culvert)	65.81	50-year	63.09	65.51	66.13	66.45	66.72
East Fire Tower Road – U/S (Culvert)	64.51	50-year	61.96	64.72	64.96	65.16	65.32
Wimbledon Drive (Culvert)	63.61	50-year	61.69	64.09	64.25	64.35	64.44
Tower Place (Culvert)	63.01	25-year	60.62	63.02	63.29	63.45	63.58
Summerhaven Drive (Culvert)	61.51	25-year	59.81	62.13	62.49	62.75	62.93
East Fire Tower Road – U/S (Culvert)	59.51	25-year	57.48	59.74	60.20	60.49	60.72

^{*}Bold text indicates the existing water surface has exceeded the crest or low point in the road thereby causing flooding.

In addition to evaluating the roadway crossings, an evaluation was performed to determine the residences along the primary system streams that are at risk of flooding during the 25- and 100-year storm event. The existing 25- and 100-year floodplains for these streams are shown in Figures 3-1 through 3-8. The mapped floodplains are based on model results obtained as part of the Master Plan and may differ from the published FEMA floodplains. For flood insurance

^{**} Green shade indicates crossing meets desired level of service. Red shade indicates crossing does not meet desired level of service.

purposes, the effective FEMA floodplain should be referenced. For structures outside of the 100-year effective FEMA floodplain, property owners must determine if purchasing flood insurance is necessary. The City is in no way responsible for determining if flood insurance is required or for notifying property owners of the potential risk of flooding.

Tables 3-4 through 3-8 lists the lowest adjacent grade elevations along with the existing 25- and 100-year water surface elevation for those properties at risk of flooding. The lowest adjacent grade (LAG) elevations shown in the table are not surveyed and are estimated based on the State of North Carolina's LiDAR data. LAG flooding shown in the tables may not result in actual LAG or finished floor flooding, but it is indicative of structures being at risk of flooding.

Table 3-4: Existing Conditions At-Risk Properties/Structures – Fork Swamp

	LAG	Calculated Water Surfac	ce Elevations (feet NAVD)
Address	(feet NAVD)	25-year flood	100-year flood
4004 ALBION DR	58.70	57.68	58.77
102 AMBER LN	70.00	68.80	71.36
103 AMBER LN	70.00	68.80	71.36
104 AMBER LN	70.00	68.80	71.36
102 ANTLER RD	70.00	68.80	71.36
103 ANTLER RD	70.53	68.80	71.36
104 ANTLER RD	70.00	68.80	71.36
105 ANTLER RD	70.16	68.80	71.36
106 ANTLER RD	70.00	68.80	71.36
107 ANTLER RD	70.16	68.80	71.36
108 ANTLER RD	70.00	68.80	71.36
109 ANTLER RD	70.62	68.80	71.36
110 ANTLER RD	70.00	68.80	71.36
111 ANTLER RD	70.62	68.80	71.36
112 ANTLER RD	70.05	68.80	71.36
114 ANTLER RD	71.02	68.80	71.36
126 ANTLER RD	70.37	68.80	71.36
129 ANTLER RD	71.10	68.80	71.36
131 ANTLER RD	70.00	68.80	71.36
133 ANTLER RD	70.00	68.80	71.36
100 E BAYWOOD LN	69.33	68.80	71.36
101 E BAYWOOD LN	69.16	68.80	71.36
102 E BAYWOOD LN	69.57	68.80	71.36
103 E BAYWOOD LN	69.16	68.80	71.36
104 E BAYWOOD LN	69.57	68.80	71.36
105 E BAYWOOD LN	69.03	68.80	71.36
106 E BAYWOOD LN	68.29	68.80	71.36
107 E BAYWOOD LN	69.03	68.80	71.36

	LAG	Calculated Water Surface	ce Elevations (feet NAVD)
Address	(feet NAVD)	25-year flood	100-year flood
201 E BAYWOOD LN	68.00	68.80	71.36
203 E BAYWOOD LN	68.00	68.80	71.36
205 E BAYWOOD LN	68.00	68.80	71.36
3101 E BAYWOOD LN	69.06	68.80	71.36
3200 E BAYWOOD LN	68.01	68.80	71.36
3202 E BAYWOOD LN	69.79	68.80	71.36
3203 E BAYWOOD LN	70.00	68.80	71.36
3205 E BAYWOOD LN	70.00	68.80	71.36
3301 E BAYWOOD LN	70.00	68.79	71.36
3303 E BAYWOOD LN	70.00	68.78	71.36
3400 E BAYWOOD LN	68.59	68.78	71.36
3402 E BAYWOOD LN	68.00	68.78	71.36
3403 E BAYWOOD LN	68.00	68.77	71.35
3404 E BAYWOOD LN	66.00	68.77	71.36
3405 E BAYWOOD LN	66.02	68.77	71.35
3406 E BAYWOOD LN	66.00	68.77	71.36
3407 E BAYWOOD LN	66.02	68.77	71.35
3409 E BAYWOOD LN	66.02	68.77	71.35
3411 E BAYWOOD LN	66.00	68.77	71.35
3501 E BAYWOOD LN	66.00	68.77	71.35
3503 E BAYWOOD LN	66.00	68.77	71.35
3505 E BAYWOOD LN	65.34	68.77	71.35
3601 E BAYWOOD LN	65.34	68.77	71.35
3603 E BAYWOOD LN	69.62	68.77	71.35
100 S BAYWOOD LN	66.31	68.80	71.36
102 S BAYWOOD LN	68.03	68.80	71.36
103 S BAYWOOD LN	69.33	68.80	71.36
104 S BAYWOOD LN	67.72	68.80	71.36
105 S BAYWOOD LN	70.00	68.80	71.36
106 S BAYWOOD LN	70.00	68.80	71.36
107 S BAYWOOD LN	70.00	68.80	71.36
108 S BAYWOOD LN	70.00	68.80	71.36
109 S BAYWOOD LN	70.00	68.80	71.36
110 S BAYWOOD LN	69.19	68.80	71.36
111 S BAYWOOD LN	70.00	68.80	71.36
112 S BAYWOOD LN	69.19	68.80	71.36
114 S BAYWOOD LN	68.86	68.80	71.36
116 S BAYWOOD LN	68.86	68.80	71.36
202 S BAYWOOD LN	68.00	68.80	71.36

	LAG	Calculated Water Surface	ce Elevations (feet NAVD)
Address	(feet NAVD)	25-year flood	100-year flood
203 S BAYWOOD LN	70.00	68.80	71.36
204 S BAYWOOD LN	70.00	68.80	71.36
205 S BAYWOOD LN	70.00	68.80	71.36
206 S BAYWOOD LN	70.00	68.80	71.36
207 S BAYWOOD LN	70.00	68.80	71.36
208 S BAYWOOD LN	70.00	68.80	71.36
209 S BAYWOOD LN	70.00	68.80	71.36
210 S BAYWOOD LN	70.00	68.80	71.36
211 S BAYWOOD LN	70.00	68.80	71.36
207 BELVEDERE DR	71.17	68.80	71.36
209 BELVEDERE DR	70.00	68.80	71.36
210 BELVEDERE DR	70.00	68.80	71.36
211 BELVEDERE DR	70.00	68.80	71.36
212 BELVEDERE DR	70.00	68.80	71.36
213 BELVEDERE DR	70.00	68.80	71.36
214 BELVEDERE DR	70.00	68.80	71.36
215 BELVEDERE DR	70.00	68.80	71.36
217 BELVEDERE DR	70.00	68.80	71.36
218 BELVEDERE DR	70.00	68.80	71.36
219 BELVEDERE DR	70.00	68.80	71.36
220 BELVEDERE DR	70.00	68.80	71.36
222 BELVEDERE DR	70.00	68.80	71.36
302 BELVEDERE DR	70.60	68.80	71.36
204 BENT CREEK DR	67.15	68.79	71.36
206 BENT CREEK DR	69.89	68.80	71.36
208 BENT CREEK DR	65.64	68.80	71.36
210 BENT CREEK DR	70.31	68.80	71.36
3800 BOXWOOD LN	70.00	68.80	71.36
3802 BOXWOOD LN	70.00	68.80	71.36
3804 BOXWOOD LN	70.00	68.80	71.36
3806 BOXWOOD LN	70.00	68.80	71.36
102 BRIARWOOD DR	70.00	68.80	71.36
103 BRIARWOOD DR	70.00	68.80	71.36
104 BRIARWOOD DR	70.00	68.80	71.36
105 BRIARWOOD DR	70.00	68.80	71.36
106 BRIARWOOD DR	70.00	68.80	71.36
107 BRIARWOOD DR	70.00	68.80	71.36
200 BRISTOL CT	67.74	68.80	71.36
201 BRISTOL CT	67.49	68.80	71.36

		LAG	Calculated Water Surface	ce Elevations (feet NAVD)
	Address	(feet NAVD)	25-year flood	100-year flood
202	BRISTOL CT	68.90	68.80	71.36
203	BRISTOL CT	69.90	68.80	71.36
204	BRISTOL CT	68.90	68.80	71.36
205	BRISTOL CT	70.86	68.80	71.36
206	BRISTOL CT	69.78	68.80	71.36
207	BRISTOL CT	70.86	68.80	71.36
208	BRISTOL CT	70.00	68.80	71.36
209	BRISTOL CT	71.28	68.80	71.36
210	BRISTOL CT	70.00	68.80	71.36
211	BRISTOL CT	71.28	68.80	71.36
212	BRISTOL CT	70.00	68.80	71.36
731	CEDAR RIDGE DR	53.17	52.29	53.31
737	CEDAR RIDGE DR	53.17	52.28	53.30
743	CEDAR RIDGE DR	51.77	52.26	53.28
749	CEDAR RIDGE DR	51.77	52.25	53.27
751	CEDAR RIDGE DR	53.20	52.23	53.25
329	CEDARHURST RD	70.38	68.80	71.36
330	CEDARHURST RD	70.00	68.80	71.36
332	CEDARHURST RD	70.00	68.80	71.36
400	CEDARHURST RD	70.00	68.80	71.36
401	CEDARHURST RD	70.00	68.80	71.36
402	CEDARHURST RD	70.00	68.80	71.36
403	CEDARHURST RD	70.00	68.80	71.36
404	CEDARHURST RD	70.00	68.80	71.36
405	CEDARHURST RD	70.00	68.80	71.36
407	CEDARHURST RD	70.00	68.80	71.36
500	CEDARHURST RD	70.00	68.80	71.36
502	CEDARHURST RD	70.00	68.80	71.36
503	CEDARHURST RD	70.00	68.80	71.36
504	CEDARHURST RD	70.00	68.80	71.36
505	CEDARHURST RD	70.00	68.80	71.36
506	CEDARHURST RD	70.00	68.80	71.36
507	CEDARHURST RD	70.00	68.80	71.36
508	CEDARHURST RD	70.00	68.80	71.36
509	CEDARHURST RD	70.00	68.80	71.36
510	CEDARHURST RD	69.74	68.80	71.36
511	CEDARHURST RD	70.00	68.80	71.36
512	CEDARHURST RD	69.74	68.80	71.36
513	CEDARHURST RD	70.00	68.80	71.36

LAG		Calculated Water Surface Elevations (feet NAVD)		
Address	(feet NAVD)	25-year flood	100-year flood	
514 CEDARHURST RD	70.00	68.80	71.36	
515 CEDARHURST RD	70.62	68.80	71.36	
516 CEDARHURST RD	70.25	68.80	71.36	
601 CEDARHURST RD	70.62	68.80	71.36	
603 CEDARHURST RD	70.07	68.80	71.36	
604 CEDARHURST RD	70.00	68.80	71.36	
605 CEDARHURST RD	70.00	68.80	71.36	
606 CEDARHURST RD	70.00	68.80	71.36	
607 CEDARHURST RD	70.00	68.80	71.36	
608 CEDARHURST RD	70.00	68.80	71.36	
609 CEDARHURST RD	70.00	68.80	71.36	
700 CEDARHURST RD	70.00	68.80	71.36	
701 CEDARHURST RD	70.00	68.80	71.36	
702 CEDARHURST RD	70.00	68.80	71.36	
703 CEDARHURST RD	70.00	68.80	71.36	
600 CHELTENHAM DR	70.58	68.80	71.36	
608 CHELTENHAM DR	70.00	68.80	71.36	
612 CHELTENHAM DR	70.00	68.80	71.36	
628 CHELTENHAM DR	70.65	68.80	71.36	
102 CLAYBOURNE CT	69.14	68.80	71.36	
104 CLAYBOURNE CT	69.14	68.80	71.36	
106 CLAYBOURNE CT	69.14	68.80	71.36	
108 CLAYBOURNE CT	70.00	68.80	71.36	
201 CLAYBOURNE CT	68.00	68.80	71.36	
103 CLUB PINES DR	70.32	68.80	71.36	
200 CLUB PINES DR	70.94	68.80	71.36	
205 CLUB PINES DR	70.38	68.80	71.36	
206 CLUB PINES DR	72.00	68.80	71.36	
300 CLUB PINES DR	70.62	68.80	71.36	
301 CLUB PINES DR	70.21	68.80	71.36	
302 CLUB PINES DR	70.19	68.80	71.36	
303 CLUB PINES DR	70.21	68.80	71.36	
304 CLUB PINES DR	70.19	68.80	71.36	
305 CLUB PINES DR	70.53	68.80	71.36	
400 CLUB PINES DR	70.00	68.80	71.36	
401 CLUB PINES DR	70.00	68.80	71.36	
402 CLUB PINES DR	70.00	68.80	71.36	
403 CLUB PINES DR	70.00	68.80	71.36	
500 CLUB PINES DR	70.00	68.80	71.36	

	LAG	Calculated Water Surface	ce Elevations (feet NAVD)
Address	(feet NAVD)	25-year flood	100-year flood
503 CLUB PINES DR	70.00	68.80	71.36
507 CLUB PINES DR	70.00	68.80	71.36
601 CLUB PINES DR	70.00	68.80	71.36
603 CLUB PINES DR	70.91	68.80	71.36
3296 COLONY CT	70.00	68.80	71.36
898 CORBETT ST	52.90	51.99	52.98
4698 COREY RD	48.00	52.13	53.13
102 CRESTLINE PL	69.07	68.80	71.36
104 CRESTLINE PL	70.00	68.80	71.36
200 CRESTLINE BV	70.64	68.80	71.36
202 CRESTLINE BV	70.00	68.80	71.36
203 CRESTLINE BV	72.00	68.80	71.36
204 CRESTLINE BV	70.00	68.80	71.36
205 CRESTLINE BV	70.00	68.80	71.36
206 CRESTLINE BV	70.00	68.80	71.36
207 CRESTLINE BV	70.00	68.80	71.36
208 CRESTLINE BV	70.00	68.80	71.36
209 CRESTLINE BV	70.00	68.80	71.36
210 CRESTLINE BV	70.00	68.80	71.36
211 CRESTLINE BV	70.00	68.80	71.36
212 CRESTLINE BV	70.00	68.80	71.36
213 CRESTLINE BV	70.00	68.80	71.36
214 CRESTLINE BV	70.00	68.80	71.36
215 CRESTLINE BV	70.00	68.80	71.36
216 CRESTLINE BV	70.00	68.80	71.36
217 CRESTLINE BV	69.26	68.80	71.36
300 CRESTLINE BV	70.00	68.80	71.36
301 CRESTLINE BV	70.00	68.80	71.36
302 CRESTLINE BV	70.00	68.80	71.36
303 CRESTLINE BV	68.85	68.80	71.36
304 CRESTLINE BV	70.00	68.80	71.36
305 CRESTLINE BV	68.85	68.80	71.36
307 CRESTLINE BV	68.43	68.80	71.36
309 CRESTLINE BV	66.12	68.80	71.36
311 CRESTLINE BV	66.12	68.80	71.36
313 CRESTLINE BV	70.00	68.80	71.36
400 CRESTLINE BV	70.00	68.80	71.36
401 CRESTLINE BV	69.20	68.80	71.36
402 CRESTLINE BV	70.00	68.80	71.36

	LAG	Calculated Water Surface Elevations (feet NAVD)		
Address	(feet NAVD)	25-year flood	100-year flood	
403 CRESTLINE BV	69.20	68.80	71.36	
404 CRESTLINE BV	70.00	68.80	71.36	
405 CRESTLINE BV	70.00	68.80	71.36	
406 CRESTLINE BV	70.16	68.80	71.36	
407 CRESTLINE BV	70.00	68.80	71.36	
408 CRESTLINE BV	70.16	68.80	71.36	
409 CRESTLINE BV	70.00	68.80	71.36	
410 CRESTLINE BV	70.78	68.80	71.36	
411 CRESTLINE BV	70.00	68.80	71.36	
412 CRESTLINE BV	70.00	68.80	71.36	
413 CRESTLINE BV	70.00	68.80	71.36	
415 CRESTLINE BV	71.36	68.80	71.36	
501 CRESTLINE BV	66.00	68.80	71.36	
502 CRESTLINE BV	71.88	68.80	71.36	
503 CRESTLINE BV	66.00	68.80	71.36	
504 CRESTLINE BV	71.14	68.80	71.36	
505 CRESTLINE BV	67.93	68.80	71.36	
506 CRESTLINE BV	70.00	68.80	71.36	
507 CRESTLINE BV	67.93	68.80	71.36	
508 CRESTLINE BV	70.00	68.80	71.36	
509 CRESTLINE BV	70.00	68.80	71.36	
511 CRESTLINE BV	70.00	68.80	71.36	
512 CRESTLINE BV	70.00	68.80	71.36	
513 CRESTLINE BV	70.00	68.80	71.36	
514 CRESTLINE BV	70.40	68.80	71.36	
515 CRESTLINE BV	70.00	68.80	71.36	
517 CRESTLINE BV	70.00	68.80	71.36	
519 CRESTLINE BV	70.49	68.80	71.36	
522 CRESTLINE BV	70.17	68.80	71.36	
524 CRESTLINE BV	70.17	68.80	71.36	
526 CRESTLINE BV	70.00	68.80	71.36	
528 CRESTLINE BV	70.00	68.80	71.36	
530 CRESTLINE BV	70.00	68.80	71.36	
531 CRESTLINE BV	70.95	68.80	71.36	
532 CRESTLINE BV	70.00	68.80	71.36	
533 CRESTLINE BV	70.00	68.80	71.36	
534 CRESTLINE BV	70.00	68.80	71.36	
535 CRESTLINE BV	70.00	68.80	71.36	
536 CRESTLINE BV	70.00	68.80	71.36	

	LAG	Calculated Water Surface	ce Elevations (feet NAVD)
Address	(feet NAVD)	25-year flood	100-year flood
537 CRESTLINE BV	70.00	68.80	71.36
538 CRESTLINE BV	70.00	68.80	71.36
539 CRESTLINE BV	70.00	68.80	71.36
540 CRESTLINE BV	70.00	68.80	71.36
543 CRESTLINE BV	70.00	68.80	71.36
545 CRESTLINE BV	70.00	68.80	71.36
547 CRESTLINE BV	70.00	68.80	71.36
3401 CUTLER CT	69.09	68.78	71.36
3402 CUTLER CT	68.00	68.80	71.36
3403 CUTLER CT	68.00	68.79	71.36
102 DARWIN CT	70.47	68.80	71.36
104 DARWIN CT	70.47	68.80	71.36
106 DARWIN CT	70.00	68.80	71.36
108 DARWIN CT	70.00	68.80	71.36
4246 DUDLEYS GRANT DR 1	54.00	54.20	54.96
4246 DUDLEYS GRANT DR 2	54.00	54.20	54.96
4246 DUDLEYS GRANT DR 3	54.00	54.20	54.96
4267 DUDLEYS GRANT DR H	54.00	53.38	54.23
4267 DUDLEYS GRANT DR I	54.00	53.46	54.29
4271 DUDLEYS GRANT DR A	54.10	53.30	54.16
4271 DUDLEYS GRANT DR B	54.10	53.27	54.14
4271 DUDLEYS GRANT DR C	54.10	53.25	54.12
4271 DUDLEYS GRANT DR D	51.68	53.08	53.98
4272 DUDLEYS GRANT DR A	54.10	53.26	54.14
4275 DUDLEYS GRANT DR F	51.68	53.08	53.98
4275 DUDLEYS GRANT DR E	51.68	53.13	54.03
4275 DUDLEYS GRANT DR D	51.68	53.05	53.97
4275 DUDLEYS GRANT DR C	51.68	53.05	53.97
4275 DUDLEYS GRANT DR B	51.68	53.08	53.98
4202 DUNHAGAN RD	58.47	58.87	59.69
4204 DUNHAGAN RD	58.00	58.62	59.49
4206 DUNHAGAN RD	58.64	58.53	59.41
4208 DUNHAGAN RD	58.00	58.42	59.33
3400 DUNHAVEN DR	68.00	68.80	71.36
3402 DUNHAVEN DR	68.00	68.80	71.36
3403 DUNHAVEN DR	68.00	68.80	71.36
3404 DUNHAVEN DR	68.73	68.80	71.36
3405 DUNHAVEN DR	68.00	68.80	71.36
3406 DUNHAVEN DR	68.72	68.80	71.36

LAG		Calculated Water Surface Elevations (feet NAVD)		
Address	(feet NAVD)	25-year flood	100-year flood	
3407 DUNHAVEN DR	68.00	68.80	71.36	
3408 DUNHAVEN DR	67.11	68.80	71.36	
3409 DUNHAVEN DR	68.00	68.79	71.36	
3410 DUNHAVEN DR	68.00	68.80	71.36	
3411 DUNHAVEN DR	67.25	68.79	71.36	
3412 DUNHAVEN DR	68.00	68.80	71.36	
3414 DUNHAVEN DR	68.00	68.79	71.36	
3416 DUNHAVEN DR	68.00	68.78	71.36	
430 E FIRE TOWER RD	53.31	56.09	58.86	
413 FORREST PK	58.54	59.30	60.06	
416 FORREST PK	60.00	59.35	60.10	
417 FORREST PK	58.54	59.33	60.08	
420 FORREST PK	58.00	59.43	60.17	
424 FORREST PK	58.00	59.45	60.19	
428 FORREST PK	58.00	59.44	60.18	
432 FORREST PK	58.00	59.32	60.07	
436 FORREST PK	58.00	59.25	60.01	
440 FORREST PK	58.00	59.17	59.95	
441 FORREST PK	58.54	59.28	60.04	
448 FORREST PK	59.07	59.12	59.90	
449 FORREST PK	60.00	59.24	60.01	
2187 FRANKLIN DR	49.13	52.19	53.20	
2197 FRANKLIN DR	49.79	52.15	53.15	
100 GREENWOOD DR	70.00	68.80	71.36	
102 GREENWOOD DR	70.97	68.80	71.36	
103 GREENWOOD DR	70.00	68.80	71.36	
104 GREENWOOD DR	70.00	68.80	71.36	
105 GREENWOOD DR	70.55	68.80	71.36	
106 GREENWOOD DR	70.20	68.80	71.36	
108 GREENWOOD DR	70.20	68.80	71.36	
111 GREENWOOD DR	71.22	68.80	71.36	
113 GREENWOOD DR	70.00	68.80	71.36	
115 GREENWOOD DR	70.52	68.80	71.36	
116 GREENWOOD DR	71.10	68.80	71.36	
118 GREENWOOD DR	70.38	68.80	71.36	
120 GREENWOOD DR	70.20	68.80	71.36	
121 GREENWOOD DR	71.32	68.80	71.36	
123 GREENWOOD DR	71.32	68.80	71.36	
200 GREENWOOD DR	70.00	68.80	71.36	

LAG		Calculated Water Surface Elevations (feet NAVD)		
Address	(feet NAVD)	25-year flood	100-year flood	
202 GREENWOOD DR	70.00	68.80	71.36	
204 GREENWOOD DR	70.00	68.80	71.36	
205 GREENWOOD DR	70.00	68.80	71.36	
206 GREENWOOD DR	70.00	68.80	71.36	
208 GREENWOOD DR	70.00	68.80	71.36	
212 GREENWOOD DR	70.00	68.80	71.36	
301 GREENWOOD DR	70.00	68.80	71.36	
303 GREENWOOD DR	70.00	68.80	71.36	
401 GREENWOOD DR	68.23	68.80	71.36	
403 GREENWOOD DR	68.48	68.80	71.36	
405 GREENWOOD DR	68.48	68.80	71.36	
200 HARMONY ST	70.88	68.80	71.36	
201 HARMONY ST	70.00	68.80	71.36	
203 HARMONY ST	70.00	68.80	71.36	
204 HARMONY ST	70.95	68.80	71.36	
205 HARMONY ST	70.00	68.80	71.36	
206 HARMONY ST	70.00	68.80	71.36	
207 HARMONY ST	70.00	68.80	71.36	
208 HARMONY ST	70.00	68.80	71.36	
209 HARMONY ST	70.00	68.80	71.36	
210 HARMONY ST	70.00	68.80	71.36	
211 HARMONY ST	70.00	68.80	71.36	
212 HARMONY ST	70.00	68.80	71.36	
213 HARMONY ST	70.00	68.80	71.36	
214 HARMONY ST	70.00	68.80	71.36	
215 HARMONY ST	70.00	68.80	71.36	
216 HARMONY ST	70.00	68.80	71.36	
217 HARMONY ST	68.05	68.80	71.36	
219 HARMONY ST	68.05	68.80	71.36	
219 HARTFORD ST	70.62	68.80	71.36	
318 HAVEN DR	68.31	68.80	71.36	
320 HAVEN DR P1	70.00	68.78	71.36	
320 HAVEN DR P5	70.00	68.78	71.36	
320 HAVEN DR P-6	70.00	68.78	71.36	
322 HAVEN DR 2	70.00	68.78	71.36	
322 HAVEN DR 4	70.00	68.78	71.36	
322 HAVEN DR 7	70.00	68.78	71.36	
322 HAVEN DR N1	70.00	68.78	71.36	
322 HAVEN DR N-5	70.00	68.78	71.36	

LAG		Calculated Water Surface	ce Elevations (feet NAVD)
Address	(feet NAVD)	25-year flood	100-year flood
322 HAVEN DR N8	70.00	68.78	71.36
324 HAVEN DR 3	70.00	68.79	71.36
324 HAVEN DR 4	70.00	68.79	71.36
324 HAVEN DR L6	70.00	68.79	71.36
324 HAVEN DR L1	70.00	68.79	71.36
324 HAVEN DR L5	70.00	68.79	71.36
324 HAVEN DR L2	70.00	68.79	71.36
326 HAVEN DR O6	70.00	68.80	71.36
326 HAVEN DR O3	70.00	68.80	71.36
326 HAVEN DR O-2	70.00	68.80	71.36
326 HAVEN DR O5	70.00	68.80	71.36
328 HAVEN DR 8	70.00	68.80	71.36
328 HAVEN DR M1	70.00	68.80	71.36
328 HAVEN DR M2	70.00	68.80	71.36
328 HAVEN DR M3	70.00	68.80	71.36
328 HAVEN DR M4	70.00	68.80	71.36
328 HAVEN DR M5	70.00	68.80	71.36
328 HAVEN DR M6	70.00	68.80	71.36
328 HAVEN DR M7	70.00	68.80	71.36
330 HAVEN DR 4K	70.00	68.80	71.36
330 HAVEN DR 5K	66.00	68.80	71.36
330 HAVEN DR 6K	70.00	68.80	71.36
330 HAVEN DR 1K	70.00	68.80	71.36
330 HAVEN DR 3K	70.00	68.80	71.36
330 HAVEN DR 2K	70.00	68.80	71.36
332 HAVEN DR R1	70.00	68.80	71.36
332 HAVEN DR R2	70.00	68.80	71.36
332 HAVEN DR R3	70.00	68.80	71.36
332 HAVEN DR R4	70.00	68.80	71.36
332 HAVEN DR R5	70.00	68.80	71.36
332 HAVEN DR R6	70.00	68.80	71.36
332 HAVEN DR R7	70.00	68.80	71.36
332 HAVEN DR R8	70.00	68.80	71.36
334 HAVEN DR Q-1	70.00	68.80	71.36
334 HAVEN DR Q-2	70.00	68.80	71.36
334 HAVEN DR Q-3	70.00	68.80	71.36
334 HAVEN DR Q-4	70.00	68.80	71.36
334 HAVEN DR Q-5	70.00	68.80	71.36
334 HAVEN DR Q-6	70.00	68.80	71.36

	LAG	Calculated Water Surface	ce Elevations (feet NAVD)
Address	(feet NAVD)	25-year flood	100-year flood
334 HAVEN DR Q-7	70.00	68.80	71.36
334 HAVEN DR Q-8	70.00	68.80	71.36
334 HAVEN DR Q-9	66.00	68.80	71.36
336 HAVEN DR T1	69.06	68.80	71.36
336 HAVEN DR T2	69.06	68.80	71.36
336 HAVEN DR T3	69.06	68.80	71.36
336 HAVEN DR T4	69.06	68.80	71.36
336 HAVEN DR T5	69.06	68.80	71.36
336 HAVEN DR T6	69.06	68.80	71.36
338 HAVEN DR S1	69.22	68.80	71.36
338 HAVEN DR S2	69.22	68.80	71.36
338 HAVEN DR S3	69.22	68.80	71.36
338 HAVEN DR S4	66.47	68.80	71.36
338 HAVEN DR S5	69.22	68.80	71.36
338 HAVEN DR S6	69.22	68.80	71.36
338 HAVEN DR S7	69.22	68.80	71.36
340 HAVEN DR U-1	68.31	68.80	71.36
340 HAVEN DR U2	68.31	68.80	71.36
340 HAVEN DR U3	69.18	68.80	71.36
340 HAVEN DR U-4	69.18	68.80	71.36
340 HAVEN DR U5	69.18	68.80	71.36
340 HAVEN DR U6	69.18	68.80	71.36
342 HAVEN DR V-1	68.00	68.80	71.36
342 HAVEN DR V-2	68.31	68.80	71.36
342 HAVEN DR V-3	68.31	68.80	71.36
342 HAVEN DR V-4	68.31	68.80	71.36
342 HAVEN DR V5	68.31	68.80	71.36
342 HAVEN DR V6	68.31	68.80	71.36
344 HAVEN DR W1	68.00	68.80	71.36
344 HAVEN DR W2	68.00	68.80	71.36
344 HAVEN DR W3	68.00	68.80	71.36
344 HAVEN DR W4	68.00	68.80	71.36
344 HAVEN DR W5	68.00	68.80	71.36
344 HAVEN DR W6	68.00	68.80	71.36
344 HAVEN DR W7	68.00	68.80	71.36
344 HAVEN DR W-8	68.00	68.80	71.36
344 HAVEN DR W-9	68.00	68.80	71.36
346 HAVEN DR 2	66.00	68.80	71.36
346 HAVEN DR 3	66.00	68.80	71.36

	LAG	Calculated Water Surfa	ce Elevations (feet NAVD)
Address	(feet NAVD)	25-year flood	100-year flood
346 HAVEN DR 6	68.00	68.80	71.36
346 HAVEN DR 8	68.00	68.80	71.36
346 HAVEN DR X 1	66.00	68.80	71.36
346 HAVEN DR X-4	68.00	68.80	71.36
346 HAVEN DR X-5	68.00	68.80	71.36
346 HAVEN DR X7	68.00	68.80	71.36
346 HAVEN DR X-9	68.00	68.80	71.36
348 HAVEN DR 1	66.47	68.80	71.36
348 HAVEN DR 2	66.47	68.80	71.36
348 HAVEN DR 3	66.00	68.80	71.36
348 HAVEN DR AA-4	66.00	68.80	71.36
348 HAVEN DR AA-5	66.00	68.80	71.36
348 HAVEN DR AA-6	66.00	68.80	71.36
350 HAVEN DR Z1	68.00	68.80	71.36
350 HAVEN DR Z-2	68.00	68.80	71.36
350 HAVEN DR Z3	68.00	68.80	71.36
350 HAVEN DR Z-4	68.00	68.80	71.36
350 HAVEN DR Z-5	69.22	68.80	71.36
350 HAVEN DR Z-6	69.22	68.80	71.36
352 HAVEN DR Y 4	68.00	68.80	71.36
352 HAVEN DR Y-1	69.06	68.80	71.36
352 HAVEN DR Y-2	69.06	68.80	71.36
352 HAVEN DR Y-3	68.00	68.80	71.36
352 HAVEN DR Y-5	68.00	68.80	71.36
352 HAVEN DR Y-6	68.00	68.80	71.36
102 HEARTHSIDE DR	70.08	68.80	71.36
103 HEARTHSIDE DR	70.00	68.80	71.36
104 HEARTHSIDE DR	70.08	68.80	71.36
105 HEARTHSIDE DR	70.00	68.80	71.36
106 HEARTHSIDE DR	70.30	68.80	71.36
107 HEARTHSIDE DR	70.00	68.80	71.36
108 HEARTHSIDE DR	70.00	68.80	71.36
109 HEARTHSIDE DR	70.00	68.80	71.36
110 HEARTHSIDE DR	70.00	68.80	71.36
112 HEARTHSIDE DR	70.00	68.80	71.36
114 HEARTHSIDE DR	70.00	68.80	71.36
116 HEARTHSIDE DR	70.00	68.80	71.36
103 IRONWOOD DR	70.00	68.80	71.36
104 IRONWOOD DR	70.57	68.80	71.36

	LAG	Calculated Water Surfa	ce Elevations (feet NAVD)
Address	(feet NAVD)	25-year flood	100-year flood
105 IRONWOOD DR	70.00	68.80	71.36
106 IRONWOOD DR	70.57	68.80	71.36
107 IRONWOOD DR	70.00	68.80	71.36
108 IRONWOOD DR	70.75	68.80	71.36
109 IRONWOOD DR	70.00	68.80	71.36
110 IRONWOOD DR	70.85	68.80	71.36
111 IRONWOOD DR	70.00	68.80	71.36
112 IRONWOOD DR	70.85	68.80	71.36
400 KEMPTON DR	70.00	68.80	71.36
402 KEMPTON DR	70.00	68.80	71.36
403 KEMPTON DR	71.30	68.80	71.36
404 KEMPTON DR	70.00	68.80	71.36
405 KEMPTON DR	70.00	68.80	71.36
406 KEMPTON DR	70.40	68.80	71.36
407 KEMPTON DR	71.17	68.80	71.36
408 KEMPTON DR	70.00	68.80	71.36
410 KEMPTON DR	70.00	68.80	71.36
412 KEMPTON DR	70.00	68.80	71.36
506 KEMPTON DR	70.00	68.80	71.36
507 KEMPTON DR	70.57	68.80	71.36
508 KEMPTON DR	70.00	68.80	71.36
510 KEMPTON DR	70.87	68.80	71.36
604 KEMPTON DR	70.00	68.80	71.36
606 KEMPTON DR	70.00	68.80	71.36
607 KEMPTON DR	71.55	68.80	71.36
700 KEMPTON DR	70.00	68.80	71.36
702 KEMPTON DR	70.00	68.80	71.36
0 LANDMARK ST	70.00	68.77	71.35
326 LANDMARK ST O1	70.00	68.80	71.36
326 LANDMARK ST O4	70.00	68.80	71.36
338 LANDMARK ST	69.22	68.80	71.36
3229 LANDMARK ST	70.61	68.75	71.36
3243 LANDMARK ST	70.00	68.77	71.36
3256 LANDMARK ST A1	70.00	68.78	71.36
3256 LANDMARK ST A2	70.00	68.77	71.36
3256 LANDMARK ST A3	70.00	68.77	71.36
3256 LANDMARK ST A4	70.00	68.77	71.36
3256 LANDMARK ST A5	70.00	68.77	71.36
3256 LANDMARK ST A6	70.00	68.78	71.36

		LAG	Calculated Water Surface	ce Elevations (feet NAVD)
	Address	(feet NAVD)	25-year flood	100-year flood
3258	LANDMARK ST B1	70.00	68.78	71.36
3258	LANDMARK ST B2	70.00	68.78	71.36
3258	LANDMARK ST B3	70.00	68.78	71.36
3258	LANDMARK ST B4	70.00	68.78	71.36
3258	LANDMARK ST B5	70.00	68.78	71.36
3258	LANDMARK ST B6	70.00	68.78	71.36
3258	LANDMARK ST B7	70.00	68.78	71.36
3260	LANDMARK ST C1	70.00	68.78	71.36
3260	LANDMARK ST C2	70.00	68.77	71.36
3260	LANDMARK ST C3	70.00	68.77	71.36
3260	LANDMARK ST C4	70.00	68.77	71.36
3260	LANDMARK ST C5	70.00	68.78	71.36
3260	LANDMARK ST C6	70.00	68.77	71.36
3262	LANDMARK ST D1	70.00	68.78	71.36
3262	LANDMARK ST D2	70.00	68.78	71.36
3262	LANDMARK ST D3	70.00	68.78	71.36
3262	LANDMARK ST D4	70.00	68.77	71.36
3262	LANDMARK ST D5	70.00	68.77	71.36
3262	LANDMARK ST D6	70.00	68.78	71.36
3262	LANDMARK ST E1	70.00	68.78	71.36
3262	LANDMARK ST E2	70.00	68.77	71.36
3262	LANDMARK ST E3	70.00	68.78	71.36
3262	LANDMARK ST E4	70.00	68.78	71.36
3262	LANDMARK ST E5	70.00	68.78	71.36
3262	LANDMARK ST E6	70.00	68.78	71.36
3262	LANDMARK ST E7	70.00	68.78	71.36
3264	LANDMARK ST F1	70.00	68.77	71.36
3264	LANDMARK ST F2	70.00	68.78	71.36
3264	LANDMARK ST F3	70.00	68.78	71.36
3264	LANDMARK ST F4	70.00	68.78	71.36
3264	LANDMARK ST F5	70.00	68.78	71.36
3264	LANDMARK ST F6	70.00	68.78	71.36
3264	LANDMARK ST G1	70.00	68.77	71.36
3264	LANDMARK ST G2	70.00	68.78	71.36
3264	LANDMARK ST G3	70.00	68.77	71.36
3264	LANDMARK ST G4	70.00	68.77	71.36
3264	LANDMARK ST G5	70.00	68.77	71.36
3264	LANDMARK ST G6	70.00	68.78	71.36
3264	LANDMARK ST G7	70.00	68.78	71.36

		LAG	Calculated Water Surfa	ce Elevations (feet NAVD)
	Address	(feet NAVD)	25-year flood	100-year flood
3264	LANDMARK ST G8	70.00	68.78	71.36
3264	LANDMARK ST G9	70.00	68.77	71.36
3275	LANDMARK ST	70.00	68.77	71.35
3300	LANDMARK ST	70.00	68.78	71.36
3300	LANDMARK ST A-1	70.00	68.78	71.36
3300	LANDMARK ST A-2	70.00	68.78	71.36
3300	LANDMARK ST A-3	70.00	68.78	71.36
3300	LANDMARK ST A-4	70.00	68.78	71.36
3300	LANDMARK ST A-4	70.00	68.78	71.36
3300	LANDMARK ST A-5	70.00	68.78	71.36
3300	LANDMARK ST A-6	70.00	68.78	71.36
3308	LANDMARK ST B1	70.00	68.78	71.36
3308	LANDMARK ST B2	70.00	68.78	71.36
3308	LANDMARK ST B3	70.00	68.77	71.36
3308	LANDMARK ST B4	70.00	68.78	71.36
3308	LANDMARK ST B5	70.00	68.77	71.36
3320	LANDMARK ST C-1	69.37	68.76	71.35
3320	LANDMARK ST C-2	70.00	68.78	71.36
3320	LANDMARK ST C-3	70.00	68.78	71.36
3320	LANDMARK ST C-4	70.00	68.78	71.36
3320	LANDMARK ST C-5	70.00	68.77	71.36
3320	LANDMARK ST C-6	70.00	68.78	71.36
3320	LANDMARK ST C-7	70.00	68.78	71.36
3320	LANDMARK ST C-8	70.00	68.78	71.36
3320	LANDMARK ST C-9	70.00	68.78	71.36
3326	LANDMARK ST D1	70.00	68.77	71.36
3326	LANDMARK ST D2	70.00	68.78	71.36
3326	LANDMARK ST D3	70.00	68.78	71.36
3326	LANDMARK ST D4	70.00	68.77	71.36
3326	LANDMARK ST D5	70.00	68.77	71.36
3326	LANDMARK ST D6	70.00	68.77	71.36
3326	LANDMARK ST D7	70.00	68.77	71.36
3326	LANDMARK ST D8	70.00	68.78	71.36
3336	LANDMARK ST H1	70.00	68.77	71.36
3336	LANDMARK ST H2	70.00	68.77	71.36
3336	LANDMARK ST H3	70.00	68.78	71.36
3336	LANDMARK ST H4	70.00	68.78	71.36
3336	LANDMARK ST H5	70.00	68.77	71.36
3336	LANDMARK ST H6	70.00	68.77	71.36

	LAG	Calculated Water Surface	ce Elevations (feet NAVD)
Address	(feet NAVD)	25-year flood	100-year flood
3336 LANDMARK ST H7	70.00	68.78	71.36
3336 LANDMARK ST H8	70.00	68.78	71.36
3344 LANDMARK ST I1	70.00	68.78	71.36
3344 LANDMARK ST I2	70.00	68.77	71.36
3344 LANDMARK ST I3	70.00	68.77	71.36
3344 LANDMARK ST I4	70.00	68.78	71.36
3344 LANDMARK ST I5	70.00	68.78	71.36
3344 LANDMARK ST I6	70.00	68.77	71.36
3344 LANDMARK ST I7	70.00	68.77	71.36
3344 LANDMARK ST I8	70.00	68.78	71.36
3348 LANDMARK ST J1	66.08	68.79	71.36
3348 LANDMARK ST J2	66.08	68.79	71.36
3348 LANDMARK ST J3	66.08	68.80	71.36
3348 LANDMARK ST J4	66.08	68.79	71.36
3348 LANDMARK ST J5	66.08	68.79	71.36
3348 LANDMARK ST J6	66.08	68.79	71.36
3348 LANDMARK ST J7	66.08	68.79	71.36
3385 LANDMARK ST	67.79	68.77	71.35
3395 LANDMARK ST	70.00	68.77	71.35
3398 LANDMARK ST	70.00	68.77	71.36
3401 LANDMARK ST	69.13	68.77	71.35
100 LINDENWOOD DR	70.00	68.80	71.36
102 LINDENWOOD DR	68.47	68.80	71.36
104 LINDENWOOD DR	68.47	68.80	71.36
106 LINDENWOOD DR	69.76	68.80	71.36
108 LINDENWOOD DR	69.76	68.80	71.36
202 LINDENWOOD DR	70.00	68.80	71.36
204 LINDENWOOD DR	70.00	68.80	71.36
513 MARY LEE CT	56.96	58.18	59.14
517 MARY LEE CT	56.96	58.17	59.13
3525 S MEMORIAL DR	70.00	68.80	71.36
3535 S MEMORIAL DR	70.00	68.80	71.36
401 MIDDLEBURY DR	70.00	68.80	71.36
403 MIDDLEBURY DR	70.00	68.80	71.36
405 MIDDLEBURY DR	70.00	68.80	71.36
4101 PARMER PL	59.07	59.14	59.92
4105 PARMER PL	59.19	59.06	59.85
4113 PARMER PL	58.04	58.93	59.75
132 PINE BRANCHES CL	57.00	56.59	57.37

		LAG	Calculated Water Surfa	ce Elevations (feet NAVD)
	Address	(feet NAVD)	25-year flood	100-year flood
133	PINE BRANCHES CL	57.00	56.59	57.37
140	PINE BRANCHES CL	54.00	56.39	57.16
141	PINE BRANCHES CL	54.00	56.35	57.12
142	PINE BRANCHES CL	57.00	56.39	57.16
143	PINE BRANCHES CL	57.00	56.45	57.23
170	PINE BRANCHES CL	56.00	56.21	56.98
172	PINE BRANCHES CL	54.84	56.26	57.03
173	PINE BRANCHES CL	54.84	56.17	56.94
180	PINE BRANCHES CL	55.58	56.07	56.84
181	PINE BRANCHES CL	55.58	55.98	56.75
103	PLACID WY	70.88	68.80	71.36
201	PLACID WY	70.84	68.80	71.36
202	PLACID WY	70.00	68.80	71.36
203	PLACID WY	70.84	68.80	71.36
103	RAVENWOOD DR	70.00	68.80	71.36
105	RAVENWOOD DR	70.00	68.80	71.36
107	RAVENWOOD DR	70.00	68.80	71.36
109	RAVENWOOD DR	70.00	68.80	71.36
111	RAVENWOOD DR	70.00	68.80	71.36
112	RAVENWOOD DR	70.00	68.80	71.36
114	RAVENWOOD DR	70.00	68.80	71.36
116	RAVENWOOD DR	70.00	68.80	71.36
200	RAVENWOOD DR	70.00	68.80	71.36
201	RAVENWOOD DR	70.00	68.80	71.36
202	RAVENWOOD DR	70.00	68.80	71.36
203	RAVENWOOD DR	70.00	68.80	71.36
204	RAVENWOOD DR	70.00	68.80	71.36
206	RAVENWOOD DR	70.00	68.80	71.36
300	RAVENWOOD DR	70.00	68.80	71.36
301	RAVENWOOD DR	70.00	68.80	71.36
302	RAVENWOOD DR	70.00	68.80	71.36
303	RAVENWOOD DR	70.00	68.80	71.36
304	RAVENWOOD DR	70.00	68.80	71.36
878	RAY CRAWFORD DR	49.97	50.54	51.50
886	RAY CRAWFORD DR	49.97	50.53	51.49
894	RAY CRAWFORD DR	49.25	50.51	51.47
895	RAY CRAWFORD DR	50.00	50.73	51.69
899	RAY CRAWFORD DR	50.00	50.70	51.66
901	RAY CRAWFORD DR	49.34	50.62	51.58

	LAG	Calculated Water Surfa	ce Elevations (feet NAVD)
Address	(feet NAVD)	25-year flood	100-year flood
902 RAY CRAWFORD DR	48.00	50.45	51.41
903 RAY CRAWFORD DR	48.09	50.54	51.50
117 RIPLEY DR	70.00	68.80	71.36
120 RIPLEY DR	70.31	68.80	71.36
122 RIPLEY DR	70.31	68.80	71.36
124 RIPLEY DR	71.32	68.80	71.36
102 SHAMROCK CI	70.00	68.80	71.36
104 SHAMROCK CI	70.00	68.80	71.36
106 SHAMROCK CI	70.00	68.80	71.36
108 SHAMROCK CI	70.00	68.80	71.36
807 SPRING RUN RD	54.00	51.37	52.33
813 SPRING RUN RD	50.71	51.25	52.20
825 SPRING RUN RD	50.71	51.09	52.05
835 SPRING RUN RD	50.00	50.93	51.89
0 STAFFORDSHIRE RD	69.56	68.80	71.36
103 STAFFORDSHIRE RD	69.67	68.80	71.36
200 STAFFORDSHIRE RD	68.82	68.80	71.36
201 STAFFORDSHIRE RD	69.56	68.80	71.36
202 STAFFORDSHIRE RD	70.00	68.80	71.36
203 STAFFORDSHIRE RD	70.00	68.80	71.36
204 STAFFORDSHIRE RD	70.00	68.80	71.36
205 STAFFORDSHIRE RD	70.00	68.80	71.36
207 STAFFORDSHIRE RD	70.00	68.80	71.36
209 STAFFORDSHIRE RD	70.00	68.80	71.36
211 STAFFORDSHIRE RD	70.00	68.80	71.36
213 STAFFORDSHIRE RD	70.00	68.80	71.36
302 SYCAMORE BRANCHES CL	53.60	55.15	55.91
303 SYCAMORE BRANCHES CL	56.96	55.48	56.25
304 SYCAMORE BRANCHES CL	54.00	55.56	56.33
3608 THORNBROOK DR	70.00	68.80	71.36
3612 THORNBROOK DR	70.00	68.80	71.36
3616 THORNBROOK DR	68.16	68.80	71.36
3625 THORNBROOK DR	70.00	68.80	71.36
3635 THORNBROOK DR	70.34	68.80	71.36
3644 THORNBROOK DR	70.00	68.80	71.36
3648 THORNBROOK DR	70.55	68.80	71.36
3652 THORNBROOK DR	70.55	68.80	71.36
3656 THORNBROOK DR	70.39	68.80	71.36
4104 TREETOPS CI	53.15	53.86	54.64

	LAG	Calculated Water Surface	Vater Surface Elevations (feet NAVD)	
Address	(feet NAVD)	25-year flood	100-year flood	
4108 TREETOPS CI	54.50	54.07	54.84	
4112 TREETOPS CI	53.67	54.41	55.16	
4114 TREETOPS CI	53.67	54.50	55.25	
4116 TREETOPS CI	55.19	54.70	55.45	
4118 TREETOPS CI	55.19	54.70	55.45	
908 VAN GERT DR	49.74	52.24	53.26	
912 VAN GERT DR	49.48	52.22	53.24	
916 VAN GERT DR	50.69	52.18	53.20	
944 VAN GERT DR	48.99	51.99	52.98	
3700 WALNUT DR	70.00	68.80	71.36	
3702 WALNUT DR	70.00	68.80	71.36	
3703 WALNUT DR	70.00	68.80	71.36	
3704 WALNUT DR	70.00	68.80	71.36	
3705 WALNUT DR	70.00	68.80	71.36	
3707 WALNUT DR	70.00	68.80	71.36	
3709 WALNUT DR	70.00	68.80	71.36	
3801 WALNUT DR	70.00	68.80	71.36	
3802 WALNUT DR	70.97	68.80	71.36	
3803 WALNUT DR	70.00	68.80	71.36	
104 WESTHAVEN RD	70.00	68.80	71.36	
105 WESTHAVEN RD	70.18	68.80	71.36	
107 WESTHAVEN RD	70.00	68.80	71.36	
109 WESTHAVEN RD	70.00	68.80	71.36	
111 WESTHAVEN RD	68.75	68.80	71.36	
113 WESTHAVEN RD	70.00	68.80	71.36	
200 WESTHAVEN RD	70.00	68.80	71.36	
201 WESTHAVEN RD	70.00	68.80	71.36	
202 WESTHAVEN RD	70.00	68.80	71.36	
203 WESTHAVEN RD	70.00	68.80	71.36	
205 WESTHAVEN RD	70.00	68.80	71.36	
206 WESTHAVEN RD	70.00	68.80	71.36	
206 WESTHAVEN RD	70.00	68.80	71.36	
207 WESTHAVEN RD	70.00	68.80	71.36	
208 WESTHAVEN RD	70.00	68.80	71.36	
209 WESTHAVEN RD	70.00	68.80	71.36	
210 WESTHAVEN RD	70.00	68.80	71.36	
211 WESTHAVEN RD	70.00	68.80	71.36	
212 WESTHAVEN RD	70.00	68.80	71.36	
300 WESTHAVEN RD	70.00	68.80	71.36	

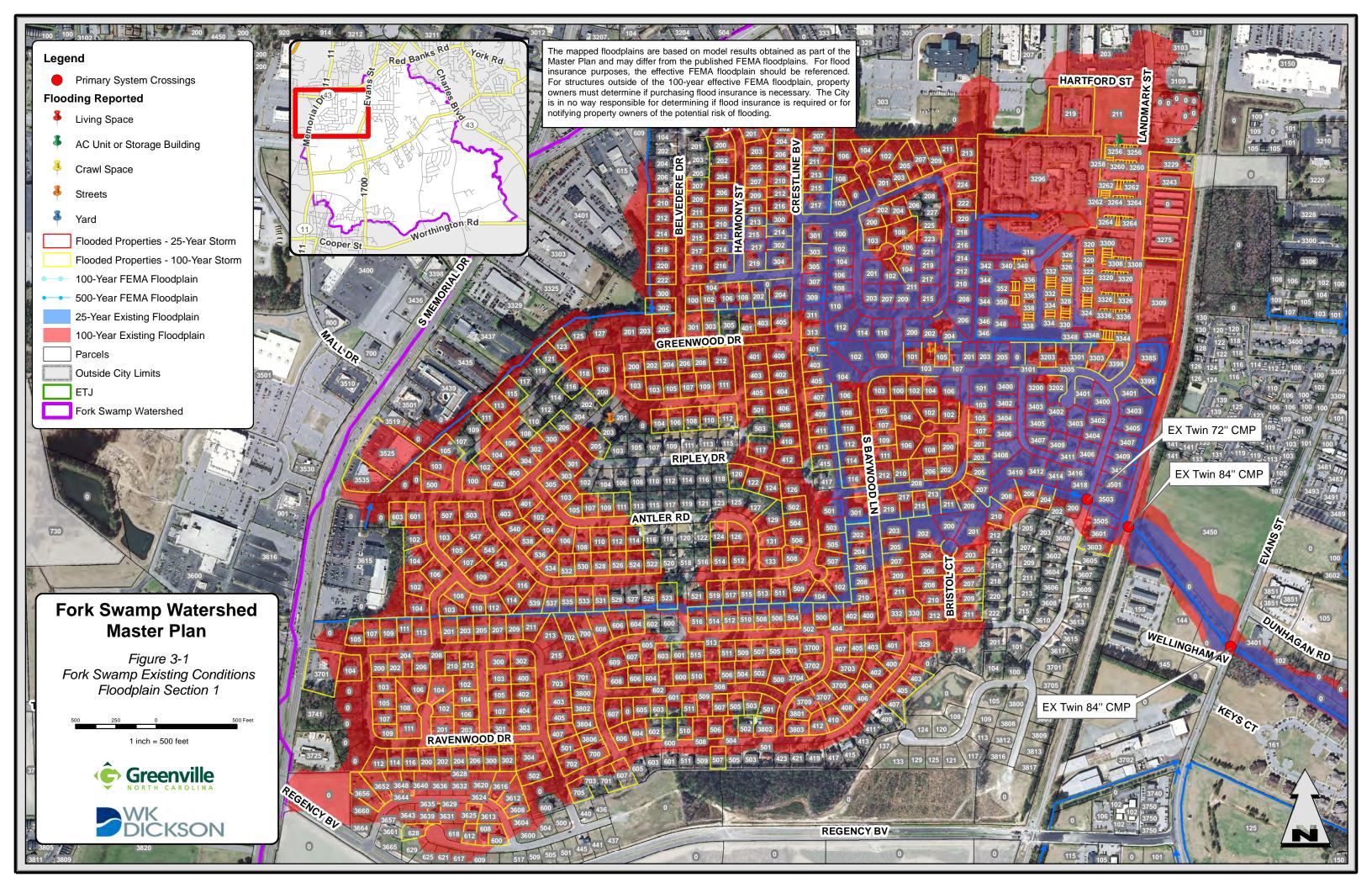
		LAG	Calculated Water Surface Elevations (feet NAVD)	
	Address	(feet NAVD)	25-year flood	100-year flood
302	WESTHAVEN RD	70.00	68.80	71.36
400	WESTHAVEN RD	70.00	68.80	71.36
402	WESTHAVEN RD	70.00	68.80	71.36
403	WESTHAVEN RD	70.00	68.80	71.36
404	WESTHAVEN RD	70.00	68.80	71.36
405	WESTHAVEN RD	70.00	68.80	71.36
407	WESTHAVEN RD	70.00	68.80	71.36
501	WESTHAVEN RD	70.00	68.80	71.36
502	WESTHAVEN RD	70.00	68.80	71.36
500	WINSTEAD RD	70.00	68.80	71.36
501	WINSTEAD RD	70.46	68.80	71.36
502	WINSTEAD RD	70.00	68.80	71.36
503	WINSTEAD RD	70.69	68.80	71.36
504	WINSTEAD RD	70.00	68.80	71.36
505	WINSTEAD RD	70.69	68.80	71.36
506	WINSTEAD RD	70.00	68.80	71.36
507	WINSTEAD RD	70.00	68.80	71.36
508	WINSTEAD RD	70.00	68.80	71.36
509	WINSTEAD RD	70.00	68.80	71.36
510	WINSTEAD RD	70.00	68.80	71.36
511	WINSTEAD RD	70.34	68.80	71.36
600	WINSTEAD RD	70.00	68.80	71.36
601	WINSTEAD RD	70.05	68.80	71.36
602	WINSTEAD RD	70.00	68.80	71.36
603	WINSTEAD RD	70.05	68.80	71.36
604	WINSTEAD RD	70.00	68.80	71.36
605	WINSTEAD RD	70.01	68.80	71.36
606	WINSTEAD RD	70.00	68.80	71.36
607	WINSTEAD RD	69.66	68.80	71.36
608	WINSTEAD RD	70.00	68.80	71.36
868	WINTERFIELD DR	50.62	50.19	51.16
874	WINTERFIELD DR	50.62	50.25	51.22
882	WINTERFIELD DR	50.97	50.37	51.34
888	WINTERFIELD DR	50.97	50.37	51.34
101	WOODHAVEN RD	68.00	68.80	71.36
102	WOODHAVEN RD	69.64	68.80	71.36
102	WOODHAVEN CT	70.00	68.80	71.36
103	WOODHAVEN RD	68.00	68.80	71.36
104	WOODHAVEN CT	70.00	68.80	71.36

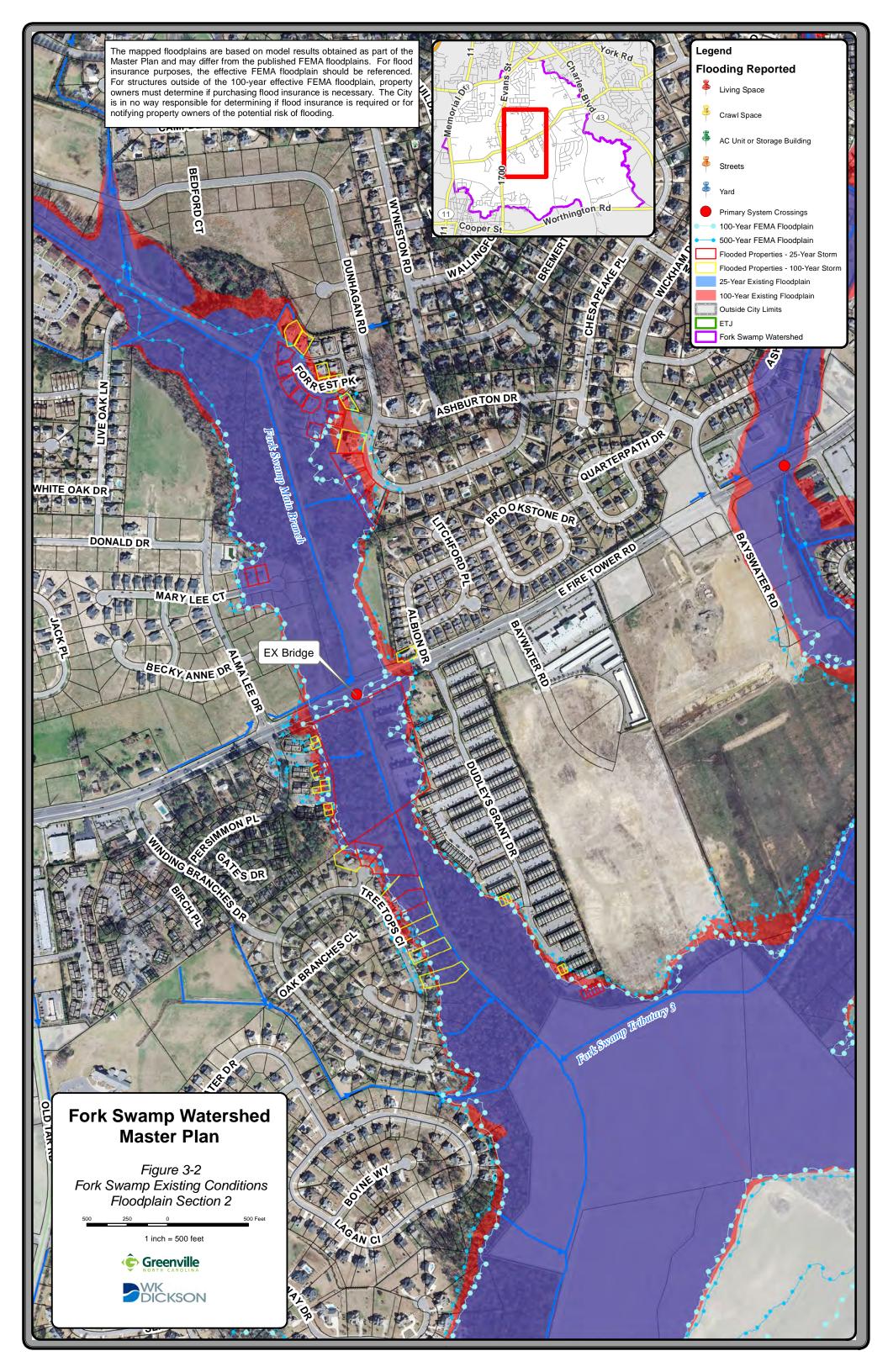
		LAG	Calculated Water Surface	ce Elevations (feet NAVD)
	Address	(feet NAVD)	25-year flood	100-year flood
105	WOODHAVEN RD	69.49	68.80	71.36
106	WOODHAVEN CT	70.00	68.80	71.36
107	WOODHAVEN RD	70.00	68.80	71.36
108	WOODHAVEN CT	70.00	68.80	71.36
200	WOODHAVEN RD	70.00	68.80	71.36
201	WOODHAVEN RD	70.00	68.80	71.36
202	WOODHAVEN RD	70.00	68.80	71.36
203	WOODHAVEN RD	69.69	68.80	71.36
205	WOODHAVEN RD	69.69	68.80	71.36
206	WOODHAVEN RD	70.00	68.80	71.36
207	WOODHAVEN RD	69.49	68.80	71.36
208	WOODHAVEN RD	70.00	68.80	71.36
210	WOODHAVEN RD	70.00	68.80	71.36
211	WOODHAVEN RD	70.00	68.80	71.36
212	WOODHAVEN RD	70.00	68.80	71.36
213	WOODHAVEN RD	70.00	68.80	71.36
215	WOODHAVEN RD	70.00	68.80	71.36
217	WOODHAVEN RD	70.00	68.80	71.36
219	WOODHAVEN RD	70.00	68.80	71.36
301	WOODHAVEN RD	68.00	68.80	71.36
100	WOODSTOCK DR	68.00	68.80	71.36
102	WOODSTOCK DR	68.00	68.80	71.36
103	WOODSTOCK DR	68.82	68.80	71.36
104	WOODSTOCK DR	68.00	68.80	71.36
106	WOODSTOCK DR	68.00	68.80	71.36
108	WOODSTOCK DR	68.00	68.80	71.36
110	WOODSTOCK DR	68.00	68.80	71.36
112	WOODSTOCK DR	68.00	68.80	71.36
114	WOODSTOCK DR	64.00	68.80	71.36
116	WOODSTOCK DR	64.00	68.80	71.36
200	WOODSTOCK DR	66.38	68.80	71.36
202	WOODSTOCK DR	66.38	68.80	71.36
203	WOODSTOCK DR	67.31	68.80	71.36
204	WOODSTOCK DR	68.84	68.80	71.36
206	WOODSTOCK DR	68.00	68.80	71.36
207	WOODSTOCK DR	67.74	68.80	71.36
208	WOODSTOCK DR	68.00	68.80	71.36
209	WOODSTOCK DR	67.74	68.80	71.36
210	WOODSTOCK DR	68.00	68.80	71.36

	LAG	Calculated Water Surface Elevations (feet NAVD)	
Address	(feet NAVD)	25-year flood	100-year flood
211 WOODSTOCK DR	68.00	68.80	71.36
212 WOODSTOCK DR	68.00	68.80	71.36
214 WOODSTOCK DR	68.00	68.80	71.36
215 WOODSTOCK DR	68.00	68.80	71.36
216 WOODSTOCK DR	68.00	68.80	71.36
217 WOODSTOCK DR	68.11	68.80	71.36
218 WOODSTOCK DR	68.00	68.80	71.36
219 WOODSTOCK DR	68.71	68.80	71.36
220 WOODSTOCK DR	70.00	68.80	71.36
221 WOODSTOCK DR	68.71	68.80	71.36
222 WOODSTOCK DR	70.00	68.80	71.36
223 WOODSTOCK DR	70.00	68.80	71.36
224 WOODSTOCK DR	70.00	68.80	71.36

^{*}Bold text indicates LAG flooding.

As shown in Table 3-4, 165 properties along Fork Swamp were identified for being at risk of flooding in the 25-year storm event and an additional 704 properties were identified for the 100-year event. There were several residents that provided feedback indicating that they are experiencing yard and AC/storage building flooding along Fork Swamp.





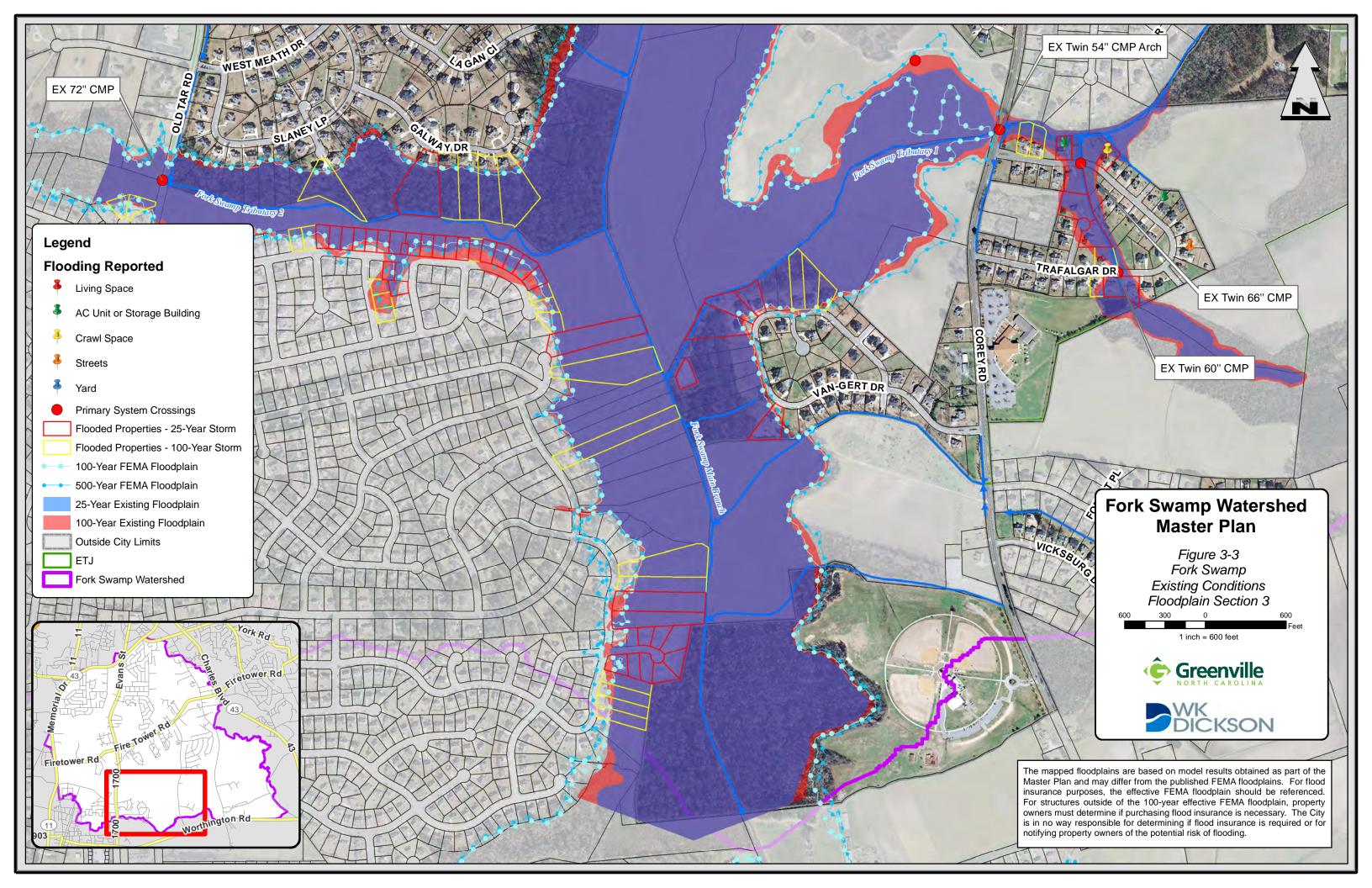


Table 3-5: Existing Conditions At-Risk Properties/Structures – FSUT1

Address	LAG (fact NAVD)	Calculated Water Surface Elevations (feet NAVD)	
	(feet NAVD)	25-year flood	100-year flood
1203 TRAFALGAR DR	55.30	54.70	55.78
1205 TRAFALGAR DR	54.84	54.79	55.86
1209 TRAFALGAR DR	52.98	55.10	55.90
1210 TRAFALGAR DR	54.40	55.25	55.96
1214 TRAFALGAR DR	55.80	55.14	55.99
1215 TRAFALGAR DR	52.55	55.14	55.93
1404 TRAFALGAR DR	54.25	55.38	56.16
1405 TRAFALGAR DR	54.17	56.36	56.76
1407 TRAFALGAR DR	55.86	56.33	56.71
1409 TRAFALGAR DR	55.86	56.29	56.70
4800 TREVVETT CI	54.00	55.30	56.01
4801 TREVVETT CI	54.82	55.36	56.08
812 VAN GERT DR	51.56	53.47	54.62
816 VAN GERT DR	50.51	53.47	54.62
820 VAN GERT DR	50.51	53.46	54.61

^{*}Bold text indicates LAG flooding.

As shown in Table 3-5, twelve (12) properties along FSUT1 were identified for being at risk of flooding in the 25-year storm event and an additional three (3) properties were identified for the 100-year event. Residents along this stream reach have provided feedback indicating that they are experiencing yard, crawl space and AC/storage building flooding.

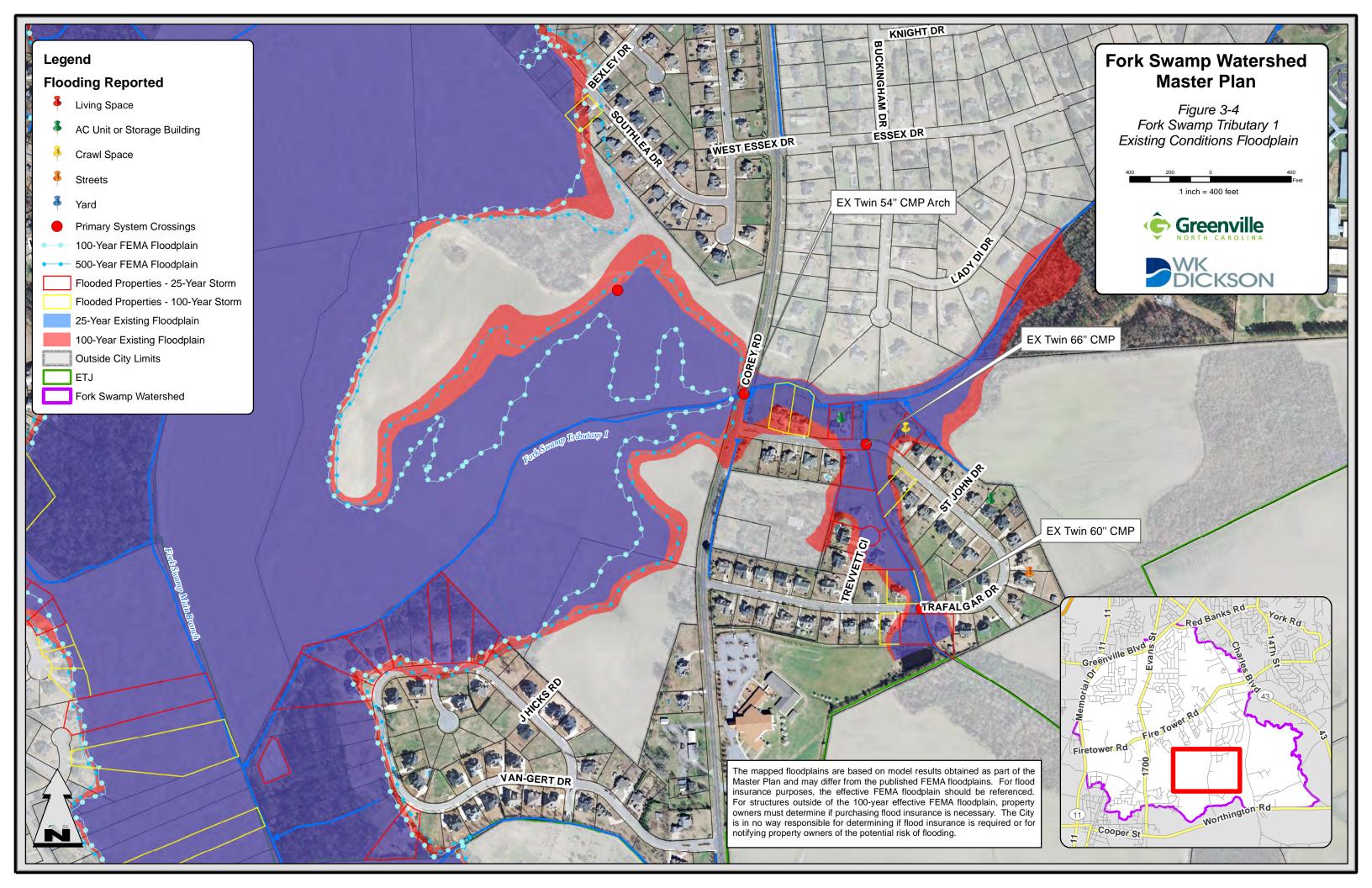


Table 3-6: Existing Conditions At-Risk Properties/Structures – FSUT2 R1

Address	LAG (feet NAVD)	Calculated Water Surface Elevations (feet NAVD)	
		25-year flood	100-year flood
595 CEDAR RIDGE DR	53.45	54.41	55.44
603 CEDAR RIDGE DR	53.38	54.43	55.40
611 CEDAR RIDGE DR	52.50	54.36	55.36
619 CEDAR RIDGE DR	52.50	54.33	55.35
623 CEDAR RIDGE DR	52.05	54.28	55.30
631 CEDAR RIDGE DR	52.05	54.23	55.26
639 CEDAR RIDGE DR	51.71	54.18	55.23
647 CEDAR RIDGE DR	53.51	54.10	55.17
650 CEDAR RIDGE DR	54.00	54.06	55.14
657 CEDAR RIDGE DR	53.51	54.05	55.14
675 CEDAR RIDGE DR	53.10	53.90	55.03
681 CEDAR RIDGE DR	52.90	53.85	54.99
689 CEDAR RIDGE DR	52.80	53.82	54.98
697 CEDAR RIDGE DR	53.40	53.78	54.95
705 CEDAR RIDGE DR	53.60	53.76	54.92
711 CEDAR RIDGE DR	53.20	53.73	54.90
719 CEDAR RIDGE DR	52.25	53.71	54.88
725 CEDAR RIDGE DR	52.25	53.69	54.87
731 CEDAR RIDGE DR	53.17	53.67	54.85
4410 DONEGAL CT	54.30	54.42	55.41
4442 GALWAY DR	53.26	53.93	55.05
4448 GALWAY DR	53.68	53.67	55.00
4454 GALWAY DR	53.86	53.85	54.95
4460 GALWAY DR	54.10	53.74	54.91
4466 GALWAY DR	53.50	53.70	54.89
2116 HAWKS NEST LN	54.00	54.05	55.13
650 MILTON DR	56.60	56.59	56.92
651 MILTON DR	56.90	56.90	56.97
2121 NORTH STAR LN	54.40	54.11	55.18
2129 NORTH STAR LN	54.47	54.08	55.15
2137 NORTH STAR LN	55.00	54.05	55.14
CEDAR RIDGE DR PUMP STATION	52.30	54.00	55.10

^{*}Bold text indicates LAG flooding.

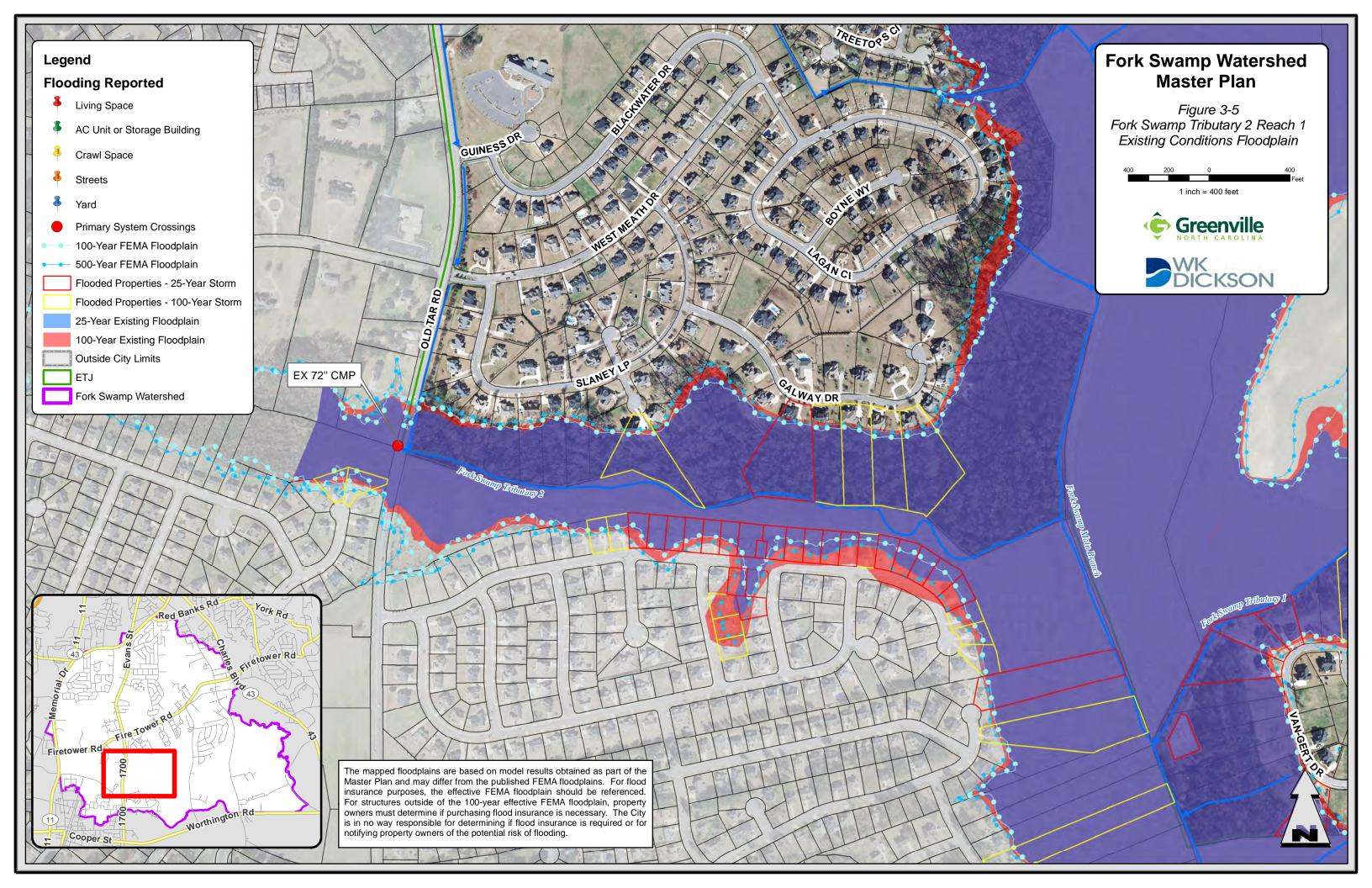
As shown in Table 3-6, twenty-five (25) properties along FSUT2R1 were identified for being at risk of flooding in the 25-year storm event and an additional seven (7) properties were identified for the 100-year event. There were no reports of flooding received from residents along this stream reach.

Table 3-7: Existing Conditions At-Risk Properties/Structures – FSUT2 R2

Address	LAG	Calculated Water Surface Elevations (feet NAVD)	
	(feet NAVD)	25-year flood	100-year flood
505 HILLSHADE CT , UNIT B	71.33	71.98	72.23
505 HILLSHADE CT , UNIT A	71.82	71.98	72.23
509 HILLSHADE CT , UNIT B	71.33	71.98	72.23
509 HILLSHADE CT , UNIT A	71.33	71.98	72.23
3901 SEDONA DR , UNIT B	70.22	71.98	72.23
3901 SEDONA DR , UNIT A	70.22	71.98	72.23
3905 SEDONA DR , UNIT B	71.82	71.97	72.22
3905 SEDONA DR , UNIT A	70.22	71.98	72.23
3909 SEDONA DR , UNIT A	71.82	71.70	72.16
3909 SEDONA DR , UNIT B	71.82	71.70	72.06
205 SOUTH POINTE DR , UNIT A	70.00	71.98	72.24
208 SOUTH POINTE DR , UNIT B	70.22	71.98	72.23
208 SOUTH POINTE DR , UNIT A	70.22	71.98	72.23
209 SOUTH POINTE DR , UNIT A	70.00	71.98	72.24
209 SOUTH POINTE DR , UNIT B	70.00	71.98	72.24
213 SOUTH POINTE DR , UNIT A	70.00	71.98	72.24
213 SOUTH POINTE DR , UNIT B	70.00	71.98	72.24
217 SOUTH POINTE DR , UNIT A	70.00	71.98	72.24
217 SOUTH POINTE DR , UNIT B	70.00	71.98	72.24
220 SOUTH POINTE DR , UNIT B	70.39	71.98	72.23
220 SOUTH POINTE DR , UNIT A	70.39	71.98	72.23
221 SOUTH POINTE DR , UNIT A	70.00	71.98	72.24
221 SOUTH POINTE DR , UNIT B	70.00	71.98	72.24
305 SOUTH POINTE DR , UNIT A	70.00	71.97	72.23
305 SOUTH POINTE DR , UNIT B	70.00	71.97	72.23
341 SOUTH POINTE DR , UNIT B	72.00	71.88	72.13
341 SOUTH POINTE DR , UNIT A	72.00	71.92	72.16
401 SOUTH POINTE DR , UNIT B	72.00	71.79	72.04
401 SOUTH POINTE DR , UNIT A	72.00	71.81	72.06

^{*}Bold text indicates LAG flooding.

As shown in Table 3-7, twenty-three (23) properties along FSUT2R2 were identified for being at risk of flooding in the 25-year storm event and an additional six (6) properties were identified for the 100-year event. There were no reports of flooding received from residents along this stream reach.



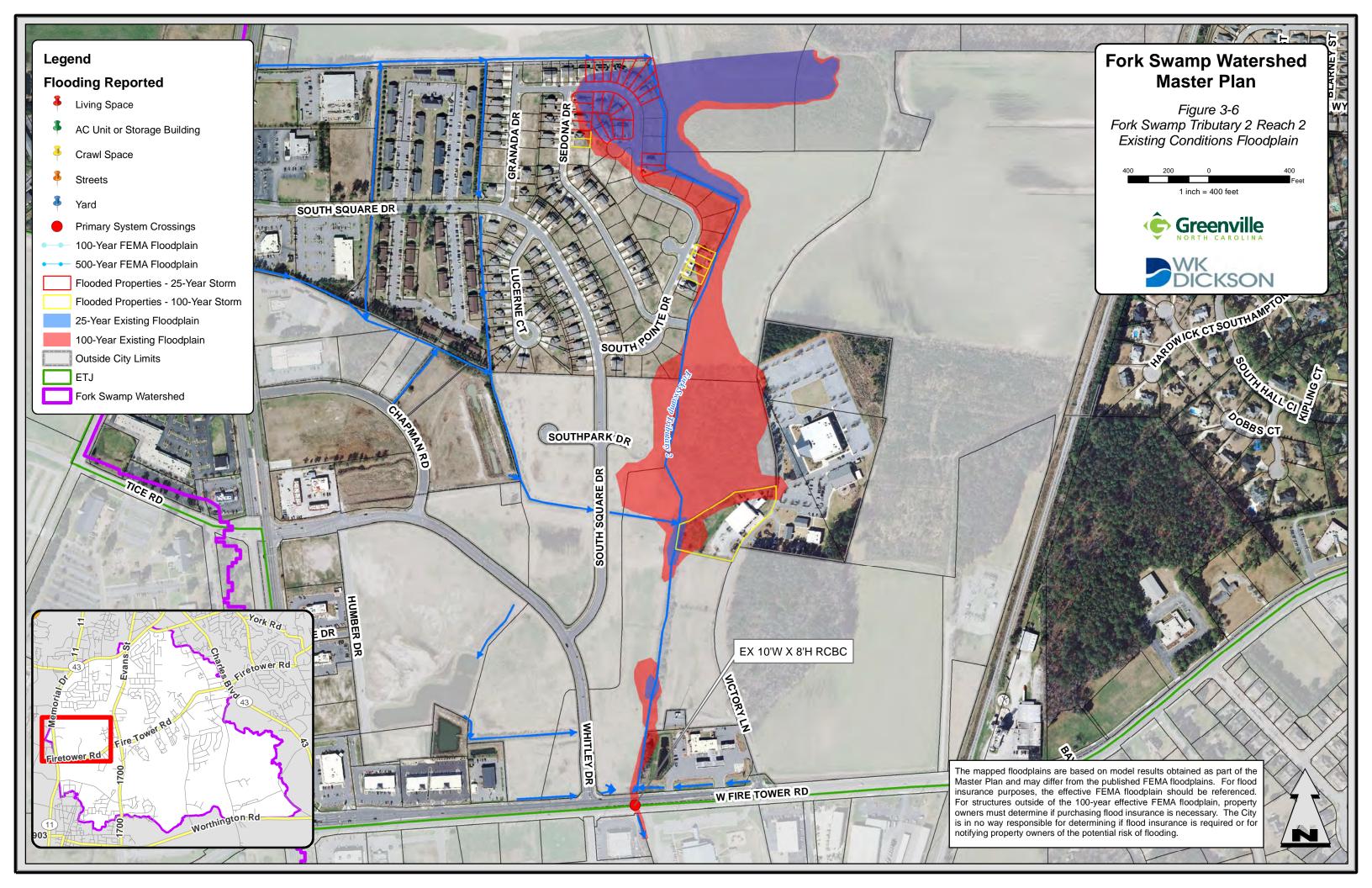


Table 3-8: Existing Conditions At-Risk Properties/Structures – FSUT3

	LAG	Calculated Water Surface Elevations	
Address	(feet NAVD)	(feet NAVD)	
	(ICCLIVAVD)	25-year flood	100-year flood
1303 ANGELS END, UNIT A	62.00	62.61	63.12
1303 ANGELS END, UNIT B	62.50	62.59	63.08
1305 ANGELS END, UNIT A	62.50	62.54	63.01
1305 ANGELS END, UNIT B	62.61	62.53	63.01
1402 ANGELS END, UNIT A	62.00	63.36	63.69
1402 ANGELS END, UNIT B	62.11	63.33	63.64
1404 ANGELS END, UNIT A	62.00	63.38	63.73
1404 ANGELS END, UNIT B	62.00	63.38	63.73
1406 ANGELS END, UNIT A	62.04	63.39	63.74
1409 ANGELS END, UNIT B	62.04	63.37	63.79
1409 ANGELS END, UNIT A	63.66	63.36	63.78
1903 ARLINGTON PARK DR	64.72	66.29	66.87
1907 ARLINGTON PARK DR	66.20	66.31	66.88
1911 ARLINGTON PARK DR	66.80	66.16	66.88
1915 ARLINGTON PARK DR	66.80	66.18	66.89
3709 ASHCROFT DR	60.00	61.45	62.19
3713 ASHCROFT DR	60.70	61.34	62.07
3717 ASHCROFT DR	59.73	61.28	62.01
3721 ASHCROFT DR	59.73	61.17	61.90
3725 ASHCROFT DR	58.29	61.06	61.79
3729 ASHCROFT DR	58.29	60.96	61.68
3733 ASHCROFT DR	60.03	60.86	61.57
3805 ASHCROFT DR	60.03	60.82	61.52
3901 ASHCROFT DR	59.22	60.66	61.32
3905 ASHCROFT DR	59.22	60.57	61.22
3909 ASHCROFT DR	58.00	60.53	61.17
3913 ASHCROFT DR	58.00	60.47	61.10
3916 ASHCROFT DR	59.79	59.70	61.13
3920 ASHCROFT DR	59.79	60.43	61.04
3921 ASHCROFT DR	56.51	60.41	61.01
3925 ASHCROFT DR	58.84	60.35	60.94
3928 ASHCROFT DR	58.84	60.38	60.97
3929 ASHCROFT DR	58.84	60.33	60.90
3933 ASHCROFT DR	58.48	60.26	60.81
3936 ASHCROFT DR	60.52	60.37	60.92
3937 ASHCROFT DR	59.70	60.25	60.79
4100 BRIDGE CT, UNIT A	58.02	59.09	59.98

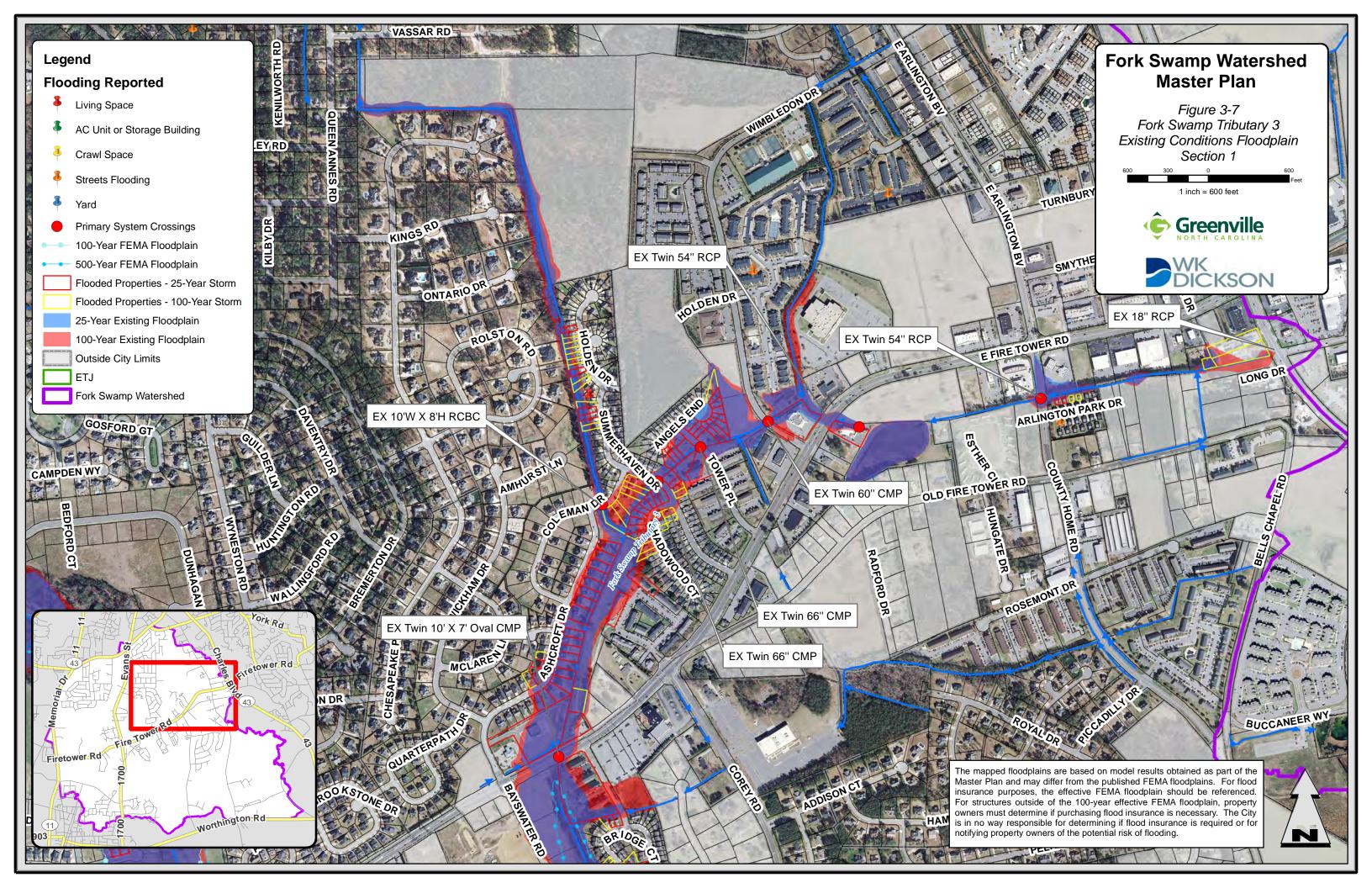
Address	LAG (feet NAVD)	Calculated Water Surface Elevations (feet NAVD)	
		25-year flood	100-year flood
4100 BRIDGE CT, UNIT B	58.02	59.09	59.98
4107 BRIDGE CT	58.00	58.00	59.38
4109 BRIDGE CT	58.00	58.39	59.30
4110 BRIDGE CT, UNIT A	58.50	58.49	59.44
4110 BRIDGE CT, UNIT B	59.50	58.60	59.51
4112 BRIDGE CT	58.00	58.00	59.38
4114 BRIDGE CT	58.00	58.42	59.33
4116 BRIDGE CT	54.00	58.27	59.21
4118 BRIDGE CT, UNIT B	56.21	58.14	59.10
4118 BRIDGE CT, UNIT A	56.21	58.11	59.07
4120 BRIDGE CT, UNIT B	56.21	58.14	59.11
4120 BRIDGE CT, UNIT A	56.21	58.11	59.07
4122 BRIDGE CT	57.60	57.00	59.04
3730 CHARLES BV	69.00	70.17	70.84
3740 CHARLES BV	70.50	70.53	71.06
2001 COLEMAN DR, UNIT A	62.00	62.00	62.79
2001 COLEMAN DR, UNIT B	62.00	62.00	62.79
2003 COLEMAN DR, UNIT A	62.00	61.90	62.73
2003 COLEMAN DR, UNIT B	60.96	61.90	62.66
2005 COLEMAN DR, UNIT A	62.00	61.70	62.53
2005 COLEMAN DR, UNIT B	62.00	61.70	62.54
915 E FIRE TOWER RD	60.16	60.20	60.72
1011 E FIRE TOWER RD	63.80	60.30	63.81
1025 E FIRE TOWER RD	60.19	60.22	60.76
1209 E FIRE TOWER RD	60.75	61.03	61.76
1213 E FIRE TOWER RD	60.50	61.20	61.93
1604 E FIRE TOWER RD	64.04	64.97	65.33
1605 E FIRE TOWER RD	64.00	64.28	64.48
2050 E FIRE TOWER RD	68.00	68.00	68.79
1110 HOLDEN DR, UNIT A	62.00	63.04	64.27
1112 HOLDEN DR, UNIT B	63.90	62.95	64.21
1112 HOLDEN DR, UNIT A	64.10	62.95	64.17
1114 HOLDEN DR, UNIT B	64.00	62.90	64.12
1114 HOLDEN DR, UNIT A	63.73	62.80	64.08
1200 HOLDEN DR, UNIT B	63.73	62.80	64.02
1200 HOLDEN DR, UNIT A	63.73	62.70	63.98
1202 HOLDEN DR, UNIT A	60.00	62.75	63.90
1202 HOLDEN DR, UNIT B	63.73	62.70	63.94

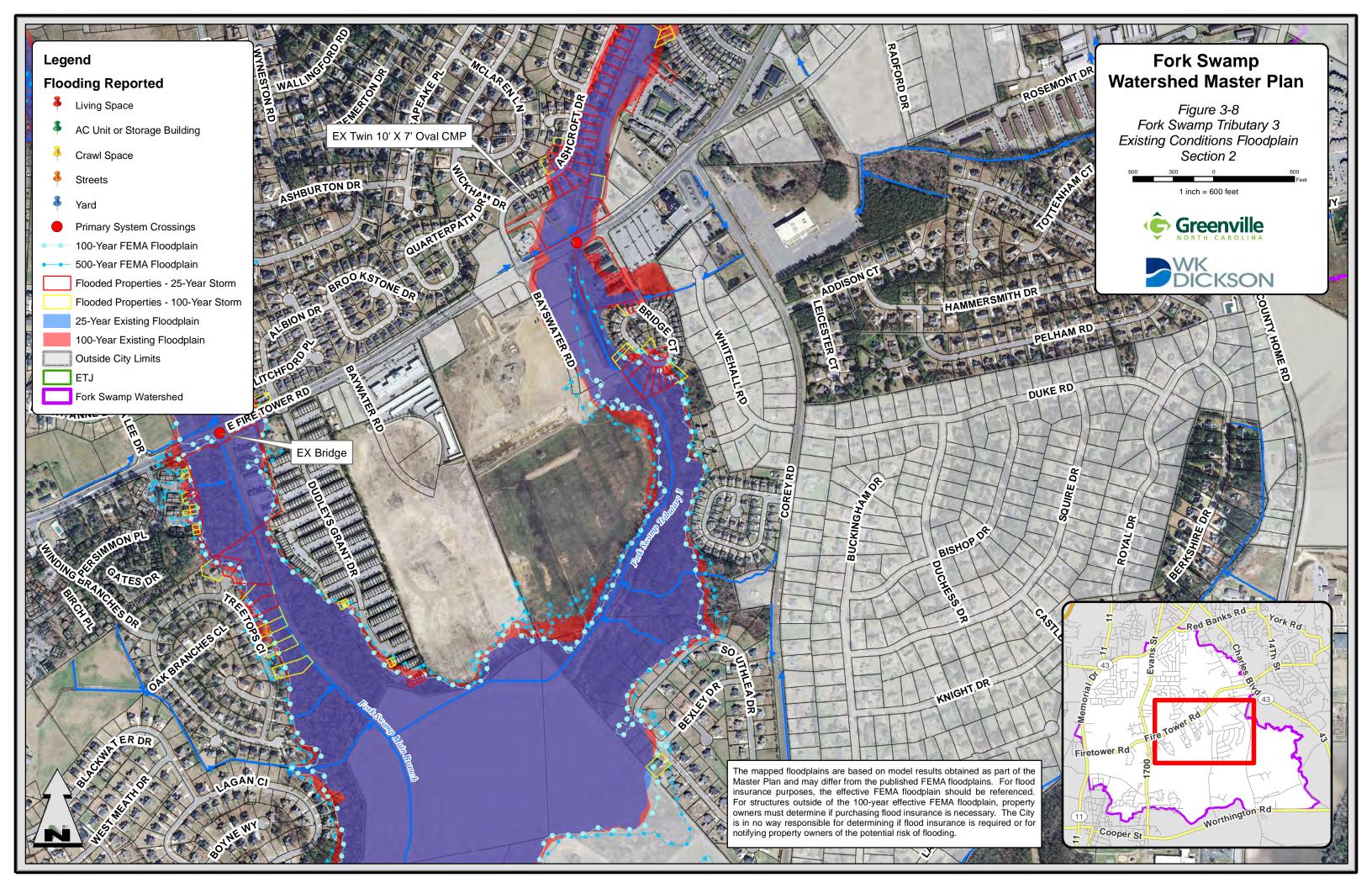
Address	LAG (feet NAVD)	Calculated Water Surface Elevations (feet NAVD)	
		25-year flood	100-year flood
1204 HOLDEN DR, UNIT B	60.00	60.00	63.86
1204 HOLDEN DR, UNIT A	60.00	60.00	63.82
2000 SHADOWOOD CT, UNIT B	61.17	62.09	62.82
2000 SHADOWOOD CT, UNIT A	61.17	62.02	62.78
2002 SHADOWOOD CT, UNIT B	60.96	61.98	62.75
2002 SHADOWOOD CT, UNIT A	60.96	61.96	62.74
2004 SHADOWOOD CT, UNIT B	60.96	61.88	62.66
2004 SHADOWOOD CT, UNIT A	60.96	61.82	62.59
2006 SHADOWOOD CT, UNIT B	60.50	61.71	62.47
2006 SHADOWOOD CT, UNIT A	60.60	61.68	62.43
2007 SHADOWOOD CT, UNIT A	62.67	61.90	62.71
2008 SHADOWOOD CT, UNIT B	62.00	61.57	62.35
2008 SHADOWOOD CT, UNIT A	62.00	61.57	62.30
2010 SHADOWOOD CT, UNIT B	61.50	61.40	62.25
2010 SHADOWOOD CT, UNIT A	61.50	61.40	62.20
4327 SOUTHLEA DR	53.30	53.00	54.52
1802 SUMMERHAVEN DR, UNIT A	63.50	62.50	63.64
1804 SUMMERHAVEN DR, UNIT B	62.00	62.49	63.56
1804 SUMMERHAVEN DR, UNIT A	61.50	62.45	63.51
1806 SUMMERHAVEN DR, UNIT B	62.50	62.45	63.50
1806 SUMMERHAVEN DR, UNIT A	62.50	62.41	63.45
1995 SUMMERHAVEN DR, UNIT B	62.39	62.50	62.94
1995 SUMMERHAVEN DR, UNIT A	62.30	62.50	62.94
1997 SUMMERHAVEN DR, UNIT A	62.39	62.30	62.95
1997 SUMMERHAVEN DR, UNIT B	62.39	62.30	62.88
2000 SUMMERHAVEN DR, UNIT B	62.00	62.00	62.76
2000 SUMMERHAVEN DR, UNIT A	62.00	62.00	62.75
2007 SUMMERHAVEN DR, UNIT B	62.50	61.80	62.59
2001 TOWER PL, UNIT B	62.11	63.22	63.54
2001 TOWER PL, UNIT A	62.44	63.11	63.47
2002 TOWER PL, UNIT B	62.00	62.68	63.21
2002 TOWER PL, UNIT A	62.00	62.68	63.21
2003 TOWER PL, UNIT B	62.00	63.28	63.57
2003 TOWER PL, UNIT A	62.00	63.14	63.49
2004 TOWER PL	60.37	62.60	63.10
4006 WHITEBRIDGE DR	58.71	59.24	60.12

^{*}Bold text indicates LAG flooding.

SECTION 3: EXISTING WATERSHED ANALYSIS

As shown in Table 3-8, eighty-one (81) properties along FSUT3 were identified for being at risk of flooding in the 25-year storm event and an additional thirty (30) properties were identified for the 100-year event. There were no reports of flooding received from residents along this stream reach.





3.2 SECONDARY SYSTEM HYDROLOGIC AND HYDRAULIC ANALYSES

While Fork Swamp and its tributaries are the primary source of flooding within the watershed, undersized systems can also lead to structural and roadway flooding. Based on the questionnaire responses, public meeting, and feedback from City staff, four (4) secondary systems were identified for further evaluation. The secondary systems evaluated are as follows:

- Trafalgar Drive Closed System;
- Corey Road Closed System;
- Lynndale System; and
- Evans Street Channels.

3.2.1 Hydrology

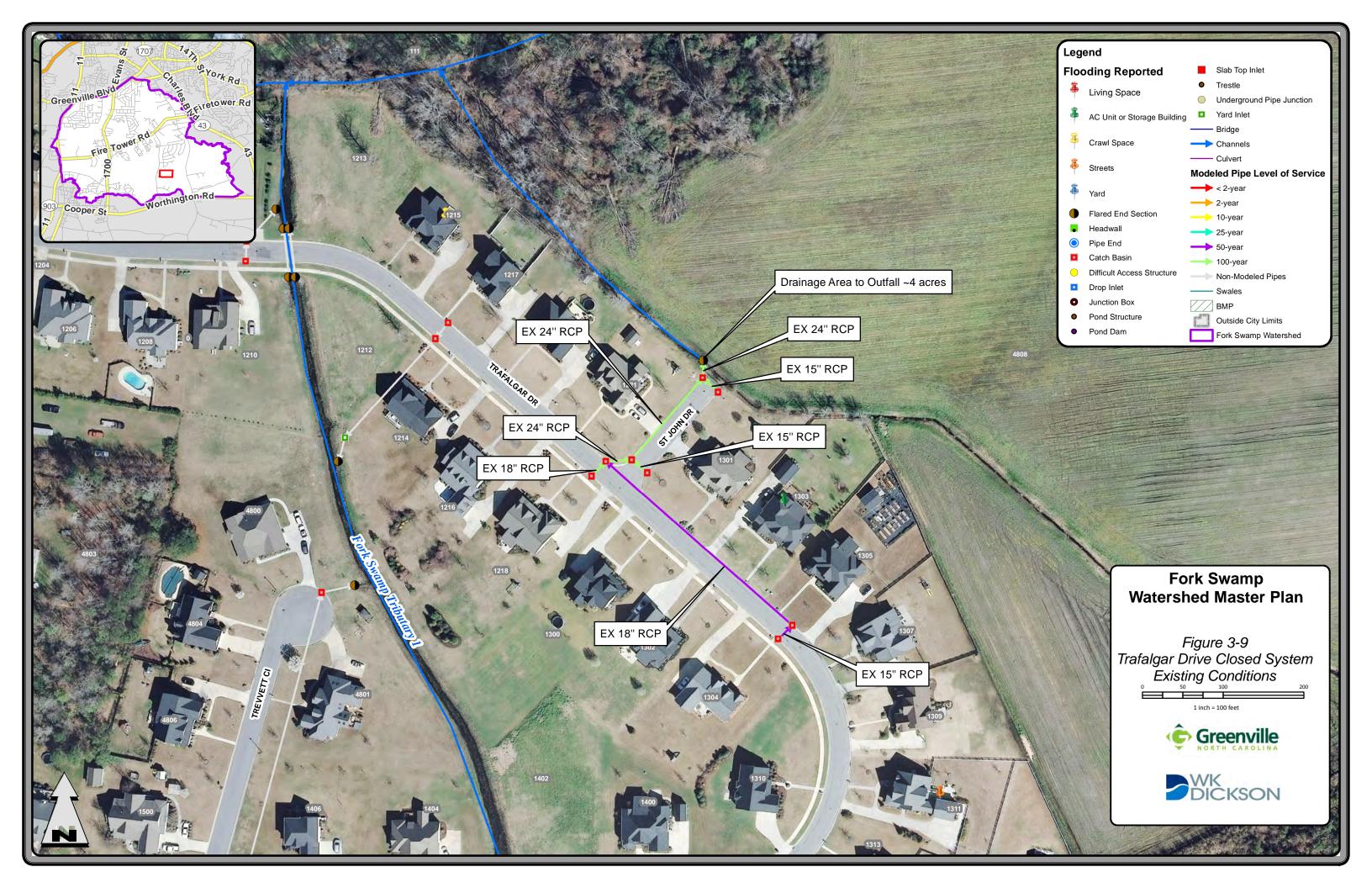
Three (3) models were used in the hydrologic evaluation of the secondary systems: HEC-HMS, EPA SWMM, and Hydraflow Storm Sewers. For the larger more complex secondary system, the Corey Road System, SWMM was selected as the hydrologic and hydraulic model. Smaller systems that were completely closed systems including Trafalgar Drive were modeled using Rational flow calculations within Hydraflow Storm Sewers. HEC-HMS was used to model the Evans Street Channels. The Lynndale System was evaluated by Rivers & Associates as a separate project, therefore modeling methodologies and parameters may not be consistent with the remaining projects within the Citywide Master Plan. A detailed description about the hydrologic modeling methodology used for they systems analyzed as part of this report is included in Appendix A.

3.2.2 Hydraulics

<u>Trafalgar Drive Closed System</u>

The Trafalgar Drive Closed System collects drainage from 4 acres in the Farrington subdivision. It discharges to a trapezoidal channel section that ultimately outlets to FSUT1. The conveyance system is comprised of RCP ranging in size from 15 to 24 inches in diameter that is in good condition based on data collected during the inventory. Flooding has historically been reported along Trafalgar Drive as noted from the City staff and public input. There is one report of flooding adjacent to this system in this area. It is a report of crawl space and AC or storage building flooding at 1303 Trafalgar Drive.

Figure 3-9 shows the level of service being provided by the existing closed system. The model results show that the existing system is operating at or above the desired 10-year level of service. Flooding appears to be related to backwater from the main stream rather than the capacity of the Trafalgar Drive conveyance system. Flooding has appeared to be less frequent and less severe since the installation of the new culverts at Corey Road.



Corey Road Closed System

The Corey Road Closed System collects drainage from approximately 60 acres in the Windsor Downs subdivision and the adjacent parcels. It discharges to a channel section the outlets directly to Fork Swamp. The conveyance system is comprised mostly of RCP ranging in size from 15 to 48 inches in diameter that is in good condition based on data collected during the inventory. Flooding has historically been reported is this area as reported by City staff and the findings in the Watershed Action Plan prepared by Baker dated October 12, 2012.

Figure 3-10 shows the level of service being provided by the existing closed system. The model results show that the majority of the existing system is operating at or above the desired 10-year level of service. There are three segments of pipe that are only meeting a 2-year level of service including the twin 36" RCPs that discharges to the outlet channel.

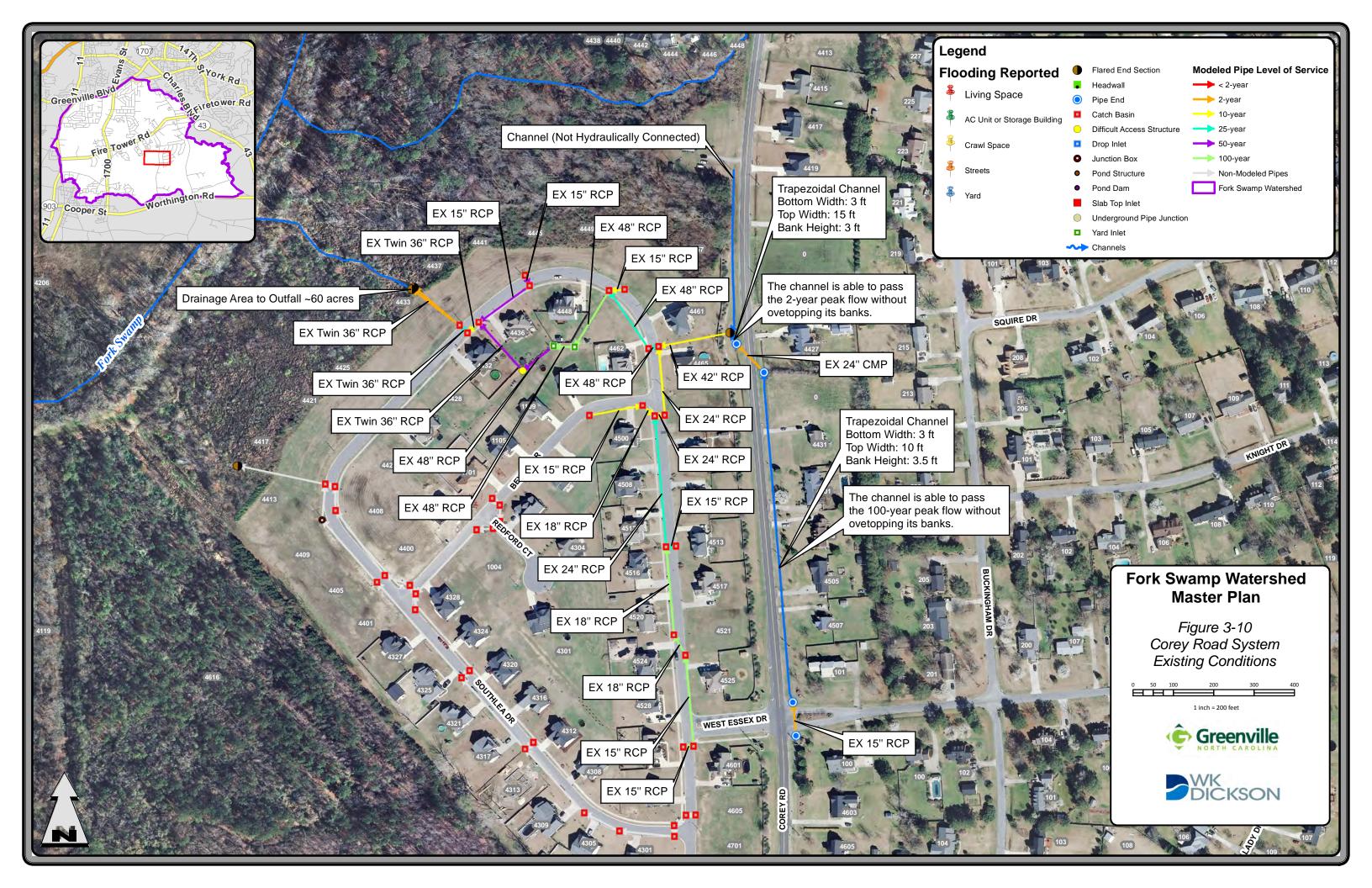
Lynndale System

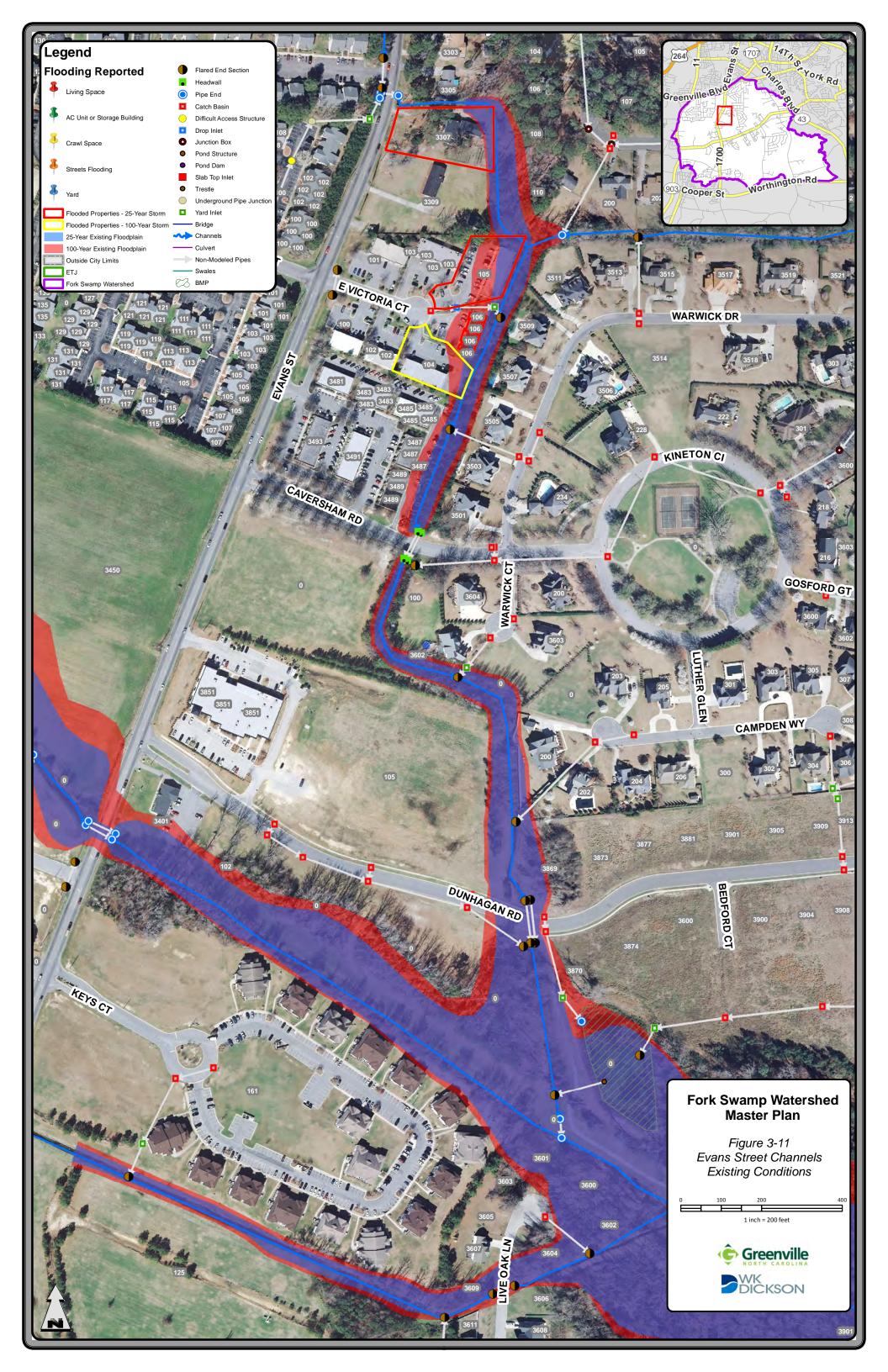
Seven (7) questionnaires were received from the residents in the Lynndale subdivision reporting yard and street flooding. Based on the feedback from residents and City staff, significant roadway flooding occurs along Fort Sumter Drive, Crown Point Road, and Martinsborough Road. A study for this area has been completed with proposed recommendations by River & Associates. The Lynndale System was not reanalyzed as part of the Fork Swamp Watershed Master Plan, although improvements proposed by Rivers & Associates are included in the Master Plan prioritization.

Evans Street Channels

The Evans Street channels are located in the northern section of the Fork Swamp watershed. The upstream segment of these analyzed channels is adjacent to a highly impervious area including an office park and high-density residential area (townhouse/condominium complex). There are no reports of flooding from property owners however, the City staff has identified this area as being severely eroded. Additionally, the resident at 3307 Evans Street has reported erosion on the property that is associated with the channel.

Figure 3-11 shows the 25- and 100- year existing conditions floodplain for the Evans Street channel sections. The model shows that there is yard and parking lot flooding expected in the 25- and 100-year storm events. The channel velocities reported from the model range between 0.2 and 3.3 feet per second in the 10-year storm event. Stream bank erosion can be a concern when channel velocities exceed 4.0 feet per second for the types of soil present in the streambed, however the velocity at which erosion can occur will vary based on the site specific soil type and vegetative cover. This stream reach was walked and evaluated by WK Dickson personnel. Based on this evaluation, a stream stabilization project was developed as part of this Master Plan. The stream stabilization project (Project #7) is outlined in Section 5.1 of this report.





3.3 STREAM STABILITY FIELD ASSESSMENTS

There are 13.4 miles of stream located in the Fork Swamp Watershed. Within the watershed, all 3.6 miles of Fork Swamp is classified for secondary recreation and aquatic wildlife survival and propagation (Class C) by NCDWR. Fork Swamp is also classified as nutrient sensitive waters (NSW) by NCDWR, indicating it is subject to excessive growth of microscopic or macroscopic vegetation, or it may contribute to downstream nutrient loading (NCDWR 2011). None of the streams in the watershed are listed on the NC Water Quality Assessment and Impaired Waters list (also known as the Integrated 305 (b) and 303 (d) Report).

Field assessments measuring bank stability were conducted on all of the major stream channels within the Fork Swamp Watershed. The Bank Erosion Hazard Index (BEHI) developed by Rosgen was used to evaluate the streams in the watershed. BEHI is an assessment tool that is used to quantify the erosion potential of a stream bank. Characteristics assessed as part of the BEHI rating include bank height ratio (stream bank height/maximum bankfull depth), ratio of rooting depth to bank height, root density, bank angle, and percent surface protection, and bank material composition. Each of these variables that affect the potential rate of stream bank erosion is assigned points based on specific evaluation criteria. BEHI scores range from five to fifty, with a score of fifty indicating the highest potential for erosion. A BEHI score of 5 to 19.5 indicates a very low or low potential for erosion; a score between 20 and 29.5 indicates a moderate potential for erosion; scores from 30 to 45 represent a high to very high potential for erosion; and scores between 46 and 50 indicate extreme erosion potential. The completed BEHI scores are provided in Appendix K.

In addition to BEHI ratings, a modified version of the channel stability assessment method (CSA) provided in "Assessing Stream Channel Stability at Bridges in Physiographic Regions" by Johnson (2006) was used to assess channel stability channels in the watershed. The CSA method was designed to evaluate stability indicators in the field. These parameters include: watershed characteristics, flow habit, channel pattern, entrenchment/channel confinement, bed material, bar development, presence of obstructions/debris jams, bank soil texture and coherence, average bank angle, bank vegetation/protection, bank cutting, and mass wasting/bank failure. The twelve (12) indicators were scored in the field, and a rating of excellent, good, fair, or poor was assigned to each project reach based on the total score. The completed CSA scores and a field datasheet are provided in Appendix K.

There are four (4) main drainage features within the Fork Swamp Watershed (See Figure 3-12). The largest of these is Fork Swamp. Three unnamed tributaries also drain to Fork Swamp. UT1 and UT3 originate in the eastern portion of the watershed before draining to Fork Swamp. UT2 originates in the western portion of the watershed before draining to Fork Swamp. BEHI scores for each of these drainage areas are discussed below.

Fourteen (14) BEHI assessments were performed along the Fork Swamp drainages. Four (4) of these assessments were performed on the main branch of Fork Swamp. Sampling points 1 and 2, the samples upstream of the confluence with UT3, had ratings of Very High. Both of these

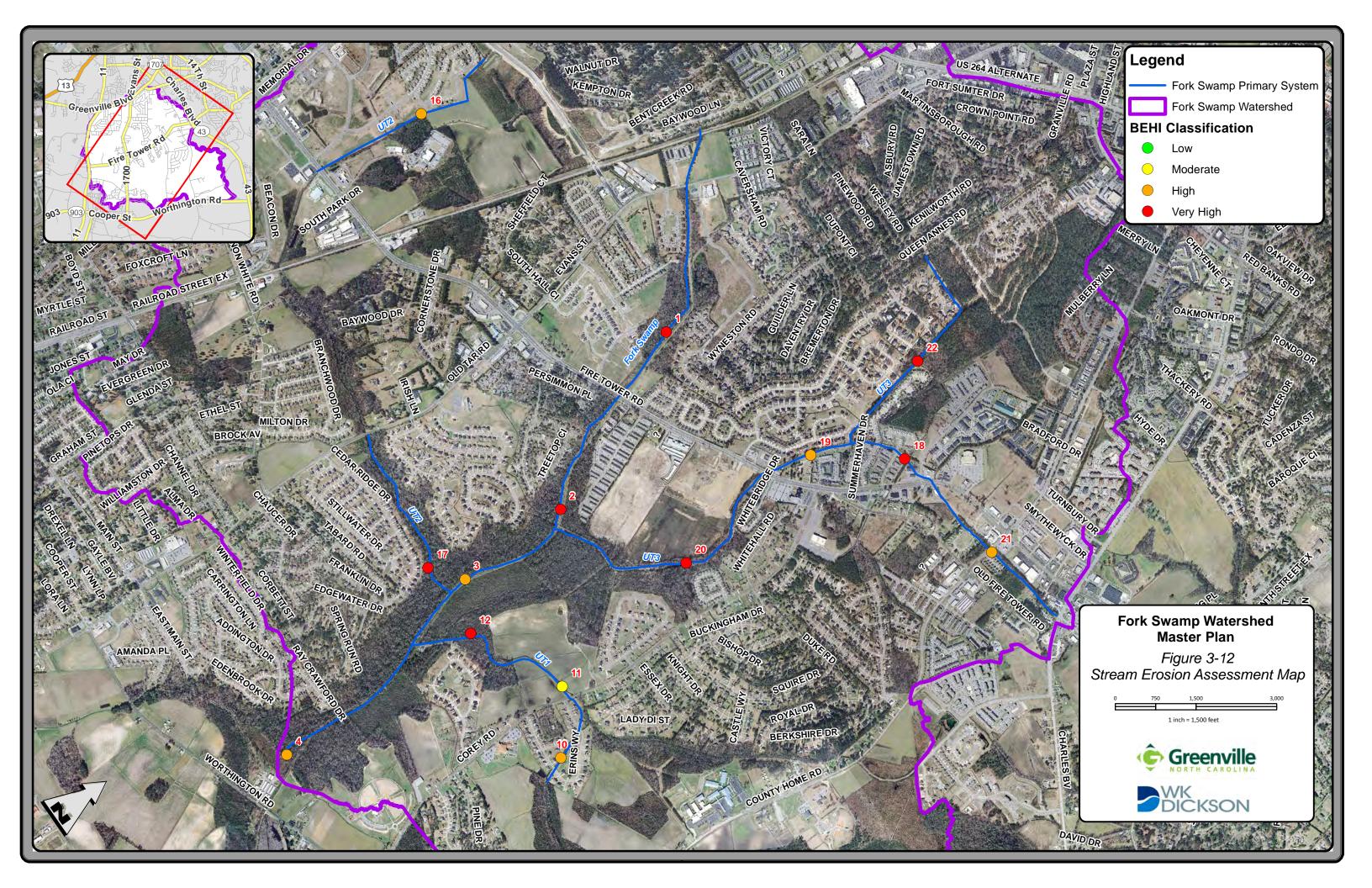
SECTION 3: EXISTING WATERSHED ANALYSIS

sampling points had bank height/bankfull ratios in the very high range. Additionally, these stream reaches had moderate to high surface protection and bank angles approaching 70 degrees. The downstream reaches of Fork Swamp (sampling points 3 and 4), had BEHI ratings of High. These samples had bank height/bankfull ratios in the low to moderate range, and very low root densities along the stream banks. Bank angles and surface protection scored in the very low range. These assessments illustrate that the main branch of Fork Swamp in the study area is primarily a sand bed channel with high potential for erosion.

Two (2) BEHI assessments were performed on UT2, one on the downstream reach (UT2-1) and one on the upstream reach (UT2-2). UT2-1 scored Very High and UT2-2 scored High on the BEHI assessment. UT2-1 is a sandbed channel with a fairly intact riparian buffer. UT2-1 scored moderate for bank height/bankfull ratios and bank angle, but in the high to very high range for root density and surface protection. UT2-2 is a sandbed channel with no little riparian buffer throughout most of the reach. UT2-2 scored near the extreme range for bank height/bankfull ratios, but scored in the low range for bank angle and surface protection.

Three (3) BEHI assessments were performed along UT1. The most downstream sampling point, point 12, is a sandbed channel with a fairly intact riparian buffer. This point scored moderate for bank height/bankfull ratios and bank angle, but in the high to very high range for root density and surface protection. The most upstream assessment, sampling point 10, scored High on the assessment. This reach is a sandbed channel that runs through a residential neighborhood and has areas of noticeable erosion encroaching on multiple landowner fences. Bank height/bankfull ratios in this neighborhood are very high, but bank angles and root density are in the low to moderate range. Sampling point 11, runs through a large tract of agricultural land and scored in the moderate range to high range. This reach had little to no riparian buffer and areas of obvious erosion. This section of UT1 is a good candidate for bank stabilization and buffer restoration, as highlighted in Section 5.1 for Stream Stabilization Project #2.

Five (5) BEHI assessments were performed along UT3, all ranging in the High to Very High range. All of these sampling points scored in the Extreme range for bank height/bankfull ratios and High for root density. All samples scored in the low to moderate range for bank angle and surface protection. UT3 is a sand bad channel that, as highlighted in Section 5-1, has many opportunities for bank stabilization, floodplain benching, and buffer enhancement/restoration. Upstream of Sample location 22, the City has recently completed a bank stabilization project with a hardened approach at a 90 degree turn in the stream. Stream Stabilization Project #6 detailed in Section 5-1 addresses additional stabilization issues just upstream of the completed City project.



FLOOD MITIGATION ALTERNATIVES

4.1 Primary Systems

Developing flood control alternatives in an urban environment is a complex process based on limitations imposed by the constraints within the environment such as floodplain encroachments, increased peak flows due to impervious areas, public and private utilities, and private property. Improvements in this portion of the study were identified through an iterative process of infrastructure improvements, increasing floodplain storage, and evaluating detention options. Alternatives were finalized based on discussions with City staff. The top alternatives that achieve the goals of the project while minimizing impacts to residents and traffic are presented.

4.1.1 FORK SWAMP

East Baywood Lane – As determined by the existing conditions analysis, the existing twin 72" CMPs at this crossing do not meet the desired 25-year level of service without overtopping. Currently, it provides a 2-year level of service and is in good condition as shown in Picture 4-1.



Picture 4-1. East Baywood Lane Culvert – Upstream Face

The hydraulic performance at East Baywood Lane is affected by the backwater from the downstream railroad crossing. With the improvements proposed downstream, the resultant 25-year water surface elevation (WSEL) is reduced by over 2 feet. However, East Baywood Lane still does not meet the required 25-year level of service and will operate at a 10-year level of service. Increasing the capacity at the crossing does not impact the WSEL since the culvert is in outlet control. Additionally, there is no room available to incorporate floodplain benching immediately

downstream of the crossing to lower the tailwater. It should be noted that no reports of flooding have been collected in the vicinity of East Baywood Lane. Therefore, no capital improvements are proposed at this location.

Railroad Crossing – The existing twin 84" CMPs at this crossing are currently operating at a 25-year level of service. In order to aid in lowering the tailwater at East Baywood Lane, floodplain benches are proposed downstream of the railroad crossing in the left overbank for approximately 770 linear feet.

Figure 4-1 shows the locations of the proposed floodplain benching. The benching will range in width between 140 and 150 feet. The proposed floodplain benching will improve the performance of the existing twin 84" CMPs and bring it up to the desired 100-year level of

service. The resulting upstream water surface elevation will be reduced by 2.07 to 2.35 feet in the 25-year storm event.

There are 121 properties located in the existing conditions 25-year floodplain upstream of the railroad crossing in the Westhaven subdivision and an additional 671 in the 100-year floodplain. If this alternative is implemented, 15 properties will be removed from the 25-year floodplain and an additional 18 properties from the 100-year floodplain. The majority of the residents will remain in the floodplain however, the severity, duration, and frequency of flooding will be reduced. Lowering the tailwater at the railroad by installing the floodplain benching is the only feasible alternative for reducing the water surface elevations in the Westhaven subdivision.

During a field inspection, there were several potential site restrictions and utility conflicts that were identified including overhead power lines that are located above Evans Street which may possibly be used as a construction entrance. These overhead power lines may need to be temporarily relocated based on where the contractor accesses the site. There also appears to be sanitary sewer lines that may need to be replaced or relocated. Impacts to traffic flow during construction were considered. The proposed project is not located in the roadway therefore anticipated impacts to traffic are minimal. In order to gain access and to install the proposed floodplain benching, minimal tree removal will be required. The installation of construction staging areas and entrances will require additional tree removal and temporary construction easements. It should be noted that the majority of the proposed improvements are located on private property therefore an easement would be required to complete this project and maintain the bench in the future. Approximately 25% of the proposed floodplain bench appears to be located within a Pitt County Drainage District easement based on the Pitt County OPIS website. Coordination with the Drainage District will be required to implement the proposed project. The floodplain benching could be coordinated with the proposed Fork Swamp Greenway referenced in the 2004 Greenway Master Plan. Economy of savings could be provided if both projects are constructed at the same time.

The total estimated cost for floodplain benching downstream of the Railroad crossing is \$1,000,000.

Evans Street – As determined by the existing conditions analysis, the twin 84" CMPs at this crossing are currently providing a 25-year level of service. Since Evans Street is classified as a major NCDOT thoroughfare, the desired level of service is the 50-year storm.

This alternative entails replacing the existing CMPs with twin 7' x 7' RCBCs coupled with floodplain benching downstream of the crossing to lower the tailwater. The floodplain benching is proposed in the left overbank for approximately 1,200 linear feet. The improvements proposed will bring Evans Street up to the desired 50-year level of service. It should be noted that NCDOT has an upcoming widening project planned for Evans Street. In order to implement the culvert improvements with this planned roadway widening project, coordination with NCDOT will be required. Depending upon the timing, another option would

be to complete this project in phases. Phase 1 would be the installation of the proposed floodplain benching followed by Phase 2, the culvert upgrades. With regards to sequencing of proposed improvements along Fork Swamp, the Evans Street floodplain benching should be completed before the Railroad Crossing improvements. This will help to further reduce the tailwater between Evans Street and the railroad. The floodplain benching could be coordinated with the proposed Fork Swamp Greenway referenced in the 2004 Greenway Master Plan. Economy of savings could be provided if both projects are constructed at the same time.

The reductions in water surface elevation will range from 2.76 to 2.95 feet in the 25-year storm event between the railroad crossing and Evans Street. There are no structures located in the existing conditions 25- and 100-year floodplain. Figure 4-1 summarizes the improvements proposed for this location. The total estimated cost for completing the culvert improvements and floodplain benching at Evans Street is \$1,920,000.

During a field inspection, there were several potential site restrictions and utility conflicts that were identified including overhead power lines that are located above the Evans Street culvert. There also appears to be sanitary sewer lines that may need to be replaced or relocated. Impacts to traffic flow during construction were considered. Evans Street is a major thoroughfare and it is anticipated that a road closure or flagged two-way one-lane operation will be required. The proposed floodplain benching is located on private property therefore an easement would be required to complete this project and maintain the bench in the future. The majority of the proposed floodplain bench appears to be located within a Pitt County Drainage District easement based on the Pitt County OPIS website. Coordination with the Drainage District will be required to implement the proposed project.

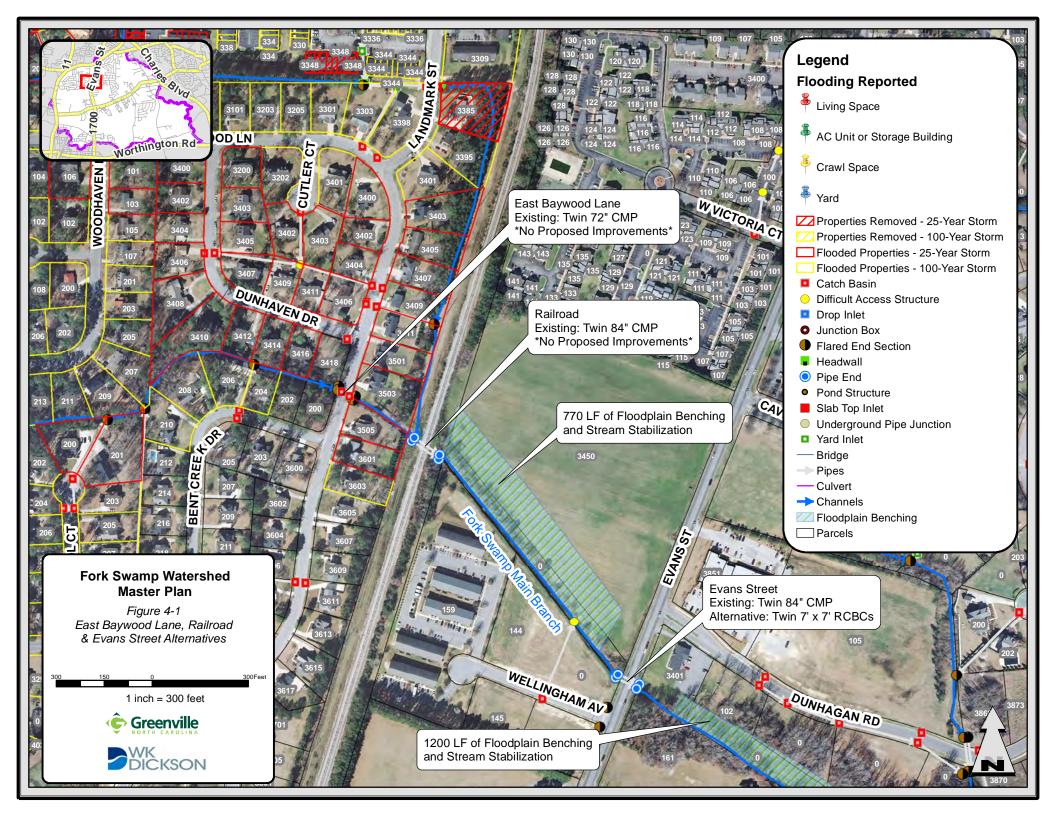
East Fire Tower Road – The existing bridge at this crossing is in good condition and currently performs at a 25-year level or service. Since East Fire Tower Road is a major thoroughfare, the desired level of service is the 50-year storm. In order to provide a 50-year level of service at this crossing, the recommended alternative is to reduce the tailwater by grading floodplain benches downstream of East Fire Tower Road.

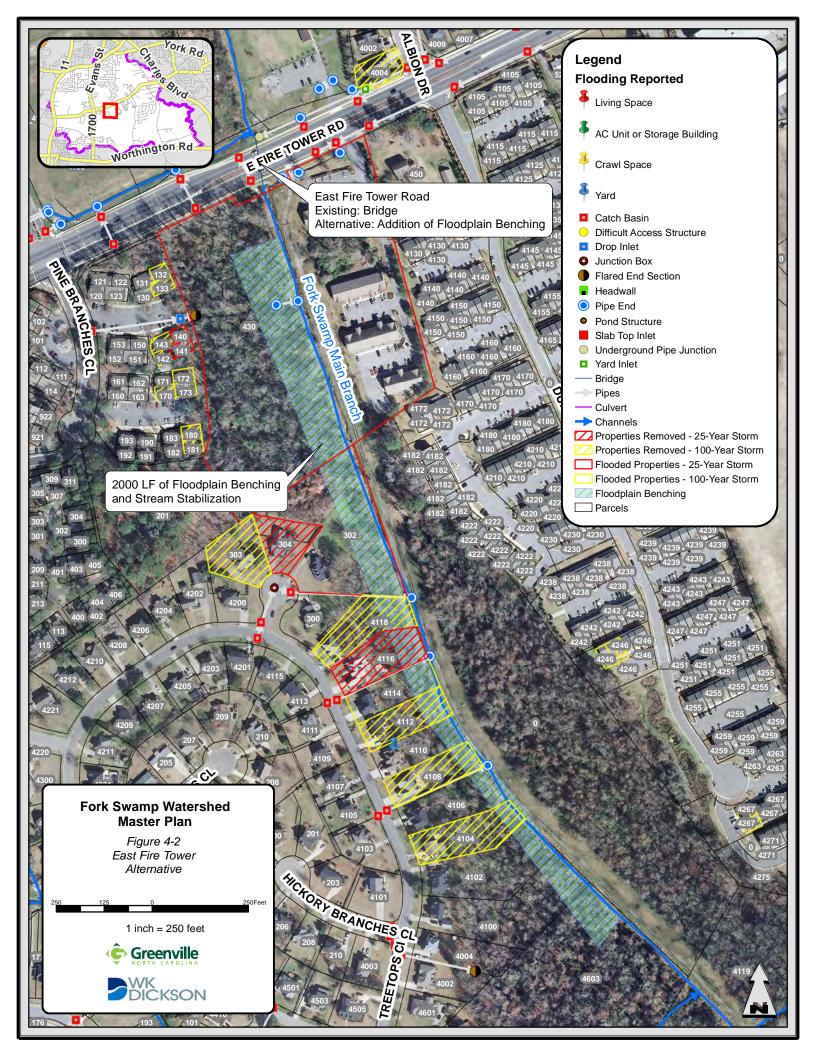
As shown in Figure 4-2, this alternative entails proposed floodplain benching in the right overbank for approximately 2,000 linear feet. The floodplain benching could be coordinated with the proposed Fork Swamp Greenway referenced in the 2004 Greenway Master Plan. Economy of savings could be provided if both projects are constructed at the same time.

The improvements proposed will bring East Fire Tower Road up to the desired 50-year level of service. The reductions in water surface elevation will range from 0.28 to 2.31 feet in the 25-year storm event downstream of East Fire Tower Road. This will provide potential flood relief to the Treetops Circle residents. There are six (6) properties in the existing conditions 25-year floodplain and sixteen (16) additional properties in the 100-year floodplain, that have potential to experience LAG or structural flooding. The water surface elevation will be reduced for all of these properties. Four (4) will be removed from the 25-year floodplain and twelve (12) from

the 100-year floodplain with the implementation of this project. The remaining properties will continue to be exposed to LAG or structural flooding, although depth will be reduced.

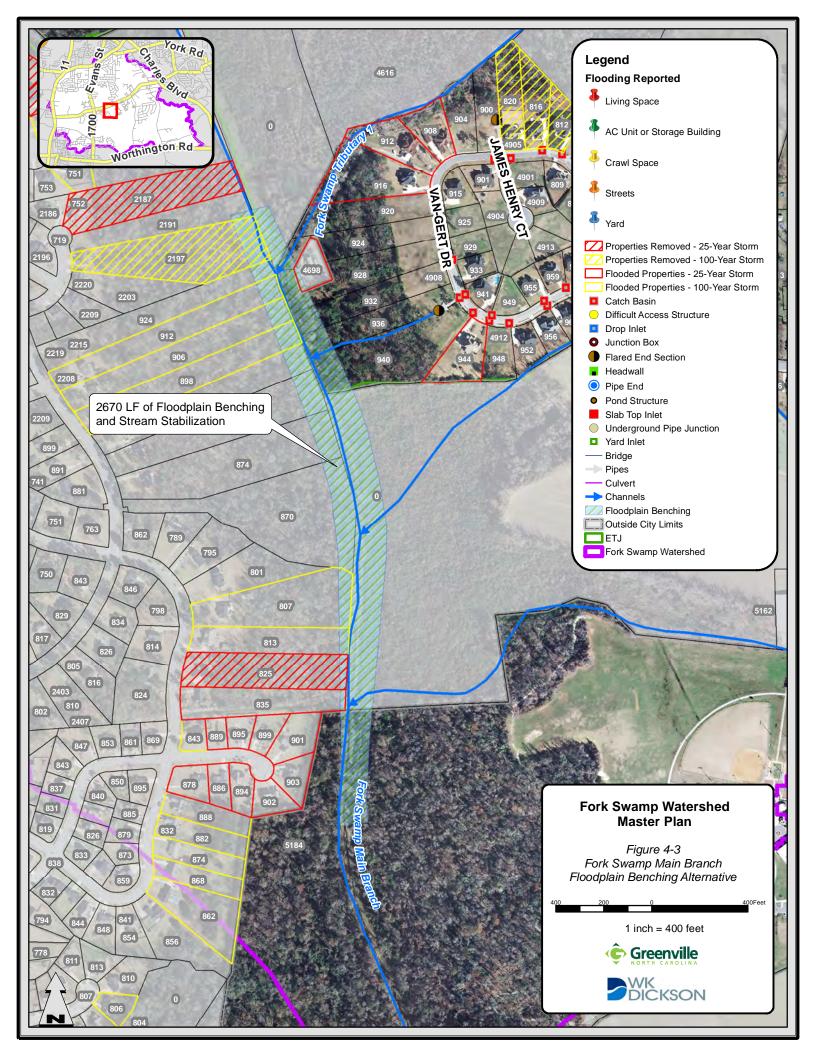
During a field inspection, there were several potential site restrictions and utility conflicts that were identified including overhead power lines that are located above East Fire Tower Road which may possibly be used as a construction entrance. The proposed grading area is heavily wooded in some locations and private easements would be required from approximately fourteen (14) property owners, however the land requiring easements does not currently seem to be utilized by the property owners. There are two sanitary sewer lines that cross the proposed project area to reach the sanitary main on the east bank. These lines may need to be replaced or relocated based on the elevations and material type of those lines. The total estimated cost for these improvements is \$1,740,000. The majority of the proposed floodplain bench appears to be located within a Pitt County Drainage District easement based on the Pitt County OPIS website. Coordination with the Drainage District will be required to implement the proposed project.





Fork Swamp Main Branch Floodplain Benching – In addition to the improvements proposed at and near the individual road crossings, there is a proposed floodplain benching and stream stabilization project located along the main branch of Fork Swamp downstream of FSUT1 and FSUT2. As shown on Figure 4-3, 2,670 linear feet of floodplain benching is proposed in the left and right overbanks. This will help to lower the tailwater at these two tributaries. Additionally, it will help to offset some of the increased flows generated from upsizing upstream culverts. The floodplain benching could be coordinated with the proposed Fork Swamp Greenway referenced in the 2004 Greenway Master Plan. Economy of savings could be provided if both projects are constructed at the same time.

Four (4) properties will be removed from the 25-year existing conditions floodplain and one (1) from the 100-year existing conditions floodplain as a result of the proposed floodplain benching. The proposed project is not located in the roadway therefore anticipated impacts to traffic are minimal. In order to gain access and to install the proposed floodplain benching, significant tree removal will be required, which will be costly and can be considered a negative impact of the project to some stakeholders, although the proposed graded area can be replanted after completion of construction. The installation of construction staging areas and entrances will require additional tree removal and temporary construction easements. It should be noted that the majority of the proposed improvements are located on private property therefore easements would be required to complete this project and maintain the bench in the future. The total estimated cost for these improvements is \$5,240,000. The majority of the proposed floodplain bench appears to be located within a Pitt County Drainage District easement based on the Pitt County OPIS website. Coordination with the Drainage District will be required to implement the proposed project.



A summary of the hydraulic performance for the improvements proposed along Fork Swamp are included in Tables 4-1 and 4-2. The water surface elevations shown assume all proposed primary system improvements for Fork Swamp are constructed. The level of improvement will be reduced if all projects are not implemented.

Table 4-1: Hydraulic Performance for Fork Swamp Main Branch Alternative

Location	Minimum Elevation at	Desired Level of	Calculated Water Surface Elevations (feet NAVD)				
	Top of Road (feet NAVD	Service (Year)	2-year flood	10-year flood	25-year flood	50-year flood	100-year flood
East Baywood Lane (Existing Twin 72" CMPs)	66.01	25-year	63.87	66.00	66.55	68.10	70.91
Railroad (Existing Twin 84" CMPs with Proposed Floodplain Benching)	70.89	100-year	63.03	65.03	66.42	68.02	70.87
Evans Street (Proposed Twin 7' x 7' RCBCs with Floodplain Benching)	66.51	50-year	60.29	61.90	62.86	63.78	64.99
East Fire Tower Road (Existing Bridge with Proposed Extended Floodplain Benching)	58.23	50-year	54.40	56.10	57.53	58.22	58.58

^{*}Bold text indicates the existing water surface has exceeded the crest or low point in the road thereby causing flooding.

Table 4-2: WSEL Reductions and Properties Removed from Floodplains – Fork Swamp Main Branch Alternative

Location		Reduction NAVD)	Properties Removed/ Properties in Floodplain		
	25-Year	100-Year	25-Year	100-Year	
East Baywood Lane	2.22	0.45	N/A*	N/A*	
Railroad	2.32	0.48	15/121	18/792	
Evans Street	2.92	2.21	0/0	0/0	
East Fire Tower Road with Floodplain Benching	0.28 - 2.31	0.33 - 1.12	4/6	12/22	

^{*}No proposed improvements at this location.

^{**} Green shade indicates crossing meets desired level of service. Red shade indicates crossing does not meet desired level of service.

4.1.2 FORK SWAMP UT1

Trafalgar Drive – South – As determined by the existing conditions analysis, the twin 60" CMPs at this crossing are undersized and not meeting the desired 25-year level of service. The culverts are in good condition. To provide the 25-year level of service and reduce the frequency and severity of flooding for the residents adjacent to the Trafalgar Drive – South culvert crossing, the installation of a 60" floodplain culvert with a new headwall is proposed (See Figure 4-4). The existing CMPs shown in Picture 4-2 will be left in place.



Picture 4-2. Trafalgar Drive - South Culverts

There are three (3) downstream properties in the 100-year existing conditions floodplain, that have the potential to experience yard, LAG, or structural flooding. These properties are as follows: 1405, 1407, and 1409 Trafalgar Drive. The proposed improvements will reduce the water surface elevations for the 25-year storm by 0.56 to 0.67 feet upstream of Trafalgar Drive – South. The water surface elevation will be reduced for all of these properties, only 1405 and 1407 Trafalgar Drive will be removed from the 100-year floodplain. The property at 1409 Trafalgar Drive will remain in the floodplain and continue to be subject to yard, LAG, or structural flooding but at reduced depths and likely reduced duration.

There are several potential site restrictions and utility conflicts that were identified at this project location. There appears to be sanitary sewer, electric, and gas lines that may need to be replaced or relocated. Impacts to traffic flow during construction were considered. Trafalgar Drive is a two-lane residential roadway. It is anticipated that a road closure or a flagged two-way one-lane operation will be required. The total estimated cost for this project is \$180,000.

Trafalgar Drive – North – As determined by the existing conditions analysis, the 60" and 66" CMPs at this crossing are not meeting the desired 25-year level of service. In order to provide a 25-year level of service at this crossing, the recommended alternative is to replace and upsize the culverts at Trafalgar Drive – North.

As part of this alternative, the existing CMPs will be replaced with twin 8′ x 5′ RCBCs. The upsized culvert will provide the desired 25-year level of service with 0.16 feet of freeboard. Figure 4-4 summarizes the improvements proposed at Trafalgar Drive – North. The resulting upstream water surface elevations will be reduced by as much as 0.95 feet in the 25-year storm event if improvements are also completed at Corey Road as described below.

There are three (3) properties in the existing conditions 25-year floodplain and two (2) additional properties in the 100-year floodplain, that have potential to experience LAG or structural flooding. These properties are as follows: 1210, 1214, 1404 Trafalgar Drive and 4800,

4801 Trevvett Circle. The water surface elevation will be reduced for all of these properties. The property at 1210 Trafalgar Drive and 4801 Trevvett Circle will be removed from the 25-year floodplain while 1404 Trafalgar Drive and 4800 Trevette Circle will be removed from the 100-year floodplain with the implementation of this alternative. The remaining property at 1214 Trafalgar Drive will continue to be exposed to LAG or structural flooding, although depth will be reduced. The total estimated cost for this project is \$440,000.

There are several potential site restrictions and utility conflicts that were identified at this project location. There appears to be sanitary sewer, electric, and gas lines that may need to be replaced or relocated. Impacts to traffic flow during construction were considered. Trafalgar Drive is a two-lane residential roadway. It is anticipated that a road closure or a flagged two-way one-lane operation will be required.

Corey Road – Based on the results obtained from the existing conditions analysis, the existing twin 13′ x 4.5 CMP arches (See Picture 4-3) at Corey Road are passing the desired 25-year storm.

However, in order to lower the tailwater and improve the performance of the culvert at Trafalgar Drive – North, the capacity at Corey Road will be increased. This alternative proposes the installation of twin 48" floodplain culverts along with a new headwall at Corey Road.

In addition to the proposed floodplain culvert, it is recommended that 2,300 linear feet of floodplain benching be included downstream of Corey Road as shown on Figure 4-4. The floodplain benching will be located in the left and right overbanks.



Picture 4-3. Corey Road CMP arches

Although the benching is located outside of the City limits, it will help to reduce the tailwater at Corey Road and subsequently Trafalgar Drive which directly impacts City residents. To implement proposed improvements for FSUT1, the Corey Road project should be completed before the Trafalgar Drive improvements.

There are four properties (1203, 1205, 1209, and 1215 Trafalgar Drive) upstream of Corey Road located in the existing conditions 25- and 100-year floodplain. The resident located at 1209 Trafalgar Drive has reported storage building flooding. The property at 1215 Trafalgar Drive will be removed from the 25-year floodplain and 1209 Trafalgar Drive will be removed from the 100-year floodplain. While the water surface elevations will be reduced at remaining properties, they will remain in the 25- and 100-year floodplains. They will continue to experience flooding but the severity and frequency will be reduced.

During a field inspection, there were several potential site restrictions and utility conflicts that were identified. Overhead power lines are located along Corey Road, which may need to be temporarily relocated based on where the contractor accesses the site. There also appears to be

water lines that may need to be replaced or relocated. Impacts to traffic flow during construction were considered. This section of Corey Road is a two-lane minor thoroughfare. It is anticipated that a road closure or a flagged two-way one-lane operation will be required. In order to gain access and to install the proposed floodplain benching, tree removal would be required. It should be noted that the proposed floodplain benching is located on private property therefore an easement will be required to complete this project and maintain the bench in the future. The total estimated cost for this project is \$6,870,000.

A summary of the hydraulic performance for the improvements proposed along Fork Swamp are included in Table 4-3, and a summary of the improvements realized for reduction in WSEL and properties removed from floodplains is shown in Table 4-4. The water surface elevations shown assume all proposed primary system improvements for FSUT1 are constructed. The level of improvement will be reduced if all projects are not implemented.

Table 4-3: Hydraulic Performance for FSUT1 – Alternative #1

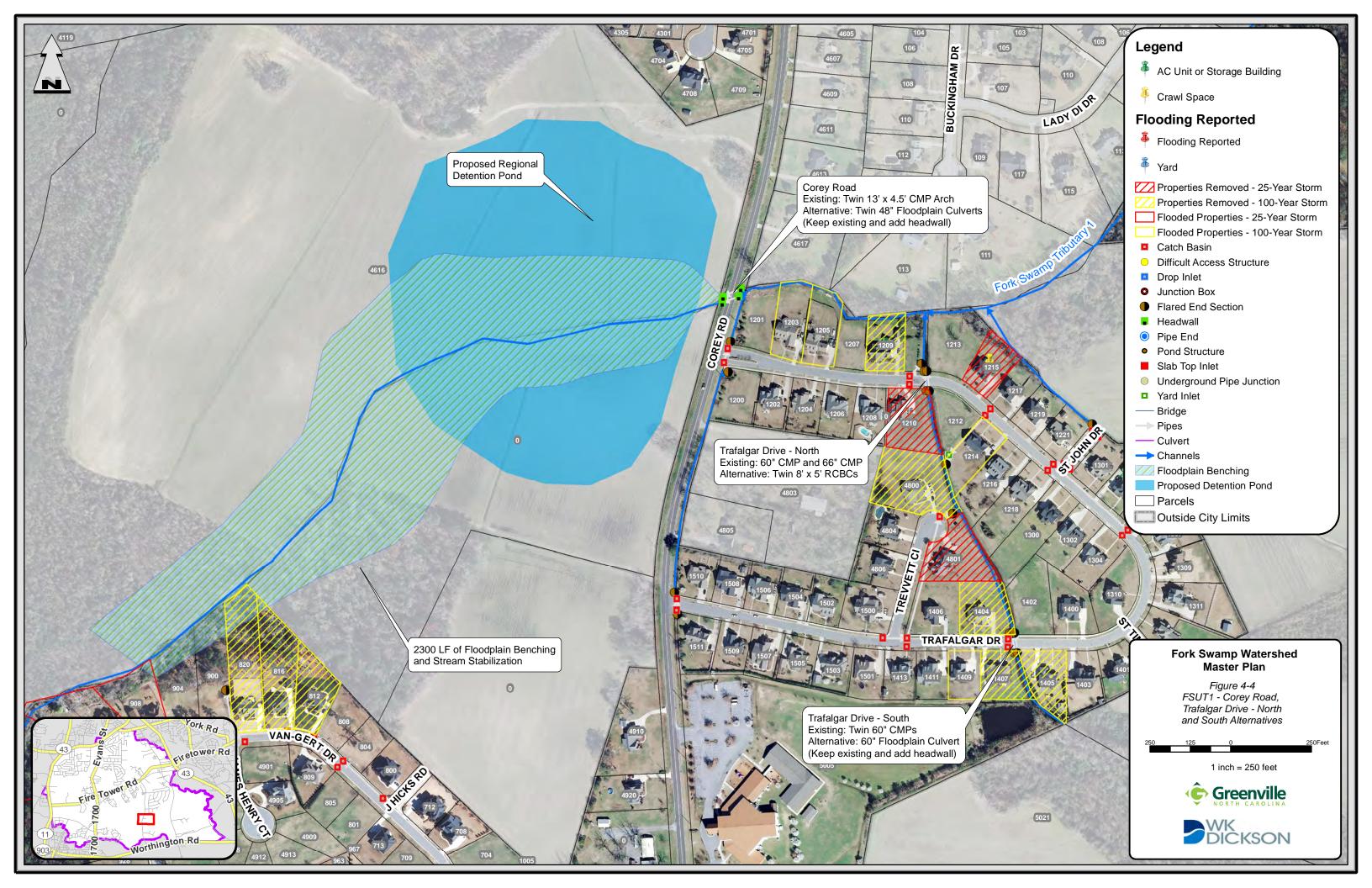
	Minimum Elevation at	Calculated Water Surface Elevations (feet NAVD)					
Location	Top of Road	Level of Service	2-year	10-year	25-year	50-year	100-year
	(feet NAVD)	(Year)	flood	flood	flood	flood	flood
Trafalgar Drive - South							
(Existing Twin 60"	55.81	25-year	53.14	54.57	55.62	56.13	56.38
CMPs with Proposed							
60" Floodplain Culvert)							
Trafalgar Drive - North							
(Proposed Twin 8' x 5'	54.35	25-year	52.40	53.48	54.19	54.73	55.16
RCBCs)							
Corey Road (Existing							
Twin 13' x 4.5 CMP Arch	E4 01	25	E0.0E	F1 (4	F2 20	F2 00	F2.06
with Proposed Twin 48"	54.81	25-year	50.95	51.64	52.30	53.00	53.96
Floodplain Culverts)							

^{*}Bold text indicates the existing water surface has exceeded the crest or low point in the road thereby causing flooding.

Table 4-4: WSEL Reductions and Properties Removed from Floodplains – FSUT2: Alt #1

Lanting	WSEL Reducti	on (feet NAVD)	Properties Removed/Properties in Floodplain		
Location	25-Year	100-Year	25-Year	100-Year	
Trafalgar Drive - South	0.67	0.25	2/3	2/3	
Trafalgar Drive - North	0.95	0.62	2/3	2/5	
Corey Road	1.96	1.47	1/4	1/4	

^{**} Green shade indicates crossing meets desired level of service. Red shade indicates crossing does not meet desired level of service.

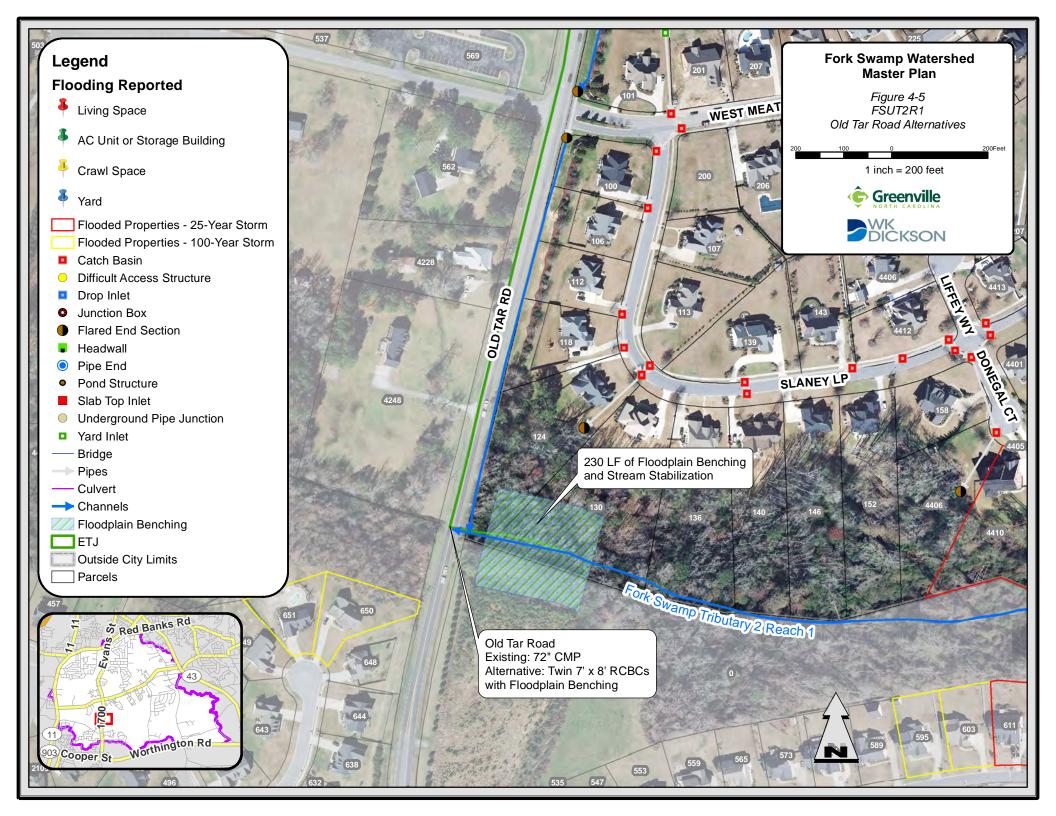


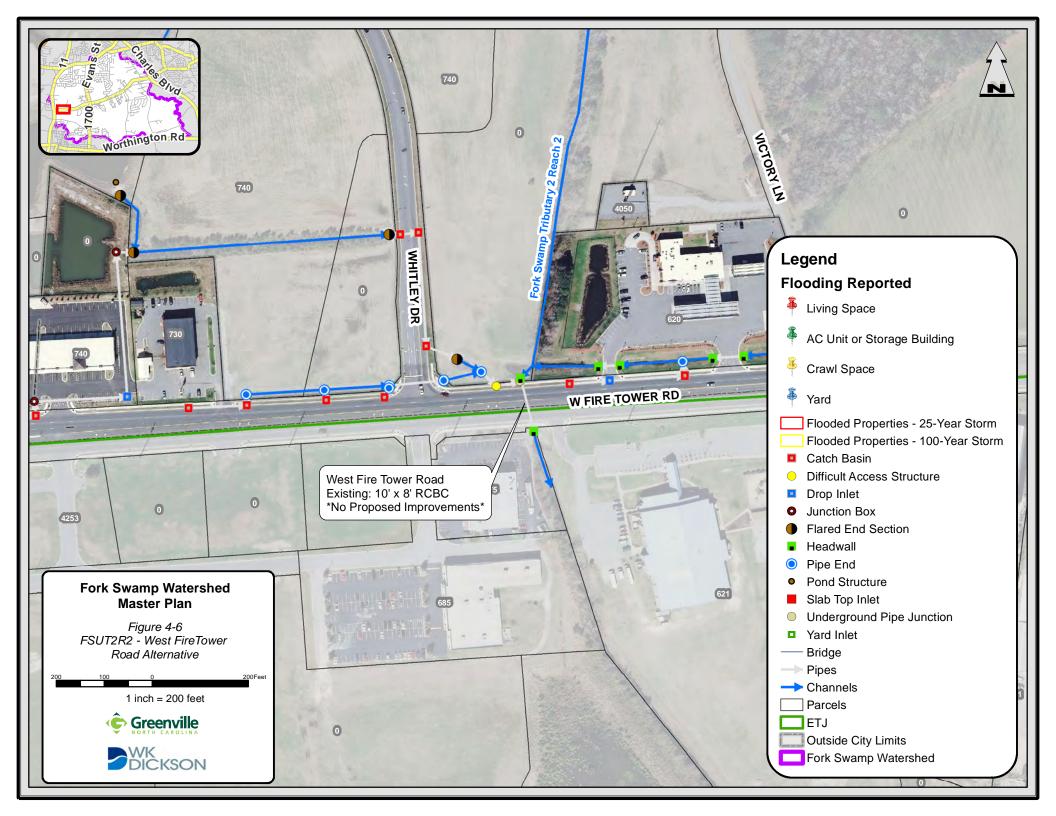
4.1.3 FORK SWAMP UT2R1

Old Tar Road – The existing 72" CMP at this crossing is currently operating at a 2-year level of service. In order to meet the desired 50-year level of service, the existing CMP will need to be replaced with twin 7' x 8' RCBCs with 230 linear feet of floodplain benching in the left and right overbanks proposed downstream of Old Tar Road (See Figure 4-5). Old Tar Road is located immediately west of the existing City limits and the City's ETJ. A portion of the proposed floodplain benching along the left bank would be inside the City limits. Old Tar Road is also a DOT maintained road. Based on the location of the road crossing outside the City limits, the Old Tar Road project is not included as a capital project for the City of Greenville. It is recommended that the City consider initiating discussions with NCDOT to determine if upgrades to the culvert could be considered to reduce the risk to City and County residents that travel along the roadway.

4.1.4 FORK SWAMP UT2R2

West Fire Tower Road – The existing 10′ x 8′ RCBC at West Fire Tower Road meets the desired 50-year level of service. The culvert is in good condition and passes the future 100-year flows with over one foot of freeboard. Consequently, no improvements are proposed for this location.





4.1.5 FORK SWAMP UT3

Fork Swamp UT3 includes a total of seven (7) crossings from County Home Road to East Fire Tower Road north of the confluence with Fork Swamp. Generally, projects should be constructed from downstream to upstream, although there may be instances when this general approach can be deviated from based on budgets, potential benefits, easement acquisition, and permitting concerns. Project sequencing will be discussed with the prioritization discussion.

Coleman Drive – The existing triple 10′ x 4′ RCBCs at this crossing are in good condition and currently meet the desired 25-year level of service. With the downstream improvements recommended along FSUT3, the RCBCs will continue to pass the 25-year storm. Therefore, no capital improvements are proposed at this location. (See Figure 4-7)



Picture 4-4. County Home Road RCPs

County Home Road – Based on the results obtained from the existing conditions analysis, the existing twin 48" RCPs at County Home Road shown in Picture 4-4 overtop during the 25-year event, therefore not providing the desired 50-year storm level of service. The proposed alternative entails adding a 42" floodplain culvert. The increased capacity provided by the floodplain culvert at County Home Road coupled with downstream floodplain benching will provide the desired 50-year level of service at County Home Road.

The proposed 243 linear feet of floodplain benching is proposed along the left bank downstream of County Home Road to provide additional capacity in the floodplain and to lower the tailwater for the culverts. The location of the proposed 40-foot-wide floodplain bench is shown on Figure 4-7. The resulting upstream water surface elevation will be decreased by as much as 1.34 feet in the 25-year storm event and 0.51 feet in the 100-year storm event. There are six (6) properties upstream of County Home Road located in the 25- and 100-year existing conditions floodplain. These properties are as follows: 1900 East Fire Tower Road and 1903, 1907, 1911, 1915, and 1923 Arlington Park Drive. Two of the six properties (1903 and 1907 Arlington Park Road) will be removed from the 25-year floodplain and two from the 100-year floodplain (1911 and 1915 Arlington Park Road). While the water surface elevations will be reduced at the remaining properties, they remain in the 25- and 100-year floodplains. The properties will continue to be floodprone during large events however the severity and frequency of flooding will be reduced.

During a field inspection, there were several potential site restrictions and utility conflicts that were identified. There appears to be sanitary sewer, water, gas, and electric lines that may need to be replaced or relocated for installation of the floodplain culvert. Impacts to traffic flow during construction were considered. County Home Road is a major multi-lane thoroughfare maintained by NCDOT. It is anticipated that a flagged two-way two-lane operation will be

required and coordination with NCDOT will be required. Additional impacts from the construction of the floodplain benching will include tree removal along the left bank and easements. Tree removal along the right bank should be minimized to provide a visual buffer between the gas station and the residential areas on the left bank. The total estimated cost for this project is \$210,000.

East Fire Tower Road – U/S – The next crossing downstream of County Home Road is East Fire Tower Road, which is also maintained by NCDOT. As determined by the existing conditions analysis, twin 54" RCPs at this crossing are currently providing a 2-year level of service. In order to provide the desired 50-year level of service at this crossing, the recommended alternative is to replace and upsize the culverts at East Tower Road – U/S. The detention pond upstream of East Fire Tower Road was considered for expansion to avoid further infrastructure improvements, however it was not considered feasible without acquisition of commercial property along East Fire Tower Road which would likely be cost prohibitive.

As part of this alternative, the existing RCPs will be replaced with twin 6′ x 6′ RCBCs. While the existing culverts were in good condition there is limited space available for infrastructure improvements at this location, therefore box culverts are proposed to maximize flow capacity in a narrow corridor. The proposed culvert will provide the desired 50-year level of service with 0.21 feet of freeboard. Figure 4-7 summarizes the improvements proposed at East Tower Road –U/S. The resulting upstream water surface elevations will be reduced by as much as 1.45 feet in the 25-year storm event and 0.58 in the 100-year storm event.

There are three (3) properties in the existing conditions 25-year floodplain and one (1) additional property in the 100-year floodplain, that have potential to experience LAG or structural flooding. These properties are as follows: 1600 and 1604 East Fire Tower Road, 1751 Old Fire Tower Road, and 2100 Esther Circle. The water surface elevation will be reduced for all of these properties and the Insurance Agency located at 1604 East Fire Tower Road will be

removed from the 25-year floodplain with the implementation of this alternative. The remaining properties will continue to be exposed to LAG or structural flooding during the 25-year event, although the depth, duration and frequency will be reduced.

During a field visit, there were several potential site restrictions and utility conflicts that were identified at this project location including light poles and electrical boxes (See Picture 4-5) which will need to be replaced. There appears to be sanitary sewer (8"



Picture 4-5. East Fire Tower Road -U/S RCPs

ductile iron) and electric lines that may also need to be replaced or relocated. East Fire Tower

Road is a major thoroughfare roadway maintained by NCDOT. Coordination with NCDOT may require additional time for permitting and design. There will be significant impacts to traffic flow during construction. The total estimated cost for this project is \$680,000.

Wimbledon Drive – Immediately downstream of East Fire Tower Road, the channel follows the property line and then turns west around the Wasabi 88 restaurant towards Wimbledon Drive. The existing twin 60" CMPs at Wimbledon Drive are currently providing a 2-year level of service. The culverts are in fair condition although some rust on the ends of the pipes were observed. In order to meet the desired 25-year level of service, it is proposed that the culverts at Wimbledon Drive be upsized with twin 10' x 5' RCBCs coupled with 245 linear feet of floodplain benching in the right overbank downstream of Wimbledon Drive (See Figure 4-7). The floodplain benching will reduce the tailwater at Wimbledon Drive allowing the proposed culverts to convey additional flow. In addition, the floodplain benching can be coupled with the recommended Stream Stabilization Project #4 recommended in Section 5.1 of this report. As noted in that section, portions of this stream have significant erosion and limited to no vegetative buffer. The proposed improvements will provide the desired 25-year level of service with 0.57 feet of freeboard.

There is one (1) property at 1605 East Fire Tower Road (Wasabi 88) that is in the existing conditions 25-year floodplain that has potential to experience LAG or structural flooding. With the implementation of this alternative, this property will be removed from the floodplain.

During a field visit, there were several potential site restrictions and utility conflicts that were identified at this project location. There appears to be sanitary sewer and water lines that may need to be replaced or relocated. Wimbledon Drive is a two-lane residential roadway. It is anticipated that a road closure or a flagged two-way one-lane operation will be required. In order to gain access and to install the proposed floodplain benching, tree removal would be required. It should be noted that the proposed floodplain benching is located on private property therefore an easement will be required to complete this project and maintain the bench in the future. The installation of construction staging areas and entrances will require additional tree removal and temporary construction easements. The total estimated cost for this project is \$610,000.

Tower Place – Tower Place is located approximately 450 feet downstream of Wimbledon Drive. The existing twin 66" CMPs shown in Picture 4-6 are currently operating at a 2-year level of service and as noted in Section 5.1, the channel is eroding for approximately 230 feet upstream of Tower Place and downstream of Tower Place due in part to an absence of trees and vegetation to stabilize the banks. Additionally, the absence of a headwall has resulted in erosion between the edge

Picture 4-6. Tower Place CMPs

of the road and the culvert that will eventually threaten the integrity of the roadway. In order to meet the desired 25-year level of service, it is proposed that the culverts at Tower Place be replaced with twin $10' \times 5'$ RCBCs (See Figure 4-7). The upsized culvert will provide a 25-year level of service with 0.68 feet of freeboard.

There are twelve (12) properties upstream of the Tower Place crossings in the Tower Village complex that are in the 25- and 100-year existing floodplains. Installing this alternative will reduce the upstream water surface elevation by as much as 0.96 feet in the 25-year storm and 0.32 feet in the 100-year storm. This will remove two properties (2001 Tower Place and 1409B Angels End) from the 25-year floodplain and 1409A Angels End from the 100-year floodplain. The remaining properties in Tower Village will continue to be exposed to LAG or structural flooding, although the depth, duration, and frequency of flooding will be reduced.

During a field visit, there were several potential site restrictions and utility conflicts that were identified at this project location. There appears to be sanitary sewer, gas, and electrical lines that may need to be replaced or relocated. Tower Place is a two-lane residential roadway. It is anticipated that a road closure or a flagged two-way one-lane operation will be required. The installation of construction staging areas and entrances will require tree removal and temporary construction easements. If possible, the proposed Tower Place improvements should be coupled with the stream stabilization recommendations shown as Project #4 in Section 5.1. The total estimated cost for the Tower Place culvert improvements is \$640,000.

Summerhaven Drive – Immediately downstream of Tower Place is the Summerhaven Drive crossing. As determined by the existing conditions analysis, the 66" CMPs at this crossing are undersized and currently providing a 2-year level of service. To provide the desired 25-year level of service at this crossing, the recommended alternative is to replace and upsize the culverts at Summerhaven Drive.

As part of this alternative, the existing CMPs will be replaced with quad 6′ x 6′ RCBCs. The upsized culvert will provide the desired 25-year level of service with 0.20 feet of freeboard. To allow additional capacity and reduce the tailwater on the Summerhaven culverts, 115 linear feet of floodplain benching has been proposed downstream of the crossing along the left overbank (See Figure 4-7). The resulting upstream water surface elevation will be decreased by as much as 1.18 feet in the 25-year storm event and 0.51 feet in the 100-year storm event. There are thirteen (13) properties upstream of Summerhaven Drive located in the 25- and 100-year existing conditions floodplain. Seven (7) properties will be removed from the 25-year floodplain. While the water surface elevations will be reduced at the remaining properties, they remain in the 25- and 100-year floodplains. The properties will continue to experience flooding but the severity and frequency will be reduced.

During a field visit, there were several potential site restrictions and utility conflicts that were identified at this project location. There appears to be water and electrical lines that may need to be replaced or relocated. Summerhaven Drive is a two-lane residential roadway. It is

anticipated that a road closure or a flagged two-way one-lane operation will be required. In order to gain access and to install the proposed floodplain benching, tree removal would be required. It should be noted that the proposed floodplain benching is located on private property therefore an easement will be required to complete this project and maintain the bench in the future. The installation of construction staging areas and entrances will require additional tree removal and temporary construction easements. The total estimated cost for this project is \$650,000.

East Fire Tower Road – D/S – East Fire Tower Road is the most downstream crossing for FSUT3. Currently, the existing twin $10' \times 7'$ corrugated metal ellipse pipes only pass the 2-year storm. To meet the desired 50-year level of service, it is proposed that the existing culverts be removed and replaced with quad $6' \times 7'$ RCBCs. In addition to the culvert upgrade, a total of 3,240 linear feet of floodplain benching is proposed (990 linear feet upstream of the crossing in the left overbank and 2,250 linear feet downstream of the crossing in the left and right overbanks). The floodplain benching could be coordinated with the proposed Fire Tower to Hub - Connector Greenway referenced in the 2004 Greenway Master Plan. Economy of savings could be provided if both projects are constructed at the same time.

Figure 4-8 summarizes the proposed improvements.

The resulting upstream water surface elevation will be decreased by as much as 1.94 feet in the 25-year storm event and 0.77 feet in the 100-year storm event. There are forty-seven (47) properties between East Fire Tower Road – D/S and Summerhaven Drive located in the 25- and 100-year existing conditions floodplain. Twenty-eight (28) will be removed from the 25-year floodplain and fourteen (14) additional from the 100-year floodplain. While the water surface elevations will be reduced for the remaining five (5) properties, they remain in the 25- and 100-year floodplains. The properties will continue to experience flooding but the severity and frequency will be reduced. The floodplain benching upstream of East Fire Tower Road could also be coupled with Stream Stabilization Project #3 described in Section 5.1 to address both the capacity and erosion issues upstream of East Fire Tower Road.

The downstream water surface elevation will also be decreased as a result of the proposed floodplain benching. The reduction will range between 0.64 and 1.93 feet in the 25-year storm and 0.62 and 2.04 feet in the 100-year storm. There are fifteen (15) properties located in the 25-and 100-year existing conditions floodplains. All of these properties downstream of East Fire Tower Road – D/S will be removed from the floodplain as a result of the proposed improvements.

During a field visit, there were several potential site restrictions and utility conflicts that were identified at this project location including light poles and electrical boxes which will need to be replaced. There appears to be gas and electric lines that may also need to be replaced or relocated. An 18" sanitary sewer line runs parallel to the creek throughout the project area. The proposed floodplain benching will avoid conflicting with the sanitary sewer line to the extent

possible. East Fire Tower Road is a major thoroughfare roadway maintained by NCDOT. There will be significant impacts to traffic flow during construction. Coordination with NCDOT may require additional time for permitting and design. Additionally, FEMA permitting may be required for the southern portion of the floodplain benching. In order to gain access and to install the proposed floodplain benching, tree removal would be required. It should be noted that the proposed floodplain benching is located on private property therefore an easement will be required to complete this project and maintain the bench in the future. The installation of construction staging areas and entrances will require additional tree removal and temporary construction easements. The total estimated cost for this project is \$4,000,000.

A summary of the hydraulic performance for the improvements proposed along Fork Swamp are included in Table 4-5, and a summary of the improvements realized for reduction in WSEL and properties removed from floodplains is shown in Table 4-6. The water surface elevations shown assume all proposed primary system improvements for FSUT1 are constructed. The level of improvement will be reduced if all projects are not implemented.

Table 4-5: Hydraulic Performance for FSUT3 – Alternative #1

Location	Minimum Elevation at	Desired Level of	Calculated Water Surface Elevations (feet NAVD)				
Location	Top of Road (feet NAVD)	Service (Year)	2-year flood	10-year flood	25-year flood	50-year flood	100-year flood
Coleman Drive (Existing Triple 10' x 4' RCBCs)	61.97	25-year	57.67	59.47	60.47	61.34	62.01
County Home Road (Twin 48" RCPs with Proposed 42" Floodplain Culvert)	65.81	50-year	63.12	63.96	64.79	65.62	66.21
East Fire Tower Road – U/S (Proposed Twin 6' x 6' RCBC)	64.51	50-year	61.06	62.39	63.51	64.31	64.74
Wimbledon Drive (Proposed Twin 10' x 5')	63.61	25-year	60.40	61.83	63.04	63.73	64.04
Tower Place (Proposed Twin 10' x 5')	63.01	25-year	59.41	61.12	62.33	62.92	63.26
Summerhaven Drive (Proposed Quad 6' x 6')	61.51	25-year	58.42	60.24	61.31	62.00	62.42
East Fire Tower Road – D/S (Proposed Quad 6' x 7' RCBC)	59.51	50-year	55.77	57.23	58.26	59.15	59.95

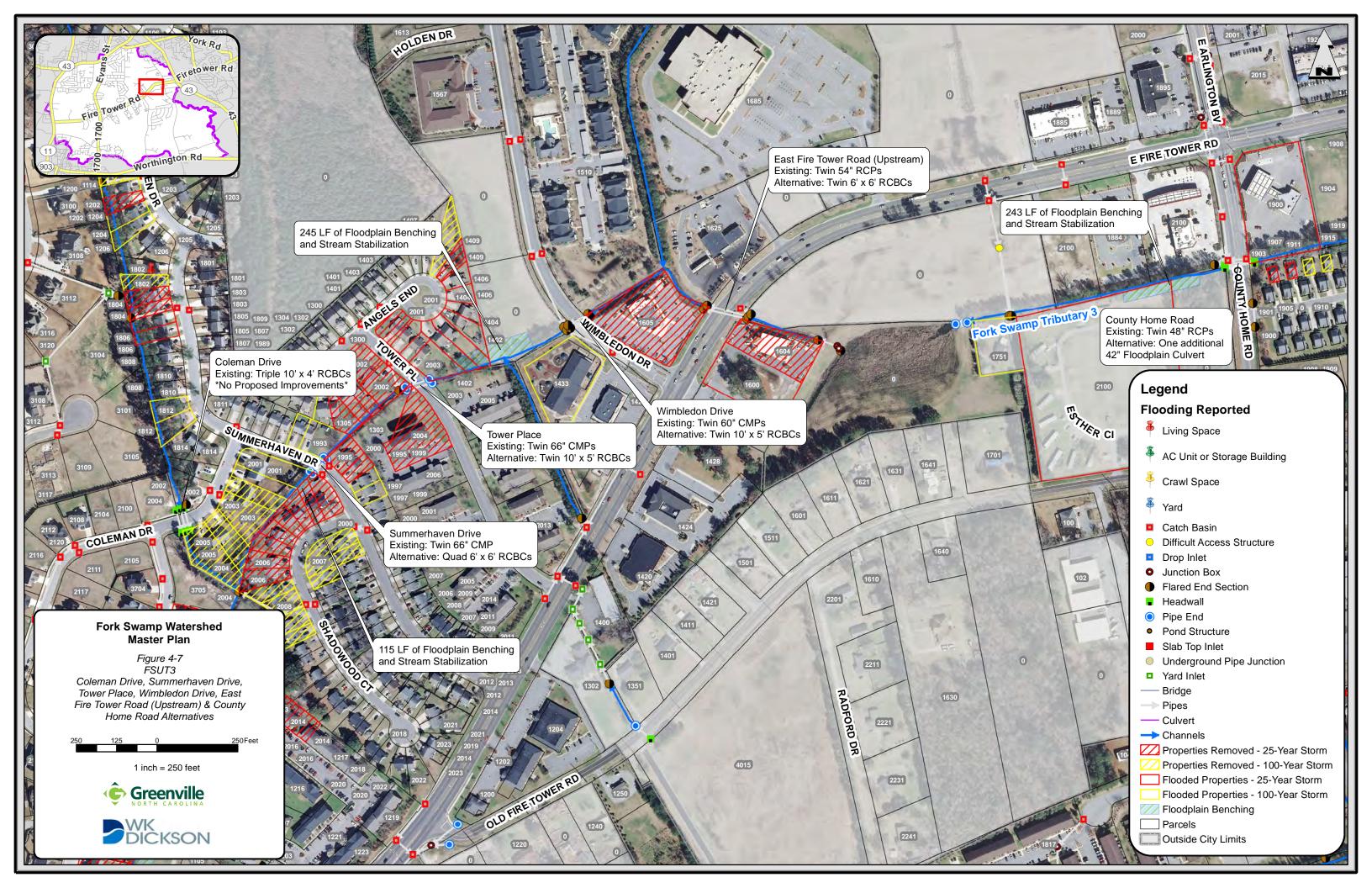
^{*}Bold text indicates the existing water surface has exceeded the crest or low point in the road thereby causing flooding.

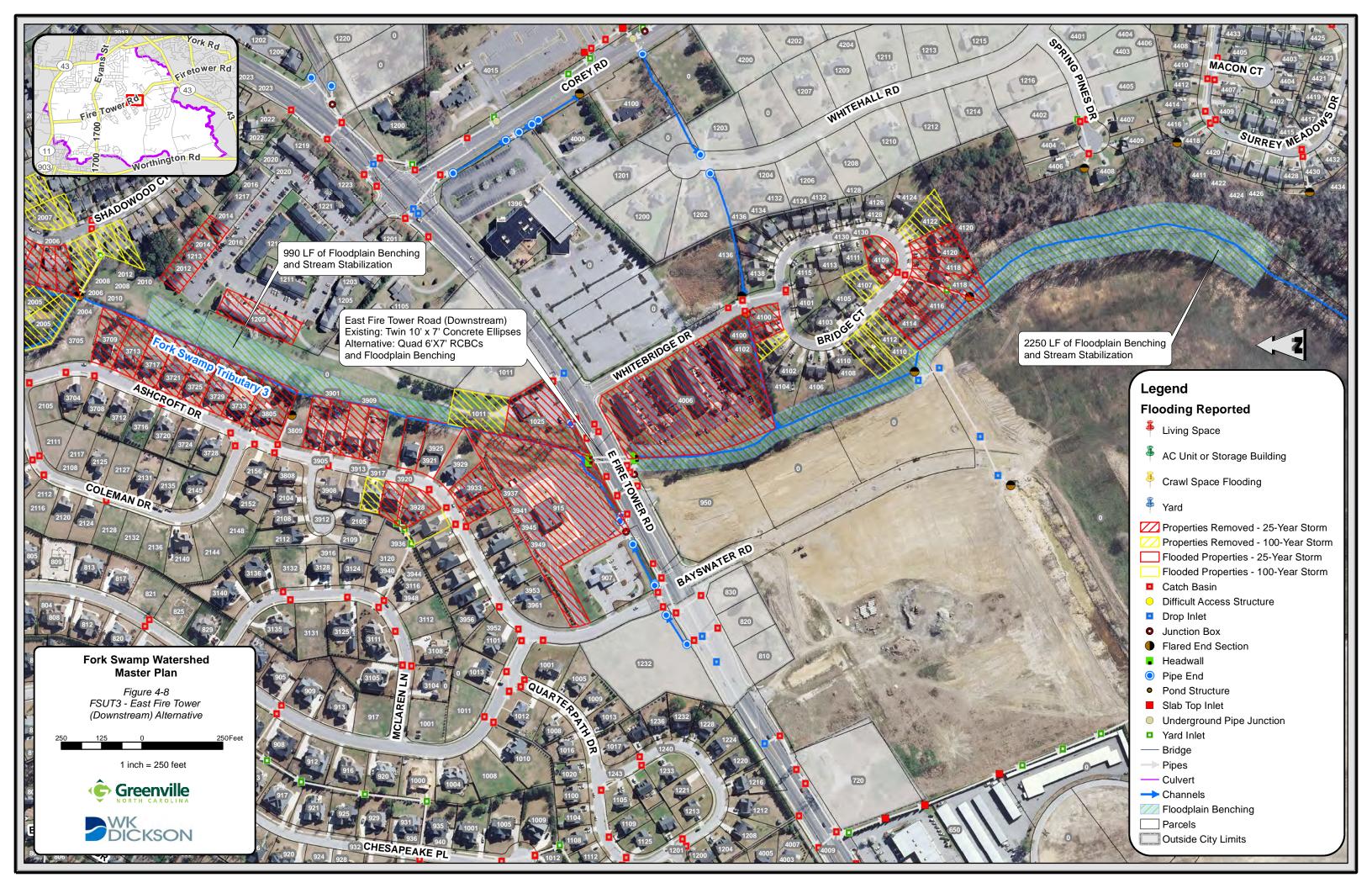
^{**} Green shade indicates crossing meets desired level of service. Red shade indicates crossing does not meet desired level of service.

Table 4-6: WSEL Reductions and Properties Removed from Floodplains – FSUT3: Alt #1

Location		Reduction NAVD)	Properties Removed/Properties in Floodplain		
	25-Year 100-Year		25-Year	100-Year	
Coleman Drive	1.49	0.80	N/A*	N/A*	
County Home Road	1.34	0.51	2/6	2/6	
East Fire Tower Road					
(Upstream)	1.45	0.58	1/3	0/1	
Wimbledon Drive	1.21	0.40	1/1	0/0	
Tower Place	0.96	0.32	1/12	2/12	
Summerhaven Drive	1.18	0.51	7/13	0/13	
East Fire Tower Road (Downstream)	1.94	0.77	28/47	42/47	

^{*}No proposed improvements at this location.





4.1.6 COREY ROAD REGIONAL DETENTION FACILITY

While developing the alternatives for the Fork Swamp watershed, opportunities for potential regional detention facilities were explored. There was one area downstream of Corey Road on FSUT1 (See Figure 4-4), that was analyzed to determine its benefits on downstream flooding. Based on the development of a conceptual model, the proposed 20-acre detention pond would lower the flows in the 2-, 10-, 25-, 50-, and 100-year storms by 20 to 25 percent at the confluence of FSUT1 with Fork Swamp. These flow reductions continue through the downstream modeling limits of the Fork Swamp watershed. If the detention is not implemented in conjunction with the other improvements proposed for the primary system, the percent increase at the outfall will be 7 percent in the 25- year storm event.

The implementation of this facility will not impact any of the sizes of the culvert recommended as part of this Master Plan. However, it will reduce downstream flows and help to offset increases that will be created by upsizing upstream culverts. The location of this facility is outside of the City limits close to the border of Winterville. It would be an opportunity to partner with this municipality which would also benefit from the implementation of the regional detention facility. If implemented, the floodplain benching shown downstream of Corey Road (See Figure 4-4) would not be necessary.

During a field inspection, there were several potential site restrictions and utility conflicts that were identified. Overhead power lines are located along Corey Road, which may need to be



Picture 4-7. Proposed Site for Regional Detention Facility

temporarily relocated based on where the contractor accesses the site. In order to gain access and to install the proposed regional detention facility, tree removal would be required. Tree removal in the upstream portion of the facility nearest Corey Road will require minimal tree removal since it is located in an open, agricultural field as shown in Picture 4-7. It should be noted that the proposed regional detention facility is located on private property therefore an easement will be required to complete this project and maintain the facility in the future. The installation of construction staging areas and entrances will require additional tree

removal and temporary construction easements. The total estimated cost for this project is \$8,370,000, which does not include land acquisition cost. Based on Pitt County tax records, an additional \$1,130,000 would be required to purchase the land bringing the total project cost to \$9,500,000.

4.1.7 Hydrology

The future land use was accounted for during the development of the proposed improvements. The hydrologic parameters including curve numbers were adjusted for the future conditions and alternatives models.

Peak flows for the primary systems were developed for the 2-, 10-, 25-, 50-, and 100-year storm events considering the future conditions and proposed alternatives. The future conditions peak flows are summarized in Table 4-7. In comparison to the existing conditions flows, the future conditions flows increases in the 25-year storm are as follows:

- Fork Swamp 0 to 7%
- FSUT1 8 to 12%
- FSUT2R1 10 to 11%
- FSUT2R2 0 to 15%
- FSUT3 1 to 14%

Table 4-7: Future Conditions Flows from HEC-HMS for Fork Swamp Watershed

	B. 1N.	HEC-		nt					
HEC-HMS Node	Road Name / Location	RAS	2-year	10-year	25-year	50-year	100-year		
		Station	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)		
FORK SWAMP									
East Baywood Lane	East Baywood Lane	55891	188	352	468	569	681		
Railroad	Railroad	55592	251	475	629	765	916		
Evans Street	Evans Street	54609	258	488	644	785	939		
E Fire Tower Road (Bridge)	East Fire Tower Road	50168	464	877	1,174	1,432	1,718		
ADD FSUT3 to FS	Confluence of FSUT3 and Fork Swamp	46863	599	1,124	1,505	1,843	2,211		
ADD FSUT2	Confluence of FSUT2 and Fork Swamp	44420	850	1,595	2,121	2,614	3,187		
ADD FSUT1	Confluence of FSUT1 and Fork Swamp	43230	1,094	2,102	2,826	3,502	4,237		
FORK SWAMP UT1									
U/S Limit FSUT1	Upstream Limit of FSUT1/Trafalgar Drive – South	5103	123	244	332	412	500		
Trafalgar Drive	Trafalgar Drive – North	4235	127	252	343	425	517		
Corey Road – FSUT1	Corey Road	3380	229	462	630	785	963		

SECTION 4: FLOOD MITIGATION ALTERNATIVES

HEC-HMS Node	Road Name / Location	HEC-	HEC- Storm Event						
		RAS	2-year	10-year	25-year	50-year	100-year		
	Location	Station	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)		
FORK SWAMP UT2R1									
ADD FSUT2-7B	Old Tar Road	3499	265	502	672	819	985		
	FORK SWAMP UT2R2								
U/S Limit FSUT2	Upstream Limit of FSUT2	4262	49	90	118	143	171		
West Fire Tower	West Fire Tower Road	303	131	241	319	389	465		
	FORK SWAMP UT3								
U/S Limit FSUT3	Upstream Limit of FSUT3	4360	112	217	294	362	438		
Coleman Drive	Coleman Drive	289	152	306	419	519	632		
County Home	County Home Road	10420	65	115	150	181	213		
East Fire Tower Road – North	East Fire Tower Road – U/S	8790	111	177	230	273	316		
Wimbledon Drive	Wimbledon Drive	8238	168	282	369	443	519		
Tower Pl_ Summerhaven Dr	Tower Place/ Summerhaven Drive	7694/ 7287	190	332	436	527	623		
East Fire Tower Road - South	East Fire Tower Road – D/S	5065	351	653	876	1,069	1,278		

The alternative flows were developed from the future conditions taking into account attenuation for the proposed culvert sizes. They differed slightly from the future condition peak flows presented in Table 4-7. The peak flows used for the proposed alternatives are summarized in Table 4-8. A hard copy of the HEC-HMS output is included as Appendix H. The CD found in Appendix J contains a digital copy of the HEC-HMS model for the Fork Swamp watershed.

Table 4-8: Alternative #1 Flows from HEC-HMS for Fork Swamp Watershed

HEC-HMS Node	Road Name /	HEC- Storm Event						
	Location	RAS	2-year	10-year	25-year	50-year	100-year	
	Location	Station	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	
FORK SWAMP								
East Baywood	East Baywood	55891	188	352	468	569	681	
Lane	Lane	55891	100	332	400	369	001	
Railroad	Railroad	55592	252	475	629	765	916	
Evans Street	Evans Street	54609	258	488	644	785	939	
E Fire Tower	East Fire Tower	50168	464	877	1 174	1,432	1 710	
Road (Bridge)	Road		404	6//	1,174		1,718	

SECTION 4: FLOOD MITIGATION ALTERNATIVES

THE CHAIN	D 137 /	HEC-	Storm Event					
HEC-HMS Node	Road Name / Location	RAS Station	2-year (cfs)	10-year (cfs)	25-year (cfs)	50-year (cfs)	100-year (cfs)	
ADD FSUT3 to FS	Confluence of FSUT3 and Fork Swamp	46863	596	1,137	1,526	1,868	2,246	
ADD FSUT2	Confluence of FSUT2 and Fork Swamp	44420	857	1,615	2,178	2,663	3,286	
ADD FSUT1	Confluence of FSUT1 and Fork Swamp	43230	1,097	2,129	2,886	3,549	4,285	
		FORK SW	VAMP UT	1				
U/S Limit FSUT1	Upstream Limit of FSUT1/Trafalgar Drive – South	5103	123	244	332	412	500	
Trafalgar Drive	Trafalgar Drive – North	4235	127	252	343	425	517	
Corey Road – FSUT1	Corey Road	3380	230	462	636	788	962	
		FORK SWA	AMP UT2	R1				
ADD FSUT2-7B	Old Tar Road	3499	265	502	672	819	985	
		FORK SWA	AMP UT2	R2				
U/S Limit FSUT2	Upstream Limit of FSUT2	4262	49	90	118	143	171	
West Fire Tower	West Fire Tower Road	303	131	241	319	389	465	
FORK SWAMP UT3								
U/S Limit FSUT3	Upstream Limit of FSUT3	4360	112	217	294	362	438	
Coleman Drive	Coleman Drive	289	152	306	419	519	632	
County Home	County Home Road	10420	65	115	150	181	214	
East Fire Tower Road – North	East Fire Tower Road – U/S	8790	113	196	255	297	347	
Wimbledon Drive	Wimbledon Drive	8238	174	305	399	469	551	
Tower Pl_ Summerhaven Dr	Tower Place/ Summerhaven Drive	7694/ 7287	192	341	452	542	643	
East Fire Tower Road - South	East Fire Tower Road – D/S	5065	349	667	898	1,095	1,314	

4.1.8 Hydraulics

The hydraulic analysis for the proposed conditions was similar to the analysis completed for the existing conditions. The model was updated to reflect the proposed culvert improvements, as well as the floodplain benching locations.

4.2 SECONDARY SYSTEMS

Developing flood control alternatives for the secondary systems typically included increase in pipe capacity and/or rerouting flows where more space was available for improvements. In general, the proposed improvements for the secondary system are less complex from a permitting perspective since they typically do not require FEMA or 401/404 permits. However, the proposed improvements for secondary systems are oftentimes constrained by private property as space is typically limited between houses or other structures. Utility conflicts are another constraint that is typical for secondary system improvements. Secondary system improvements considered feedback from City staff and residents as well as maintenance needs based on findings from the inventory and/or feedback from City staff.

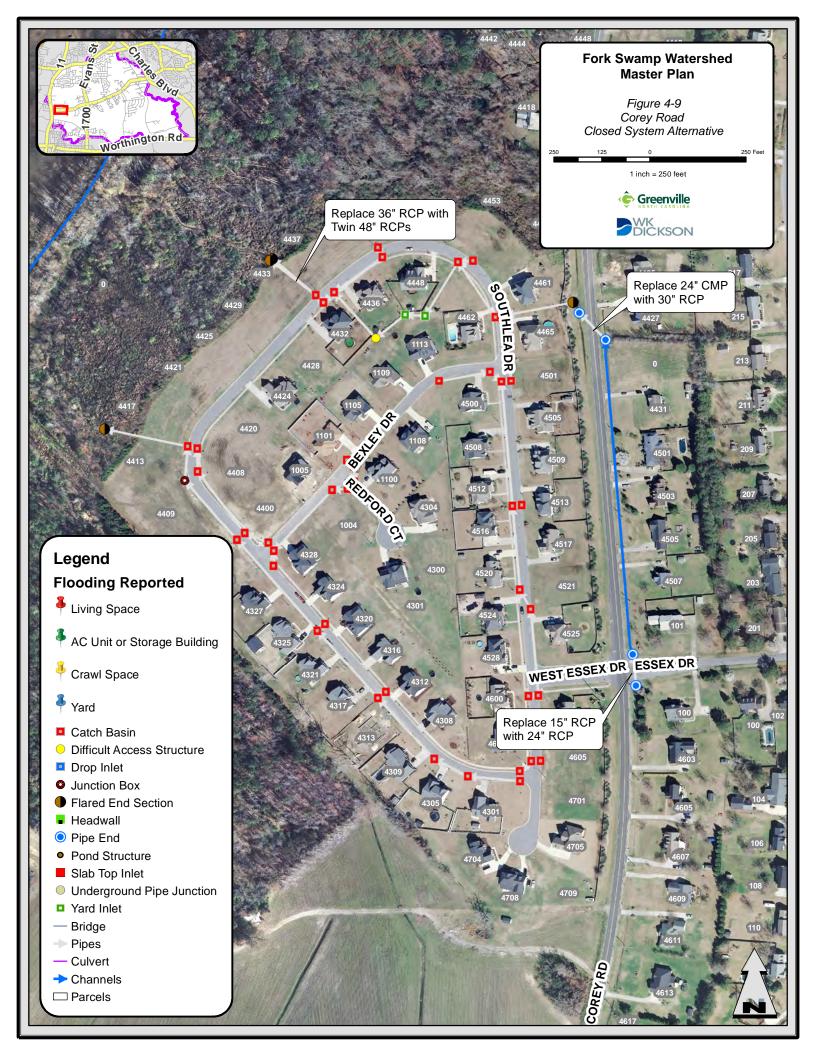
The projects described are the recommended alternatives for each of the secondary systems.

Corey Road Closed System

WK Dickson recommends the following improvements for the Corey Road Closed System as shown in Figure 4-9:

- Replace 147 linear feet of twin 36" RCPs with twin 48" RCPs along Southlea Drive;
- Replace 98 linear feet of 24" CMP with 30" RCP along Corey Road; and
- Replace 83 linear feet of 15" RCP with 24" RCP along Essex Drive (entrance of Windsor subdivision).

The proposed improvements will provide a 10-year level of service for the Corey Road Closed System including Essex Drive, a NCDOT secondary roadway. The majority of the project will be located in the right-of-way; there will minimal impacts to private properties. Sections of the curb and gutter along Southlea Drive will need to be removed and replaced as part of the proposed improvements. Underground electric, water, and sanitary sewer lines were also identified as potential site restrictions and utility conflicts. The total estimated cost for the recommended alternative is \$370,000.



SECTION 4: FLOOD MITIGATION ALTERNATIVES

Lynndale Closed System

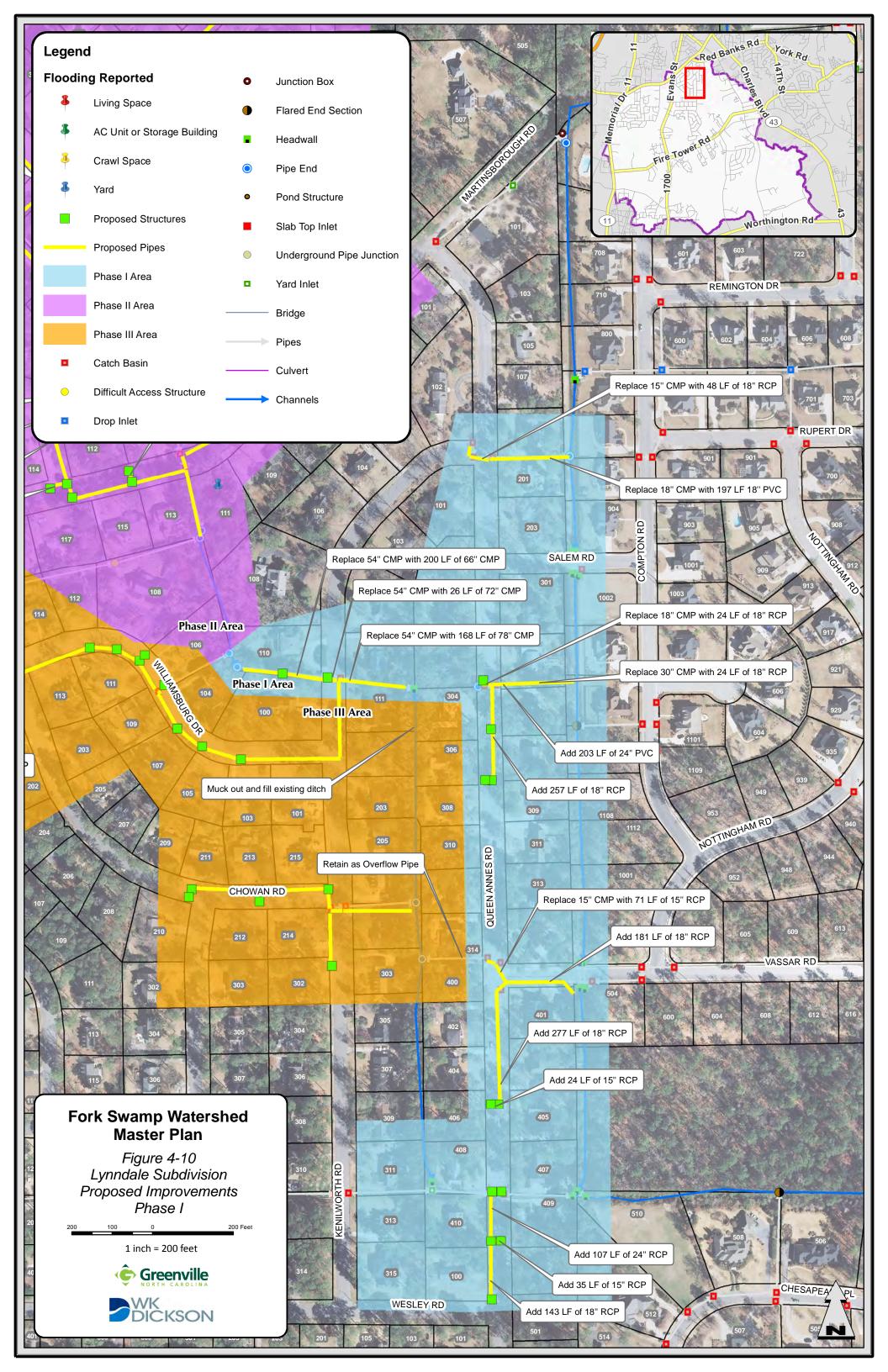
As previously mentioned, the Lynndale closed system was evaluated by River & Associates. It was not re-evaluated as part of this Master Plan. Preliminary design plans have been developed by Rivers & Associates. The design shown as Figure 4-10 through 4-13 summarizes the recommendations made by River & Associates.

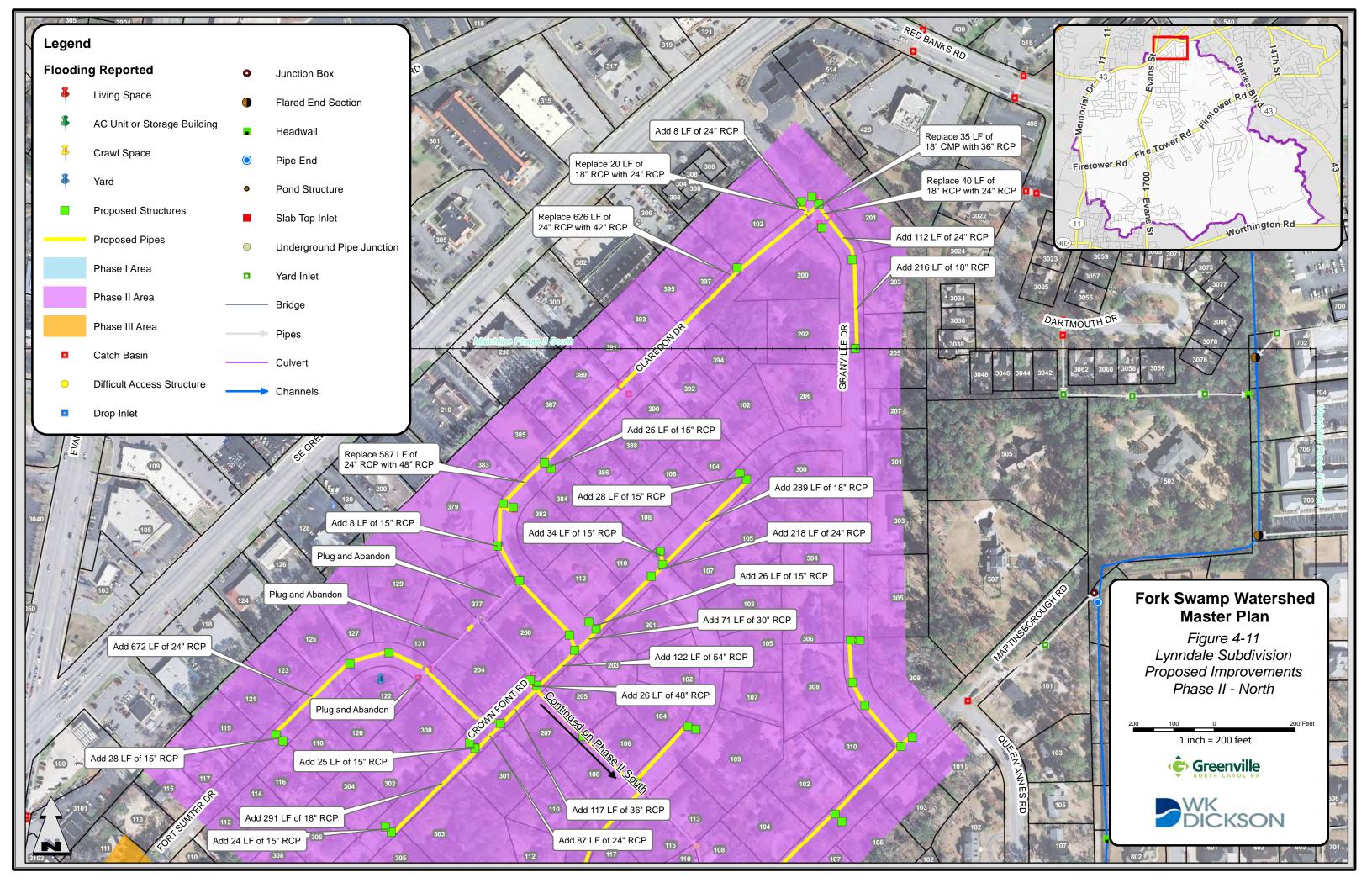
Based on the recommendations provided by the City via Rivers & Associates, WK Dickson developed costs estimates with the same unit costs used for other projects within this report. WK Dickson also included the Lynndale projects in the overall prioritization ranking for the Fork Swamp watershed. Due to the size of the project, the Lynndale system was divided into three phases as follows:

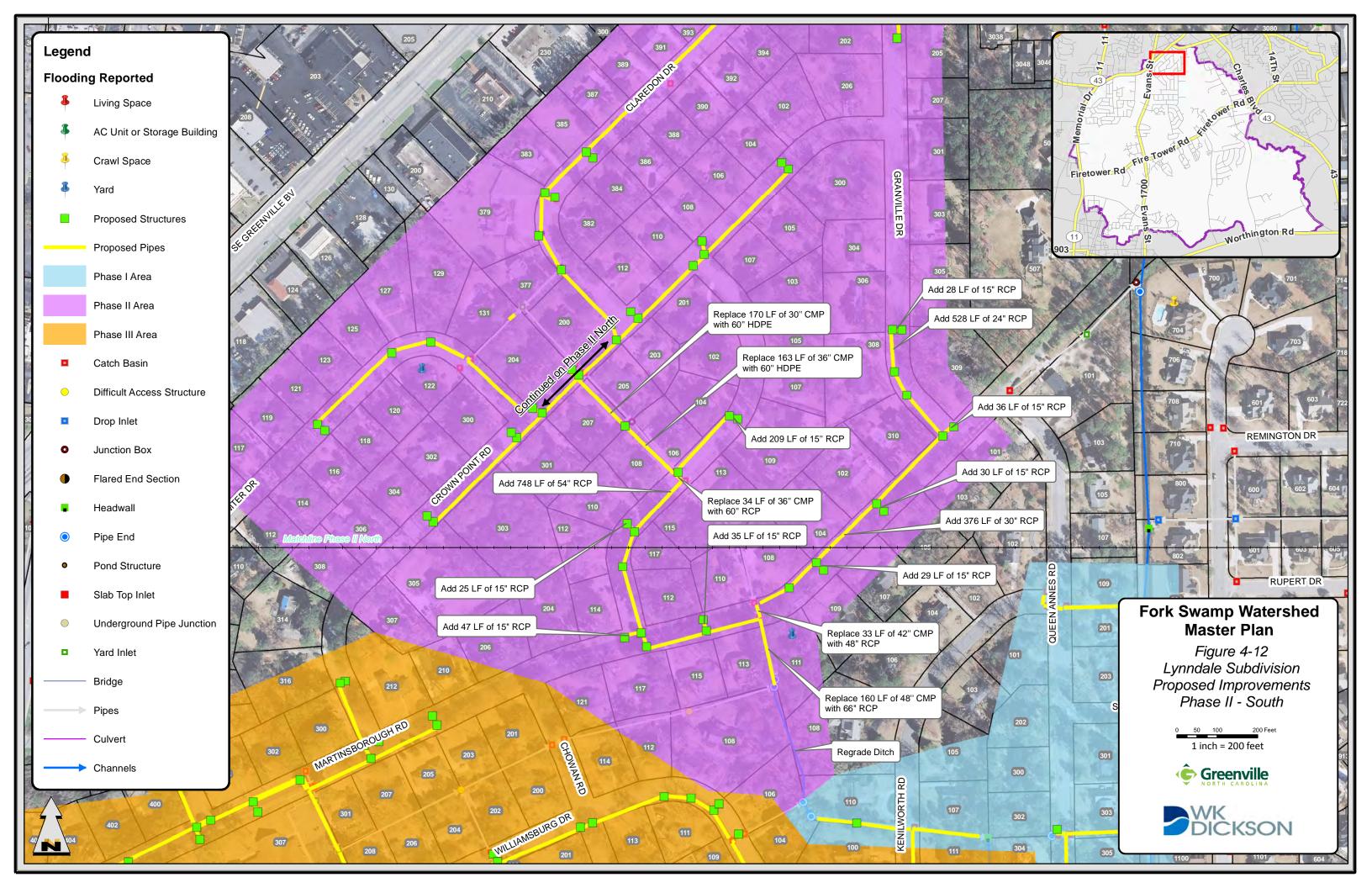
Phase I: Lynndale Phase I includes the downstream pipe improvements predominantly located along Queen Annes Road as shown on Figure 4-10. Estimated project costs are \$1,010,000 for Phase I. Utility conflicts are likely since the majority of the construction is located in the right-of-way. There will also be some private property impacts that will require drainage easements in locations that do not already have easements.

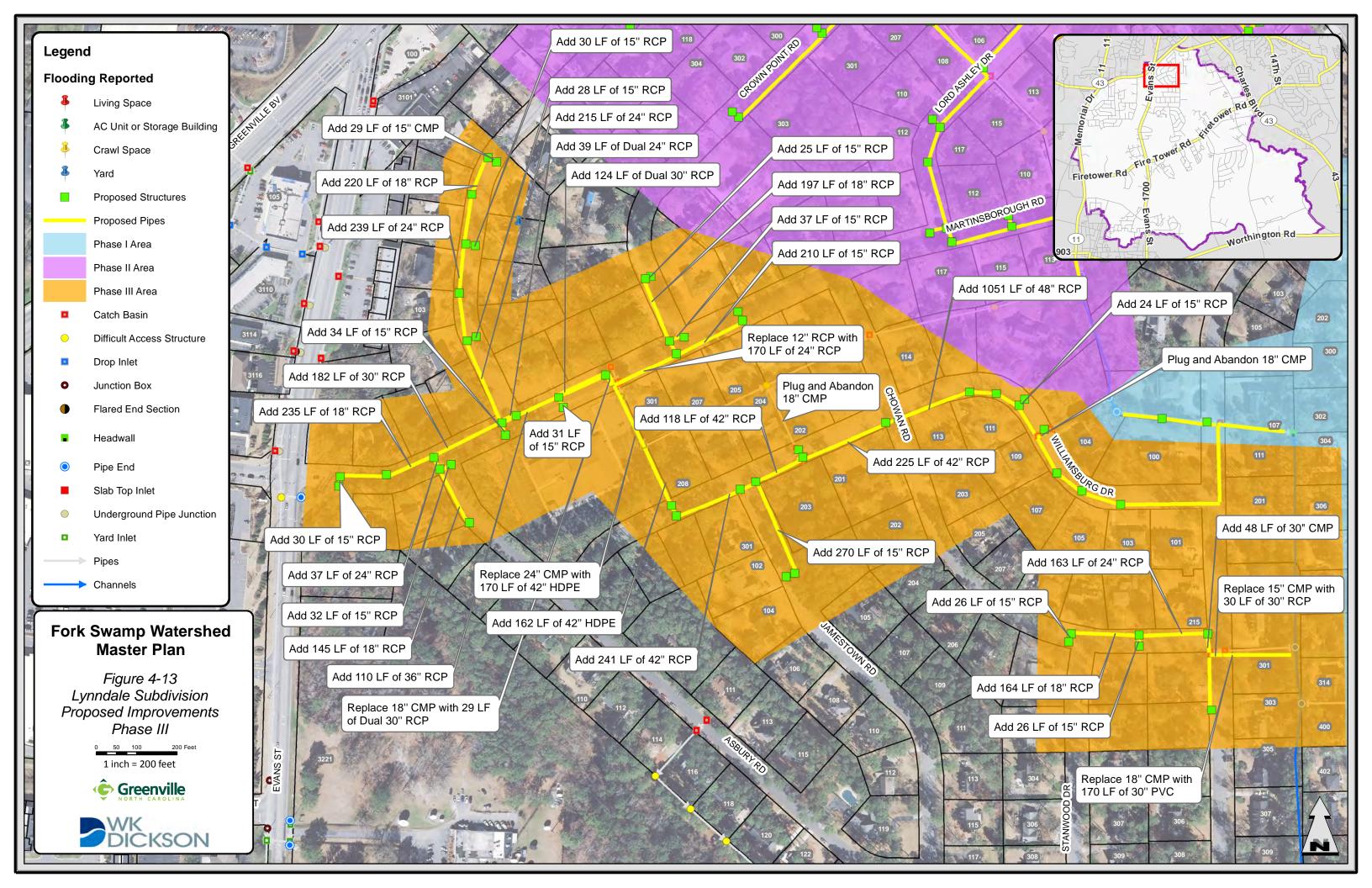
Phase II: Lynndale Phase II includes improvements in the northern portion of the neighborhood as shown in Figures 4-11 and 4-12. Improvements are located along Claredon Drive, Crown Point Road, Granville Drive, and Martinsborough Road. The majority of the improvements are located within the right-of-way, although some private property impacts will occur specifically between Crown Point Road and Lord Ashley Road. Estimated project costs are \$3,420,000 for Phase II. Phase II should only be completed after Phase I has been implemented.

Phase III: Lynndale Phase III includes improvements in the northern portion of the neighborhood as shown in Figure 4-13. Improvements are located along Fort Sumter Drive, Williamsburg Drive, Chowan Road, and Martinsborough Road. The majority of the improvements are located within the right-of-way. Estimated project costs are \$2,750,000 for Phase III. Phase III should only be completed after Phase I has been implemented, but can be constructed prior to Phase II if desired.









4.3 25-YEAR DETENTION ANALYSIS

In 2014, the City of Greenville enacted legislation requiring attenuation for new development and re-development for the one-year, five-year, and ten-year, 24-hour storm events. In addition, Section 9-9-10 of Ordinance No. 13-054 states the following:

"New development and redevelopment, as described in section 9-9-3, in areas at special risk with well documented water quantity problems as determined by the City Engineer, shall not result in a net increase in peak flow leaving the site from pre-development conditions for the 25-year, 24-hour storm event."

As part of the Fork Swamp Master Plan, an analysis was completed to determine if there are areas within the watershed and the ETJ that should be considered "well documented water quantity problems" requiring detention for the 25-year, 24-hour storm event. Areas may be defined as well documented water quantity problems if either of the following is true:

- Structural flooding has been historically noted by property owners during storms considered smaller than the design event and this structural flooding has been corroborated by either high water marks, City staff input, or model results.
- Model results indicate structural flooding or roadway overtopping during storms smaller than the design storm and model results are corroborated by City staff input.

Portions of the watershed draining to the "well documented water quantity problems" may be considered for 25-year detention if any of the following are true:

- Future condition flows are 10% or greater than existing flows for a given subwatershed upstream of the water quantity problem.
- Proposed capital projects are not deemed to be feasible or cost effective for providing the required level of service for these water quantity problems based on future land use conditions.
- Cost differential between designing for existing conditions and future conditions is deemed to be significant and/or a significant number of structures would become floodprone during the 25-year design storm based on future conditions flows when compared to existing conditions flows.

It is assumed that for this analysis, systems with a 10-year level of service design would not be considered for the 25-year detention since the existing 10-year detention requirements would result in little to no increase in peak flows for the design event. The secondary systems evaluated in Fork Swamp watershed only required a 10-year level of service, therefore requiring upstream 25-year detention would not impact the design of a system that only needs to meet a 10-year design storm.

As noted in Section 3.1, documented flooding issues are located along Fork Swamp Main Branch, Unnamed Tributary 3, and Unnamed Tributary 1 including the area between Baywood

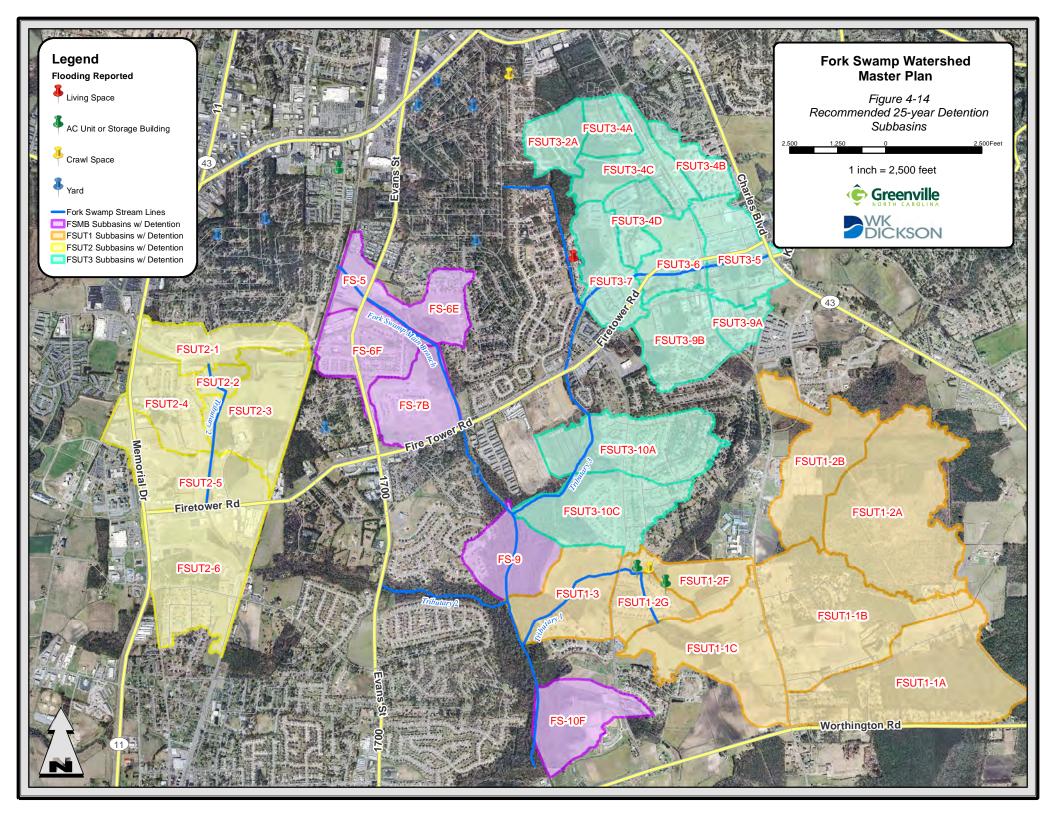
Lane and Treetops Circle along Fork Swamp Main Branch, the area between Corey Road and Trafalgar Drive along Unnamed Tributary 1, and the area between East Fire Tower Road and County Home Road along Unnamed Tributary 3. Large portions of the Fork Swamp watershed are already fully developed, however there are some areas of the watershed where the future conditions 25-year flows could be greater than 10% higher than the current existing flows. These areas are shown in Figure 4-14.

For the purposes of evaluating if 25-year detention is appropriate, the Fork Swamp watershed is divided into four (4) distinct areas based on the drainage feature that conveys runoff from that area. Then the entire Fork Swamp watershed needs to be evaluated to limit increases in runoff from the south end of the City limits entering neighboring communities.

- Fork Swamp Main Stem Flooding issues along the Fork Swamp Main Stem are predominantly located in the upstream portion of the watershed from the vicinity of East Fire Tower Road up through Baywood Lane and the Westhaven subdivision. The contributing drainage area to these locations is fully developed with the exception of some areas along Evans Road and north of East Fire Tower Road. Requiring 25-year detention in these areas will not substantially impact the proposed capital projects along Fork Swamp Main Stem however since existing flooding problems have been documented in these areas, it is recommended that the highlighted drainage basins shown in the Figure 4-14 within the Fork Swamp Main Stem drainage area require 25-year detention.
- Fork Swamp Tributary 1 Repetitive flooding has been reported within the Farrington subdivision specifically on Trafalgar Drive along Fork Swamp Tributary 1. Each of the highlighted areas shown in Figure 4-14 have the potential for the 25-year flows to increase by greater than 10% due to the potential future development in these areas. The future condition land use was based on existing zoning. The City should carefully consider rezoning requests within the Fork Swamp Tributary 1 watershed based on the existing known flooding issues. If 25-year detention is required in the proposed areas, the recommended culvert sizes at Trafalgar Drive can be decreased, although the cost savings would not be substantial. However, the severity, frequency, and duration of flooding would be reduced, which would in return provide savings to the property owners.
- Fork Swamp Tributary 2 The highlighted areas shown in the western portion of the watershed in Figure 4-14 all have the potential for future development that would result in increases greater than 10% in the 25-year peak development flows. While floodprone areas were not identified within the City limits in Tributary 2, the crossing at Old Tar Road downstream outside of the City's jurisdiction is floodprone. Furthermore, 25-year detention in these areas would reduce the increase in runoff at the City boundary under future development conditions.

SECTION 4: FLOOD MITIGATION ALTERNATIVES

- Fork Swamp Tributary 3 The majority of the culvert crossings along Fork Swamp Tributary 3 do not meet the desired level of service for existing conditions and in several locations there is a limited natural floodplain. Furthermore, significant stream erosion has already occurred throughout Tributary 3. The areas shown in Figure 4-14 should be considered for 25-year detention to minimize the size of the culvert improvements to the extent possible. While 25-year detention will not eliminate the need for culvert improvements in the area, the size of the culverts could be reduced in some areas which is particularly valuable given the tight constraints. The areas highlighted in Figure 4-14 have the potential for increasing the 25-year flows greater than 10% in future conditions when compared to existing.
- Overall Fork Swamp watershed Changes in land use (future build-out conditions) and increasing culvert capacity will increase the 25-year flow at the outlet of the study area (City limits) by approximately 8%, resulting in a 0.22-foot increase in WSEL at the outlet. Downstream communities including Winterville and Pitt County already experience flooding along Fork Swamp in existing conditions, so any increase in flows could potentially increase the duration, severity, and frequency of flooding, although the limits of this study do not evaluate these potential impacts downstream of the City limits. If 25-year detention was required in the highlighted areas in Figure 4-14, the increase in the 25-year flow would be reduced to 1.1%, a reduction in WSEL of 0.17 foot. Therefore, the City could significantly reduce the size of the Corey Road Regional Detention Area described in Section 4.1.6 to effectively ensure no net increase in the 25-year peak flow at the limits of the study. The size of the detention area could be reduced to eight (8) acres which would reduce the cost to \$2,670,000, which is approximately \$5 million less than the original cost of \$7 million.



WATER QUALITY RECOMMENDATIONS

Traditional stormwater management has typically been designed to reduce flooding, but at times has neglected water quality by collecting runoff directly from impervious surfaces into a closed drainage system. Runoff from impervious areas collects high concentrations of pollutants and nutrients that if left untreated can cause negative impacts to water quality in the receiving waters. Negative impacts may include less biodiversity, hazards to the health of fish and wildlife, as well as human health hazards. Many communities in North Carolina now require some form of water quality treatment for new development; however existing developments typically have little or no water quality treatment. The City of Greenville developed a Stormwater Management Program (September, 2004) to outline its water quality requirements.

Best management practices (BMPs) can be constructed to treat runoff prior to being discharged to the stormwater conveyance system and ultimately the receiving waters of the system. Retrofitting BMPs can be difficult due to limited space and other constraints. Several types of BMPs were evaluated: Bioretention Cells, Stormwater Wetlands, Wet Pond Retrofit, Regenerative Stormwater Conveyance (RSC), Rainwater Harvesting, Permeable Pavement, and Water Quality Swales. Projects identified in the Fork Swamp watershed are described below.

5.1 STREAM STABILIZATION PROJECTS

Based on the basin-wide stream assessment completed as described in Section 3.3, seven (7) stream stabilization projects were identified to help reduce instream erosion. Instream erosion can be a significant source of sediment that ultimately can impair the biodiversity of the downstream receiving waterbodies. Furthermore, in urban watersheds such as Fork Swamp, stream erosion is often a threat to private property and potentially the safety of structures adjacent to the stream. The proposed stream stabilization projects will have impacts to property owners that will require temporary construction easements to complete the work and permanent easements for maintenance access. Proposed projects assume that the riparian buffers can be restored to existing conditions. During final design, the City will need to refer to the current buffer regulations to determine if more significant buffer restoration is required. The projects (not presented in order of importance) are described as follows:

Stream Stabilization Project #1: Live Oak Lane

The Live Oak Lane Project is located east of Evans Street behind the residential properties on Live Oak Lane, upstream of Paramore Park. Stream Stabilization Project #1 begins to the east of Keys Court and runs approximately 1,600 feet downstream along the greenway. The project is located along a third order perennial section of Fork Swamp. As shown on Figure 5-1, this project also includes a highly eroded channel that begins downstream of a 54" RCP culvert just east of Live Oak Lane. This project has a drainage area of approximately 1,100 acres. The most downstream portion of the project lies within the FEMA 100-year floodway.

The project flows to the southeast and is confined within a steep eroded channel feature. Land use immediately surrounding the project is mostly residential with wooded reaches and maintained open area along the channel. The bank conditions are unstable and eroding at an accelerated pace due to loamy sand soil texture and a lack of sufficient bank vegetation along large portions of this reach. The bottom width is approximately 8 feet wide. The right bank is 4.5 feet tall and the left bank is approximately 7 feet tall with bank angles of 70 degrees. The



Picture 5-1. Perched outlet on left bank of Fork Swamp

average top channel width is 12 feet wide. Shear stress and channel velocities are above the ideal conditions for a stable sand bed channel, with values reaching 0.48 lb/sq ft, and 3.47 ft/s, respectively. This deeply confined channel has led to a perched outfall (See Picture 5-1) and rapid erosion along a meander of the left bank of the stream. The bank conditions along the channel draining from Live Oak Lane are also unstable and eroding due to loamy sand soil texture and a lack of sufficient bank protection along the right bank (See Picture 5-2).

The proposed project reach has opportunities for stream stabilization to prevent sediment loading and bank erosion to Fork Swamp. The existing greenway and sewer easement adjacent to this stream segment would make this project easily accessible. To improve bank stability and reduce bank erosion, several tasks could be performed. For both reaches, bank erosion can be reduced by constructing a low flow channel with additional floodplain storage, grading the channel banks back to a minimum 2 to 1 slope, and placing coir erosion control matting along banks and bare areas. In some areas along the greenway, a reinforced retaining wall may be used to restrict the stream



Picture 5-2. View from culvert at Live Oak Lane looking towards Fork Swamp

from widening towards the existing greenway trail. Downstream of the culvert at Live Oak Lane (ID #FSMB020122), the stream bed should be reinforced by installing an energy dissipater or a riffle grade control structure composed of mixed riprap on filter fabric and located below the stream bed. Once installed, the riffle will act as a grade control below the downstream headwall, which will protect it from being undercut. To reduce water velocity and help stabilize the streambed along both reaches, rock structures can be placed within the stream bed at the toe of the bank. Live staking stream banks along both reaches will also help prevent undercutting and bank failures in the future.

The estimated cost for the Live Oak project is \$280,000. The stream stabilization project will run along the backside of several private properties, therefore there may be potential impacts to landscaping and fencing at the following properties:

- 3600 Live Oak Lane;
- 3601 Live Oak Lane;
- 3602 Live Oak Lane;
- 3604 Live Oak Lane;
- 3606 Live Oak Lane; and
- 161 Keys Court (The Trellis Apartments).

Additionally, it should be noted that the project is located within a Pitt County drainage easement. Implementation of this project would require coordination between the City and County. This could impact its overall prioritization rating.



Picture 5-3. Eroding bank at 1205 Trafalgar Drive

Date of the state of the state

am Project #2 is a first order perennial stream section of an unnamed tributary to Fork Swamp. The project includes 400 feet of stabilization in the neighborhood east of Corey Road and approximately 1,450 feet of stabilization and buffer restoration to the west of Corey Road. The drainage area for the project is approximately 1,500 acres. The portion of the project west of Corey Road lies in the FEMA 100-year floodplain.

Stream Project #2 flows in a southwesterly direction before running through a wooded stream segment that leads to the confluence with

Stream Stabilization Project # 2: Corey Road

Stream Project #2 begins in a residential neighborhood along Trafalgar Drive, crosses Corey Road, and runs downstream through an agricultural field. It is not located within the City limits, but is included in the ETJ, therefore this project was not prioritized along with the other proposed projects located in the City. However, Stream Project #2 is still included because it will provide benefits to City residents.



Picture 5-4. Erosion and lack of riparian buffer downstream of Corey Road

Fork Swamp. The average bottom width along this reach is 12.5 feet and both banks are roughly 4.5 tall. The bank angles are near 65 degrees. The average top channel width along this stretch

is 15 feet. Upstream of Corey Road, the surrounding land use is entirely residential. This section of stream has a minimal riparian buffer along the right bank and the left bank is maintained, residential lawn. As shown in Picture 5-3, the erosion along the left bank is encroaching on the landowner's fence at 1205 Trafalgar Drive. The proposed stabilization continues downstream of the culvert at Corey Road, where the stream flows through an unbuffered agricultural field.

While the culvert is in good condition, shear stress and channel velocities below the culvert are above the ideal conditions for a stable sand bed channel, with values reaching 1.19 lb/sq ft, and 6.32 ft/s, respectively. The agricultural field downstream of the culvert is devoid of any riparian vegetation and there is evidence of slumping banks in many areas (See Picture 5-4). Bank conditions are currently unstable due to a loamy sand soil texture, lack of sufficient bank vegetation, and the lack of a forested buffer on either bank.

Stream Project #2 has opportunities for bank stabilization to prevent bank erosion and sediment loading along to Fork Swamp. Upstream of Corey Road, bank erosion can be reduced by grading channel banks back to a minimum 2 to 1 slope and placing coir matting along banks and bare areas. An open lot (Parcel # 062704) between residential properties on Trafalgar Drive provides good access to this site. Live staking the stream banks along this bend and planting the area with a riparian seed mix will also help prevent future erosion and sediment loading to the channel.

The stream section downstream of the culvert at Corey Road offers the potential for a compensatory mitigation project through the North Carolina Division of Mitigation Services (NC DMS) or private banker. The most likely scenario would involve a stream enhancement and/or nutrient and buffer mitigation project which employs rehabilitation activities to improve water quality and the ecological function of a fluvial system. Examples of stream enhancement could include sloping of stream banks to restore appropriate dimensions, the construction of grade-control structures to stabilize banks, and planting the riparian zones with native vegetation. Live staking stream banks and planting of hardwood species will help prevent undercutting and bank failures in the future and benefit downstream portions of the watershed.

The stream stabilization project upstream of the Corey Road culvert will run along the backside of several private properties, therefore there may be potential impacts to landscaping and fencing at the following properties:

- 1201 Trafalgar Drive;
- 1203 Trafalgar Drive;
- 1205 Trafalgar Drive; and
- 1207 Trafalgar Drive.

The potential mitigation project downstream of the culvert would require coordination with the landowners of Parcels #25822 and #08367 to assure long-term management of the restored site through a protection mechanism such as a conservation easement.

The estimated cost for the Corey Road project is \$590,000. It should be noted that the City may realize some cost savings by combining the Corey Road stabilization project with the proposed flood control work upstream and downstream of Corey Road.

Stream Stabilization Project # 3: East Fire Tower Road

Stream Project #3 is located north of East Fire Tower Road near the intersection of Ashcroft Drive and Coleman Drive. The project starts behind the homes on Ashcroft Drive and runs approximately 1,000 feet to the bridge at East Fire Tower Road. Stream Project #3 is a perennial stream section of FSUT3 with a drainage area of 889 acres. In addition to the stabilization along

the main channel, this project will also address the severely eroded drainage ditch entering the stream from the parking lot of Bella Salon.

Land use surrounding the project consists mainly of residential neighborhoods and small business in the immediate area. Stream Project #3 flows to the southwest with average bank heights of 5 feet and average bank angles of 50 degrees. This channel does not have a forested buffer. The bank conditions along this stretch are fairly unstable and eroding at an accelerated pace due to loamy sand soil texture and a lack of sufficient bank vegetation along large portions of this urbanized reach.



Picture 5-5. Highly eroded ditch at East Fire Tower Road

Stream Project #3 has opportunities for bank stabilization to prevent the banks from eroding at such an accelerated rate. This project can easily be accessed from East Fire Tower Road or Ashcroft Drive. Bank erosion can be reduced along the main stem and downstream of the Ashcroft outfall by placing coir erosion control matting along banks and bare areas and



Picture 5-6. Erosion and lack of riparian buffer at Ashcroft outfall

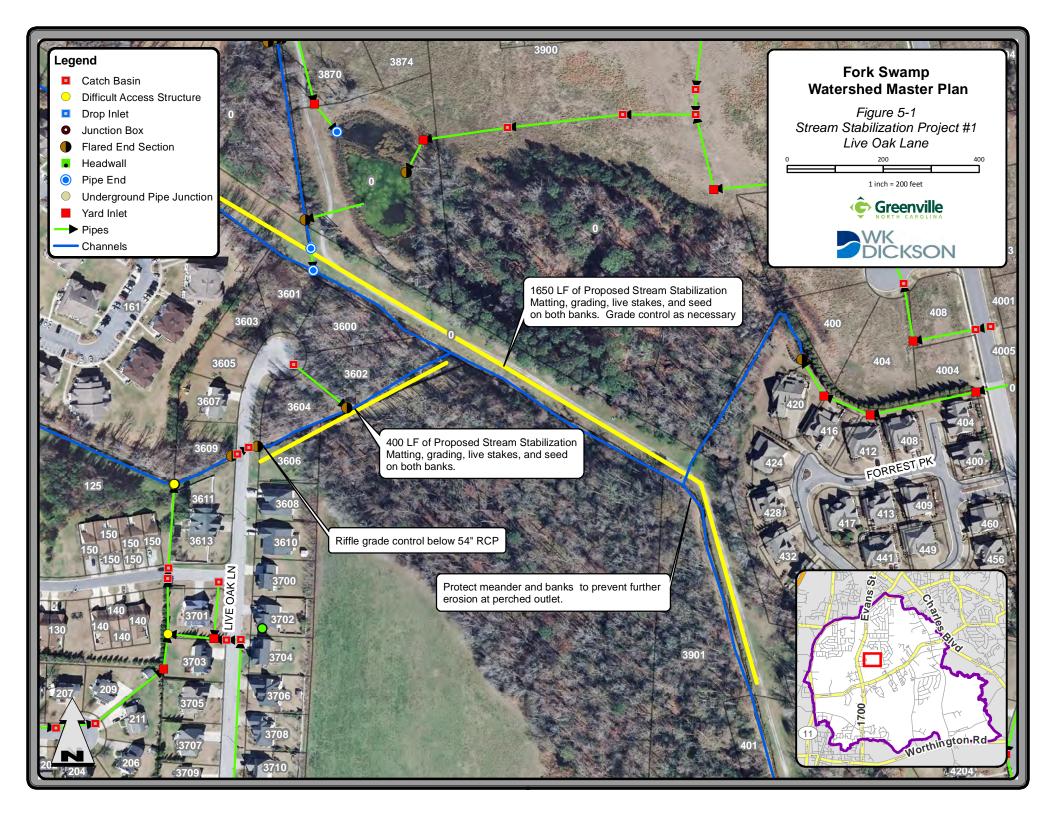
planting the entire project area with a riparian seed mix to reinforce banks. Live staking stream banks will also help alleviate future erosion. drainage ditch in the Bella Salon Parking Lot would be a potential site for a stormwater best management practice (BMP), such regenerative stormwater conveyance (RSC) system. RSC systems are capable of conveying, storing, and runoff through infiltration, filtration, and detention. RSCs are a linear system of riffles and step pools filled with a porous, carbon-rich bed material where pollutant removal processes may take place physically as well as biologically. The pools provide volume for runoff

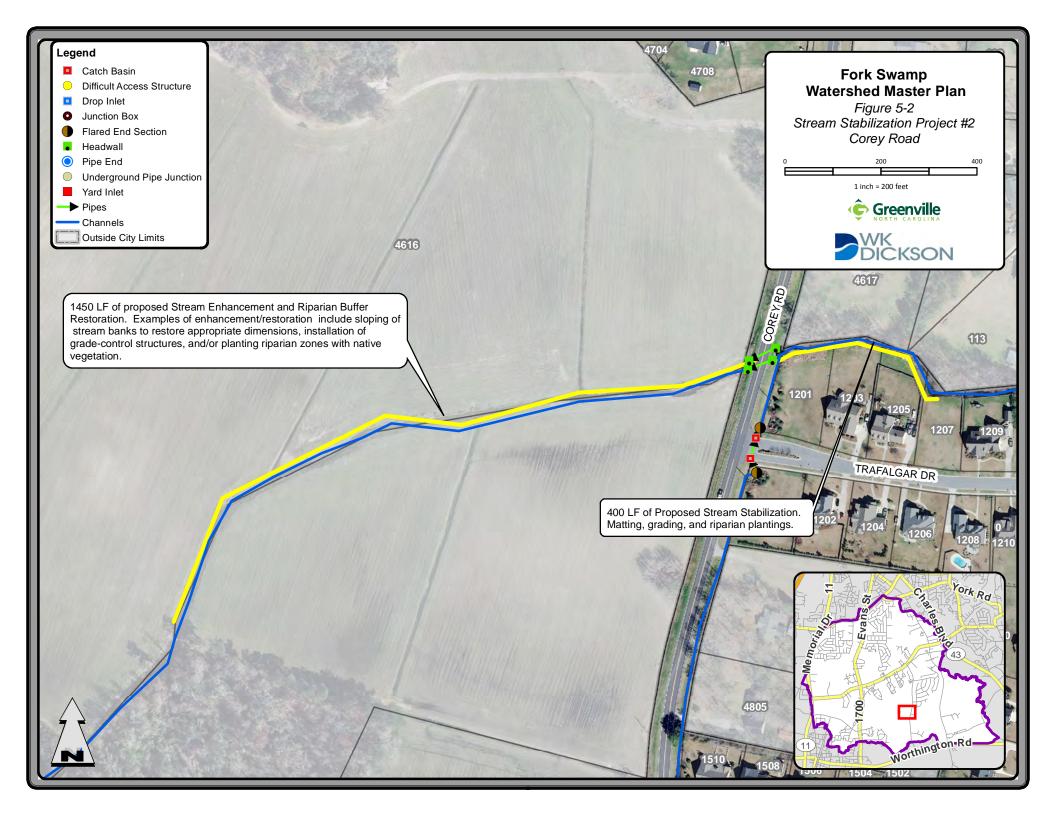
detention and infiltration, while the series of riffles are helpful in providing grade control for areas where steep slopes have caused instances of deep rill erosion or failed stream banks. RSCs can be very helpful in mitigating peak flows, as well as stabilizing channels and stream banks.

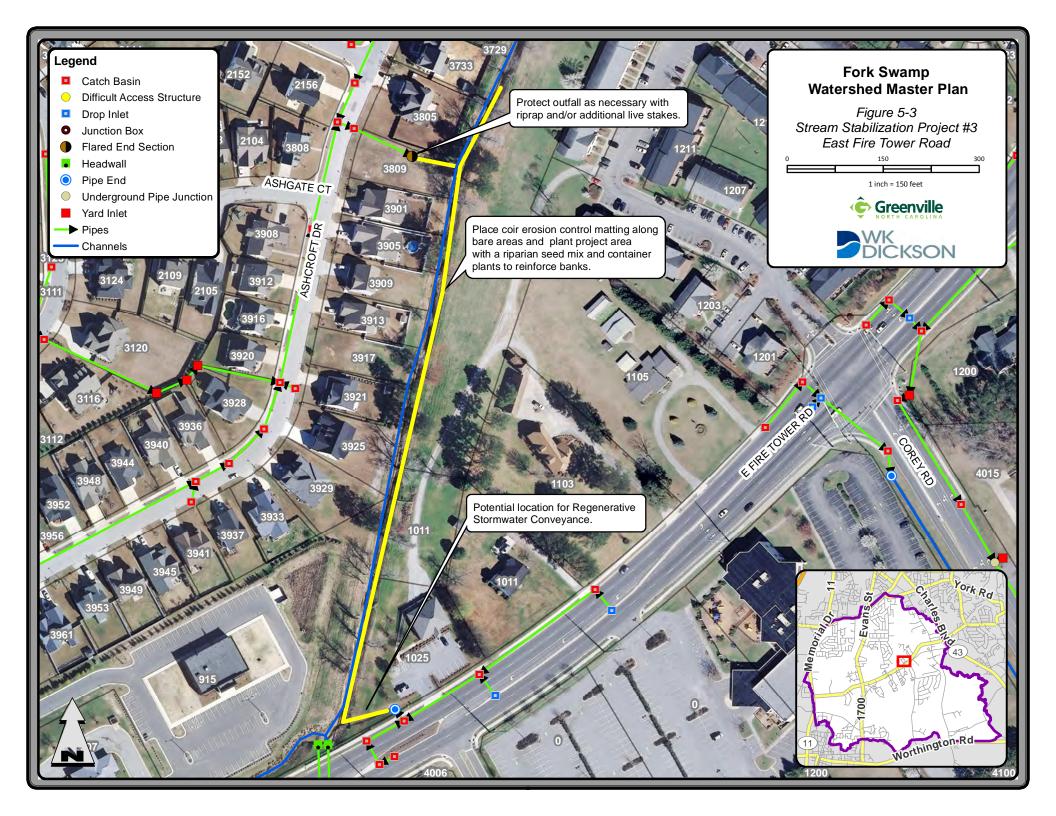
This stream stabilization project could potentially be combined with the proposed floodplain benching along FSUT3 upstream and downstream of East Fire Tower Road as well as the proposed culvert improvements at East Fire Tower Road.

The estimated cost for the East Fire Tower stream stabilization project is \$230,000. The stream stabilization project will potentially access the project at the Ashcroft outfall (#FSUT030266). The following properties may be affected:

- 3805 Ashcroft Drive; and
- 3809 Ashcroft Drive.







Stream Stabilization Project #4: Tower Place

Stream Project #4 runs between Summerhaven Drive and Wimbledon Drive. The project begins behind an apartment complex and runs approximately 550 feet to the crossing at Tower Place. Stream Project #4 is a perennial stream section of FSUT3 with a drainage area of 476 acres.

Land use surrounding Stream Project #4 is mostly residential. This stream segment flows to the west and has an average stream width of 8 feet. The average bank height ranges between 4 and 7 feet and average bank angles are 65 degrees. Bank conditions along this stretch are fairly unstable and eroding due to the lack of a forested buffer along the entire reach. The left bank is a maintained lawn and has nearly 30 continuous feet of slumping banks. The lack of riparian vegetation along this stretch is likely to lead to erosion that may begin to encroach on the apartment complex in the future.



Picture 5-6. Erosion East of Tower Place

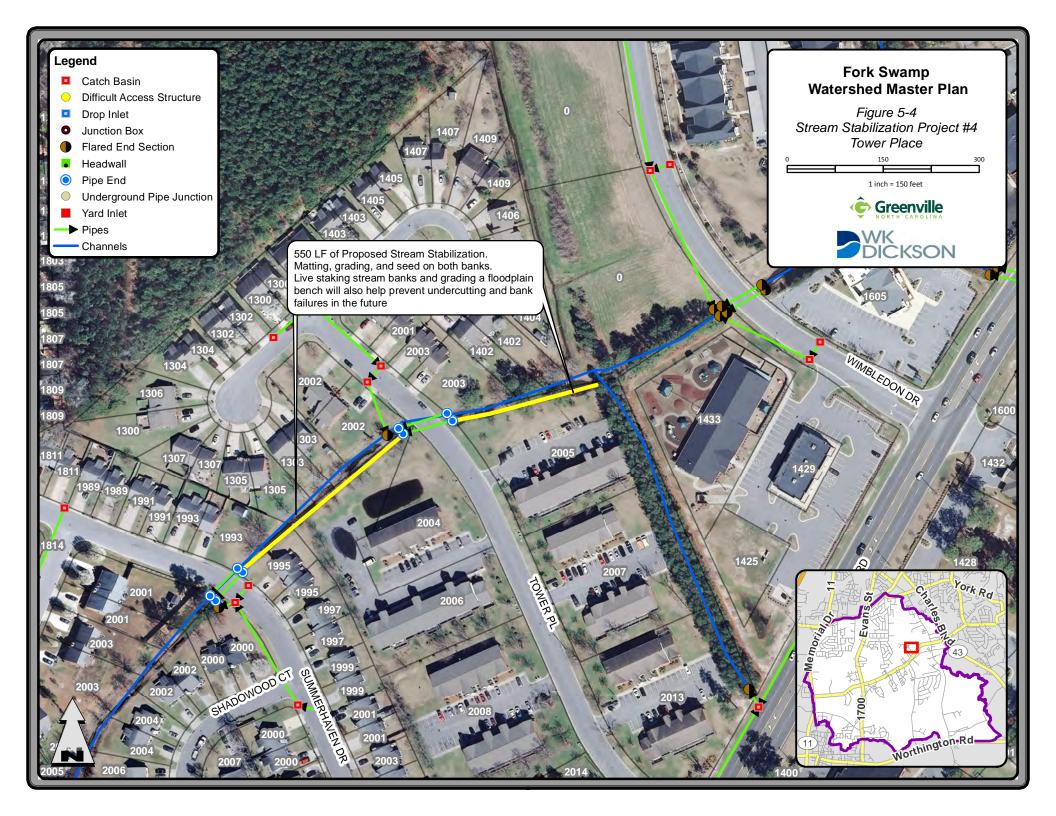
Stream Project #4 has opportunities for bank stabilization to prevent sediment loading and



Picture 5-7. Erosion East of Tower Place

bank erosion to this unnamed tributary. To improve bank stability and reduce bank erosion along Stream Project #4, several tasks could be performed. Bank erosion can be reduced by grading channel banks back to a minimum 2 to 1 slope and placement of coir erosion control matting along banks and bare areas. Live staking stream banks and grading a floodplain bench will also help prevent undercutting and bank failures in the future. Also, the entire project area could be planted with a riparian seed mix to reinforce banks. The estimated cost for the Tower Place project is \$140,000. If funding allows this stream

stabilization project could be combined with the proposed culvert improvements at Summerhaven Drive, Tower Place, and Wimbledon Drive.



Stream Stabilization Project #5: Charles Boulevard

Stream Project #5 begins west of Charles Boulevard at an incised tributary and runs 300 feet down to a perched culvert with an obstruction and pool formed. Stream Project #5 is a perennial stream section of FSUT3 with a drainage area of approximately 100 acres.

Land use surrounding Stream Project #5 is mostly small businesses and some residential areas downstream. This stream segment flows to the west and has an average stream width of 8 feet. The average bank height ranges between 4 and 7 feet and average bank angles are 65 degrees. The bank conditions along this stretch are fairly unstable and eroding at an accelerated pace

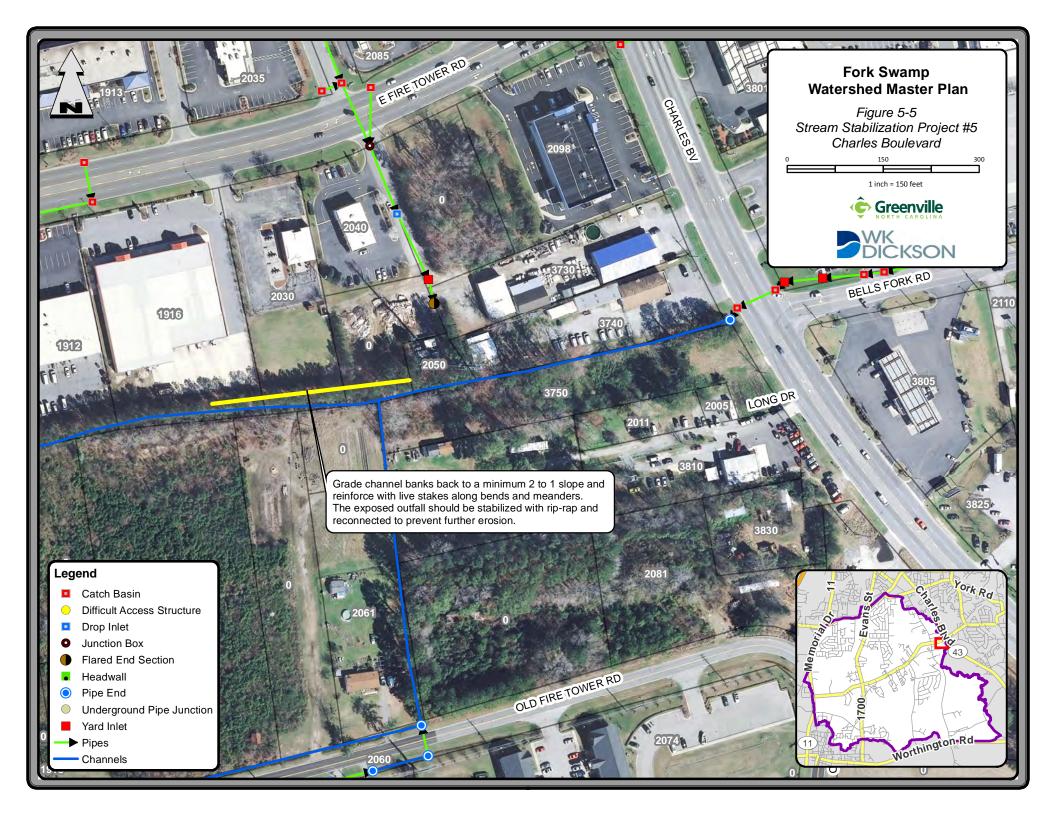
due to loamy sand soil texture and a lack of sufficient bank vegetation along large portions of this urbanized reach. Erosion and debris obstructions in this segment have led to a perched culvert that could become further exposed if not addressed.

Stream Project #5 has opportunities for bank stabilization and the stabilization of a perched outfall. To improve bank stability and reduce bank erosion along Stream Project #5, several tasks need to be performed. Bank erosion can be reduced by reinforcing banks with live stakes and debris



Picture 5-8. Exposed outfall on right bank

jams in the channel should be removed to prevent channel widening and erosion of banks near the exposed outfall. Several tasks could be performed to stabilize the outfall: the outfall could be stabilized with rip-rap and reconnected to prevent further erosion or a cross vane could be constructed just upstream of the outfall to help establish a pool just below the pipe end. Additionally, the outfall elevation could be lowered or outfall treatment such as RSC could be installed. The estimated cost for the Charles Boulevard project is \$90,000.



Stream Stabilization Project # 6: Queen Annes Road

Stream Project #6 is located east of Queen Annes Road and north of the houses on Chesapeake Place. Stream Project #6 begins downstream of an armored culvert and runs approximately 500 feet downstream to an armored 90-degree bend in the channel. Stream Project #6 is a perennial stream section of FSUT1 and has a drainage area of approximately 220 acres.

Stream Project #6 flows to the east within a channelized segment of the stream. Land use surrounding the project is mostly residential with reaches of wooded area along the sewer easement. The bottom width is approximately 10 feet wide. The right bank is 10 feet tall and the left bank is approximately 15 feet tall with bank angles of 65 degrees. The bank conditions along this stretch are unstable and eroding due to a lack of sufficient bank protection along this portion of the reach (See Picture 5-9).



Picture 5-9. Eroding left bank between armored sections

Immediately upstream and downstream of this project the left bank is heavily armored with rip-

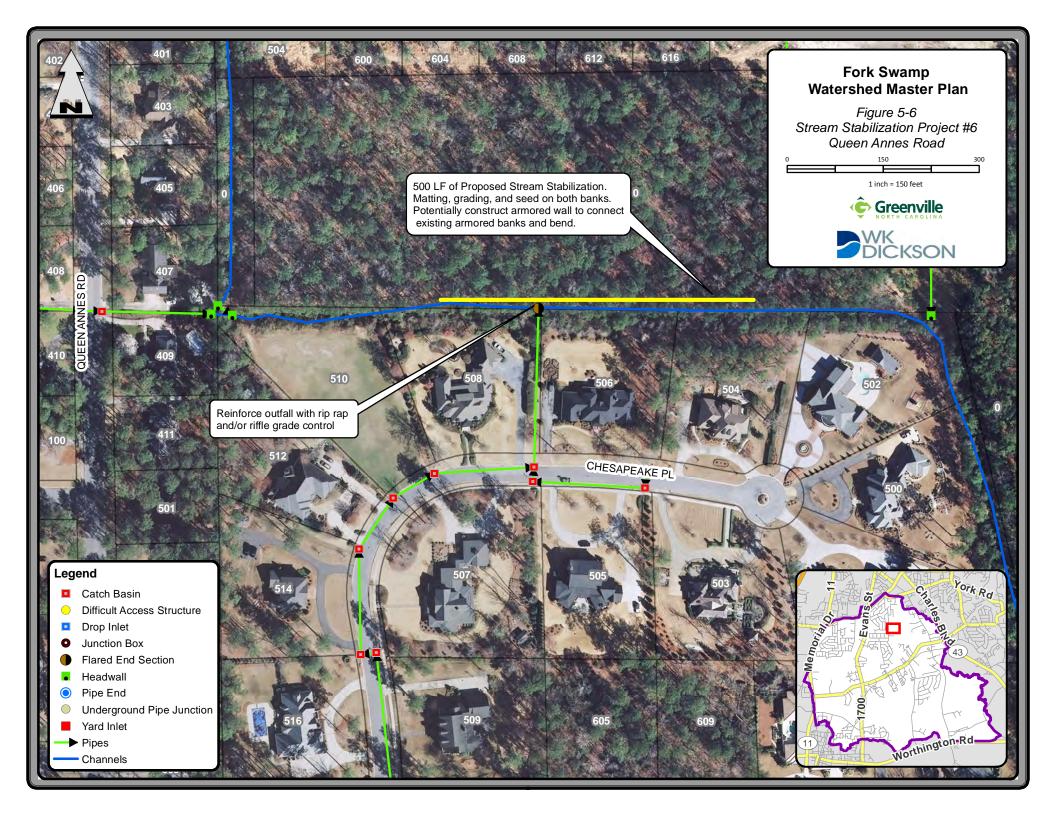
rap (See Picture 5-10). It also appears that log grade control structures previously placed along the right bank are failing (See Picture 5-11). Proposed work would include stream stabilization and potentially connecting the two already armored features along this stretch of FSUT1. To improve bank stability and reduce bank erosion along Stream Project #6, several tasks could be performed. Live staking stream banks or reinforcing banks with riprap along bends and meanders will help prevent undercutting and bank failures in the future. The City might consider reinforcing the entire reach to connect the already enforced segments of the stream. The estimated cost for the Queen Annes Road project is \$220,000.



Picture 5-10. Armored 90-degree bend



Picture 5-11. Failing log structures along right bank



Stream Stabilization Project #7: Evans Street

Stream Project #7 is located adjacent to the residence at 3307 Evans Street, where erosion at a stormwater outfall has caused severe erosion and exposed the footing of a telephone pole (See Picture 5-12). In addition to stabilizing the outfall at Evans Street, Stream Project #7 would span approximately 400 feet downstream of the culvert to address unstable conditions along this channel. Stream Project #7 is a perennial stream section and has a drainage area of approximately 125 acres.

Land use surrounding the project is mostly residential. Stream Project #7 flows to the east

within a channelized segment and then turns 90 degrees to flow to the south. The bottom width is approximately 5 feet wide. The right bank is 5.5 feet tall and the left bank is approximately 7 feet tall with bank angles of 65 degrees. The bank conditions along this stretch are unstable and eroding due to loamy sand soil texture and a lack of sufficient bank protection along this portion of the reach. The landowner at 3307 Evans Street has installed fencing Stream Project #7 in an effort to stabilize the banks and hinder future erosion.



Picture 5-12. Eroding outfall and exposed telephone pole

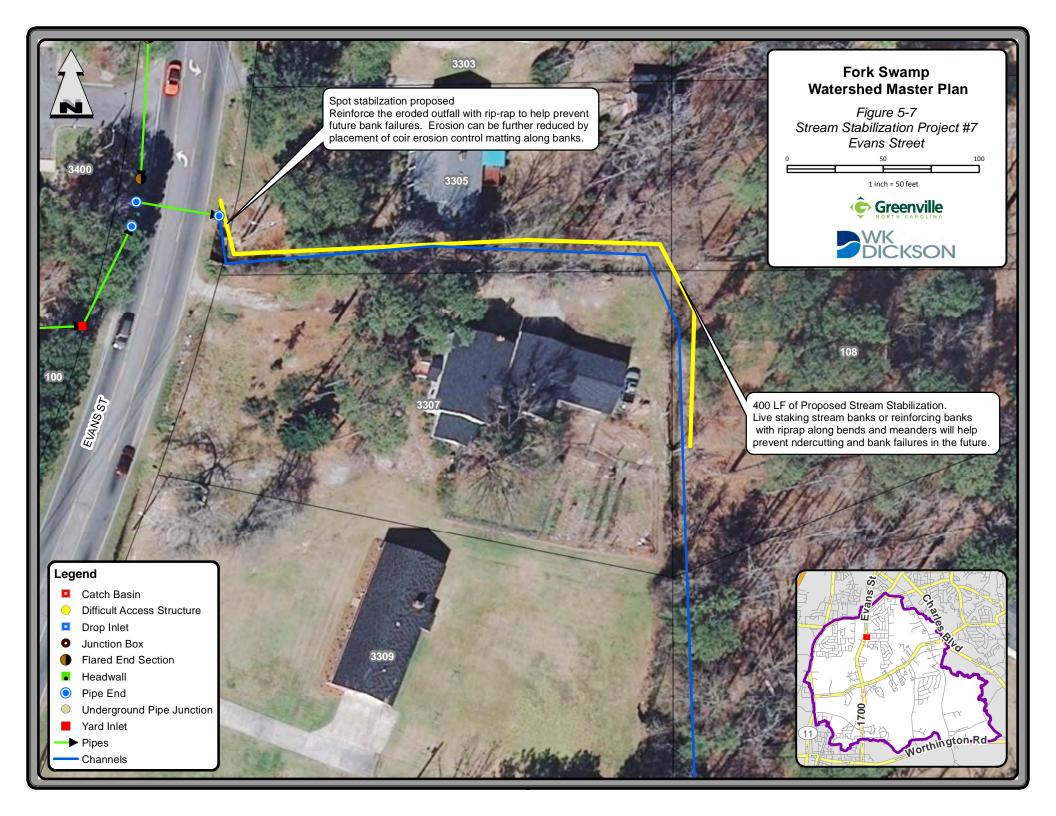
Stream Project #7 has opportunities for bank stabilization to prevent increased erosion at the

outfall and preventing the telephone pole from collapsing. Proposed work at the outfall could



Picture 5-13. Vertical stream bank behind property at 3307 Evans Street

include reinforcing the channel banks with rip-rap to help prevent future bank failures. To improve bank stability and reduce bank erosion along the downstream portion of the project, several tasks could be performed. Live staking stream banks or reinforcing banks with riprap along bends and meanders will help prevent undercutting and bank failures in the future. Also, the entire project area could be planted with a riparian seed mix to reinforce banks. The estimated cost for the Evans Street project is \$130,000.



5.2 BMP Project Identification

BMPs were initially identified using various layers in GIS including the following: aerial photography, parcels, land use, storm water inventory, and topography. Twenty-three (23) potential BMP locations were initially identified. These locations were field visited by WK Dickson staff in November 2015 to determine the feasibility of each site for a BMP. An overview map has been provided showing these sites (See Figure 5-8).

The proposed locations for the BMPs were evaluated based on the following criteria:

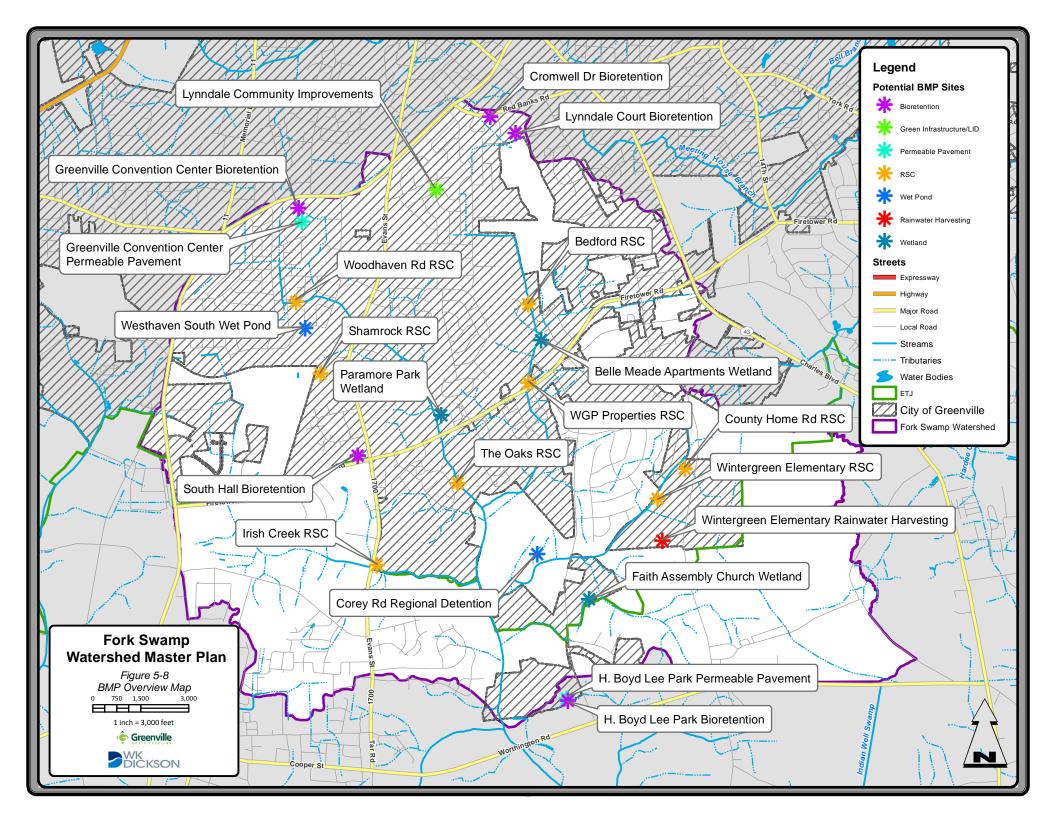
- Watershed Size/Drainage Area Larger watershed sizes allow an opportunity for more treatment. A significant contributing drainage area would allow the use of a larger, more regional BMP such as a wet pond or extended detention wetland.
- Percentage of impervious area Areas with high impervious percentages allow an opportunity for more treatment.
- Proximity to existing conveyance system Runoff will need to be diverted into the BMP and then discharged back to the conveyance system. Locations in close proximity to the existing conveyance system will reduce the cost associated with constructing new drainage structures.
- Land Availability/Ownership The proposed BMPs will require undeveloped land.
 Attempts were made to concentrate on publicly owned land because the high cost of
 private land can make a project unlikely.
- Topography Sufficient vertical relief, up to 5 feet, is required to allow certain BMPs (i.e., bioretention and wet ponds) to function per NCDEQ design requirements.
- Hydrologic conditions BMPs such as wet ponds or extended detention wetlands need the proper hydrologic conditions for plants to survive. The soils or existing water table must allow for the BMP facility to permanently hold stormwater runoff.

Public schools, parks, and churches were closely looked at due to the large impervious areas (e.g. parking lots) available for treatment and the educational benefits of installing a BMP onsite. Residents who provided feedback via online survey or by attending the public meeting held in November 2014 were also taken into account. The feedback helped determine several locations where erosion, flooding, or water quality were of concern. Several of the sites identified met multiple criteria for a successful project and were therefore recommended in this Master Plan.

5.3 RECOMMENDED BMPs

Based on field visits and the above criteria, eighteen (18) sites were recommended for BMP retrofits in the Fork Swamp Watershed. Factors that eliminated a site from consideration included the following: limited space, tree density, utility conflicts (e.g. high voltage transformers and other electrical distribution equipment), and insufficient topographic relief.

Preliminary conceptual design calculations completed for each of the eighteen (18) BMPs are included in Appendix I. The design calculations were based on methodologies found in the NCDEQ Stormwater BMP Manual. The size of the BMP is based on the contributing watershed area and the amount of impervious area within the watershed. Per NCDEQ requirements, the recommended BMPs were designed to treat runoff from the first one-inch of rainfall. The treatment volume is directly correlated to the amount of impervious area. Watersheds with larger amounts of impervious area convert more of the rainfall into runoff, thereby requiring a larger sized BMP.



Fork Swamp Water Quality Project #1: Cromwell Drive Bioretention

A bioretention area is proposed in the open space located behind the American Red Cross Blood Donation Center at 700 Cromwell Drive (See Picture 5-14). This area is adjacent to a parking lot and large building that currently drain to an open channel running perpendicular to Red Banks Road. Flow from the building and parking lot can be redirected via curb cuts to be treated before discharging to FSUT3. The bioretention area may be impacted by gas line utilities and will require minimal infrastructure retrofits.



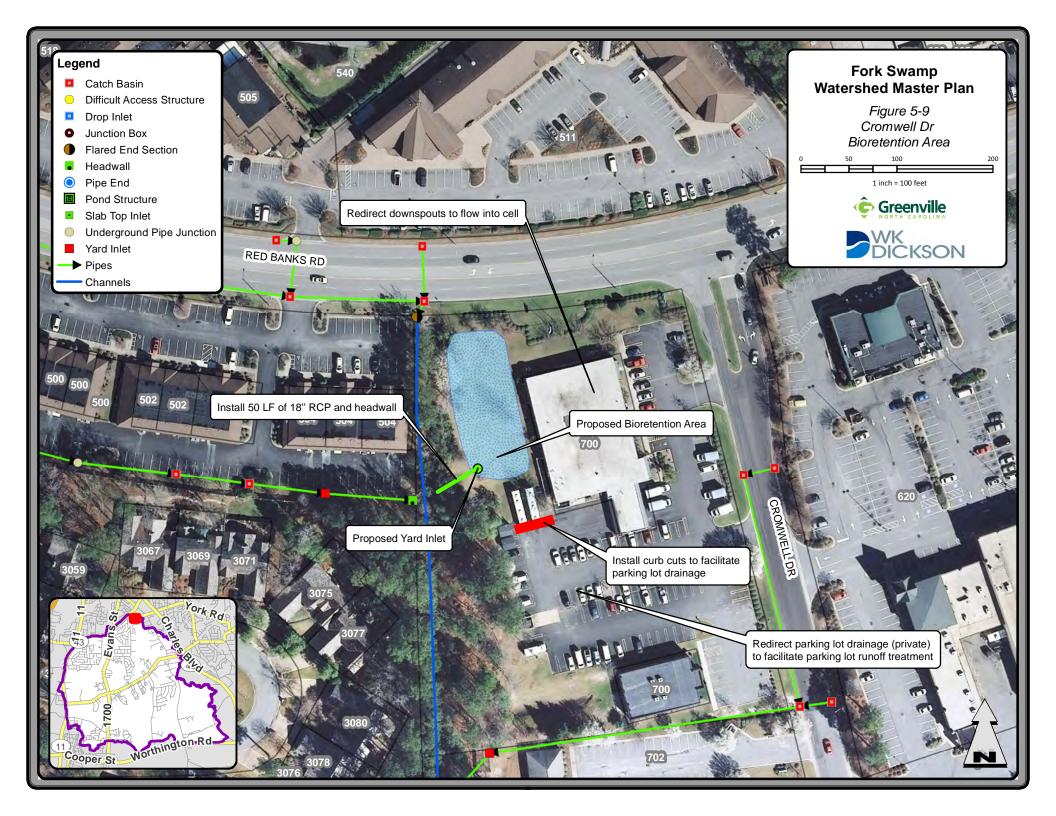
Picture 5-14. Proposed Location for Cromwell Drive Bioretention Cell

The required surface area for the proposed bioretention is approximately 2,600 square feet (0.06 acres). A concept level plan of the proposed improvements is shown in Figure 5-9.

The proposed bioretention project consists of the following improvements:

- Install a bioretention pond designed to treat runoff from the adjacent parking lot. Impervious area draining to the proposed pond is approximately 0.5 acres.
- Install a yard inlet with an 18" outfall pipe directing flow into an existing conveyance system.

The proposed water quality project is located on private property. In order to construct the bioretention area, an easement agreement would be required with the owner. The estimated construction cost for the bioretention area at Cromwell Drive is \$350,000.



Fork Swamp Water Quality Project #2: H. Boyd Lee Park Bioretention

A bioretention area is proposed in the open space south of the H. Boyd Lee Park parking area (See Picture 5-15). This area drains parking lot and street runoff, athletic fields, and buildings. Some additional drainage infrastructure has been added near the entrance of the park, and will drain towards the proposed bioretention area. Otherwise, there is minimal existing drainage infrastructure. As shown in the picture below, there is some standing water in the field area. The bioretention area will primarily provide water quality benefits by attenuating runoff prior to its discharge into Fork Swamp.



Picture 5-15. Proposed Location for H. Boyd Lee Park Bioretention Area

The required surface area for the proposed bioretention is approximately 7,500 square feet (0.2 acres). A concept level plan of the proposed improvements is shown in Figure 5-10.

The proposed bioretention project consists of the following improvements:

- Install a bioretention pond designed to treat runoff from the adjacent lot and road. The impervious area draining to the proposed pond is approximately 2.5 acres.
- Install a yard inlet with a 24" outfall pipe directing flow into an existing conveyance system.

The proposed water quality project is located on public property. The estimated construction cost for the bioretention area at H. Boyd Lee Park is \$340,000.

Fork Swamp Water Quality Project #3: H. Boyd Lee Park Permeable Pavement

A permeable pavement parking lot is proposed for the unpaved lot at H. Boyd Lee Park (See Picture 5-16). This area drains a parking lot, park buildings, streets, and open fields. As the City may intend to expand the parking area, or to convert the gravel/dirt road into paved area, this would be an opportune time to install permeable pavement instead of traditional asphalt. Field visits suggest that underdrains for the parking lot may be unnecessary however, geotechnical borings will need to be completed to confirm. The permeable pavement will primarily provide water quality benefits by attenuating runoff prior to its discharge into Fork Swamp. Educational signage could be added to both the proposed bioretention area (Project 2) and the permeable pavement since this is a City-owned park.



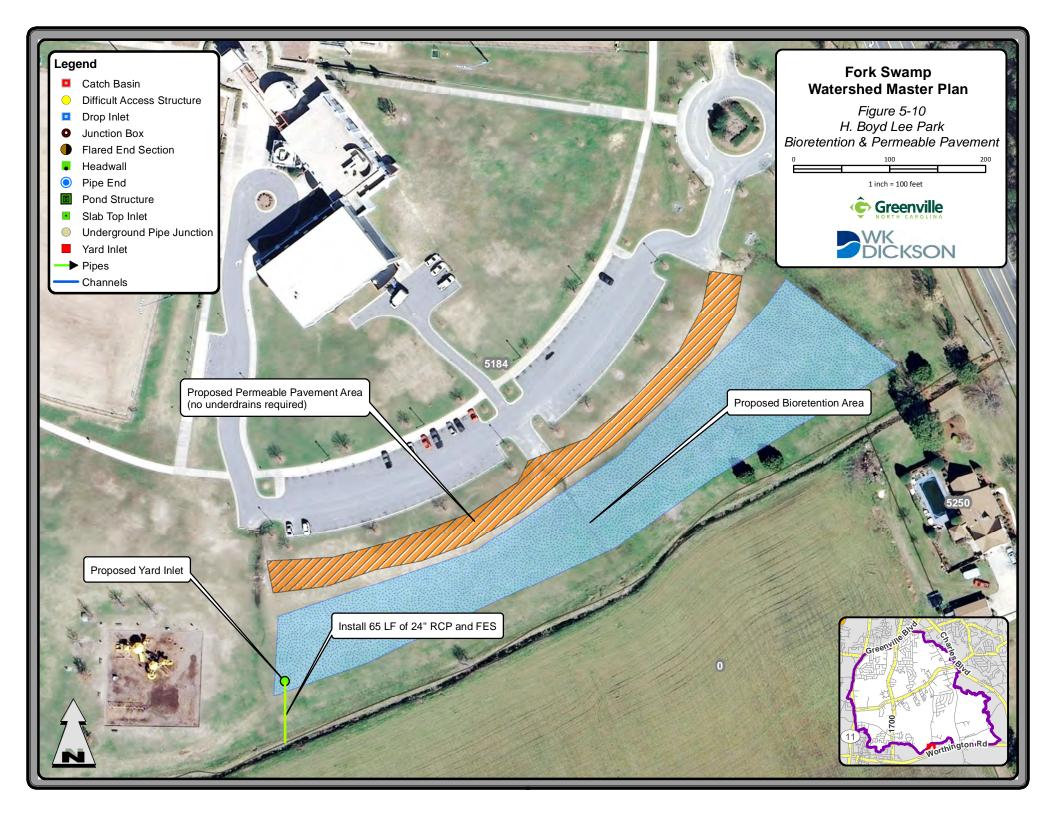
Picture 5-16. Proposed Location for H. Boyd Lee Park Permeable Pavement

The required surface area for the permeable pavement is approximately 17,000 square feet (0.39 acres). A concept level plan of the proposed improvements is shown in Figure 5-10.

The proposed permeable pavement project consists of the following improvements:

- Install 3.5-inch-thick permeable pavers over 2 inches of bedding layer, 4 inches of base aggregate, and 6 inches of gravel casing. Underdrains are not required for this design.
- The proposed impervious areas draining to the proposed pond is approximately 3.5 acres.

The proposed water quality project is located on City property. The estimated construction cost for the bioretention area at H. Boyd Lee Park is \$970,000.



Fork Swamp Water Quality Project #4: Faith Assembly Church Pond Retrofit

A stormwater pond retrofit is proposed in the open area behind Faith Assembly Church off Corey Road (See Picture 5-17). This area drains residential lots, church rooftop runoff, driveways, and sidewalks. The proposed design will add approximately 10,000 square feet of additional storage area. There are no known utility conflicts in the area, however access would require use of church land. The neighborhood downstream includes Trafalgar Drive, where several residents have complained of flooding in their living area. Existing infrastructure are located on private property, and thus were not included in the City-wide inventory. Additional analysis of the pond outlet structure would be required to determine if retrofits are feasible. Increasing the pond storage area will primarily provide water quality benefits by attenuating runoff prior to its discharge into FSUT1.



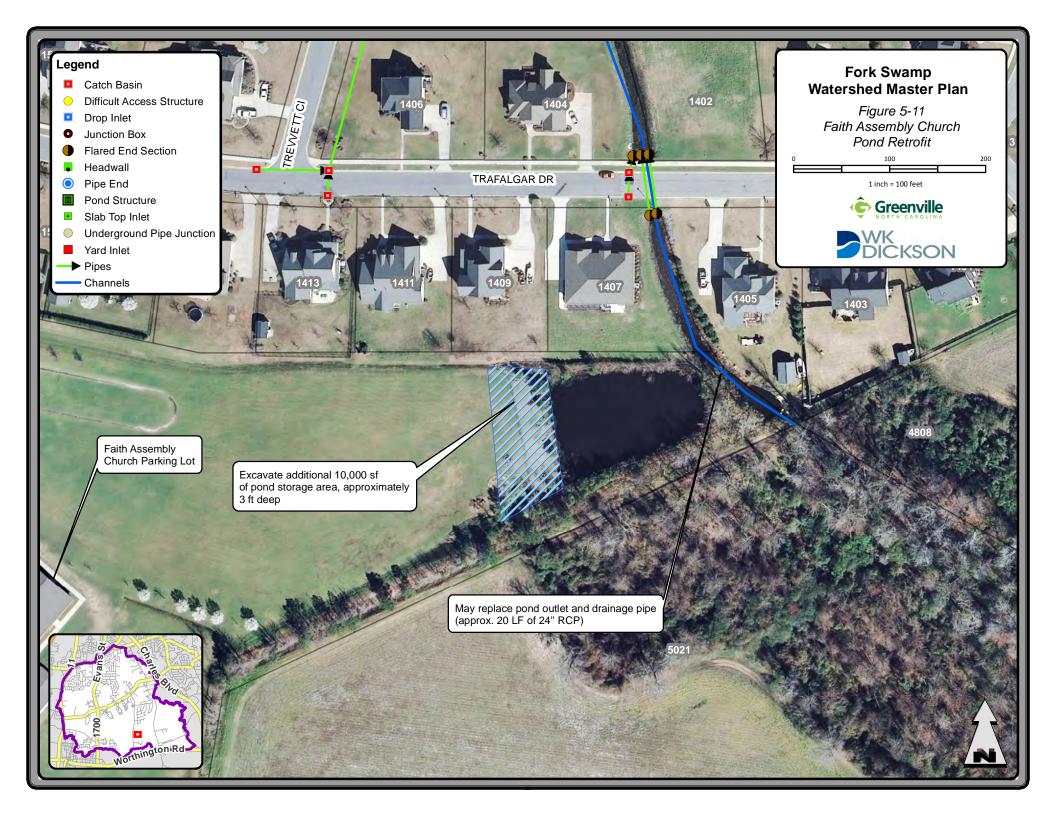
Picture 5-17. Proposed Location for Faith Assembly Church Pond Retrofit

The additional proposed surface area of the pond retrofit is approximately 10,000 square feet (0.23 acres). A concept level plan of the proposed improvements is shown in Figure 5-11.

The proposed wetland project consists of the following improvements:

- Excavate additional pond area designed to treat runoff from the adjacent lot and road. The impervious area draining to the proposed pond is approximately 1 acre.
- Install a yard inlet with an (assumed no inventory data collected) 24" outfall pipe directing flow into an existing conveyance system.

The proposed water quality project is located on private property. In order to construct the wetland, an easement agreement would be required with the owner. The estimated construction cost for the wetland at Faith Assembly Church is \$270,000.



Fork Swamp Water Quality Project #5: County Home Road Regenerative Stormwater Conveyance

A Regenerative Stormwater Conveyance (RSC) system is proposed at the outlet of a 36" CMP near District Park Drive and next to the Pitt County Animal Shelter and a waste collection facility (See Picture 5-18). This area drains some large buildings and parking lots, as well as runoff from County Home Road. Overhead power lines were noted at this location, and would need to be avoided during construction. There were no signs of severe erosion in the channel, however the runoff from the animal shelter and waste dumpsters may benefit from water quality treatment. The RSC will primarily provide water quality benefits by slowing and infiltrating runoff prior to its discharge into Fork Swamp.



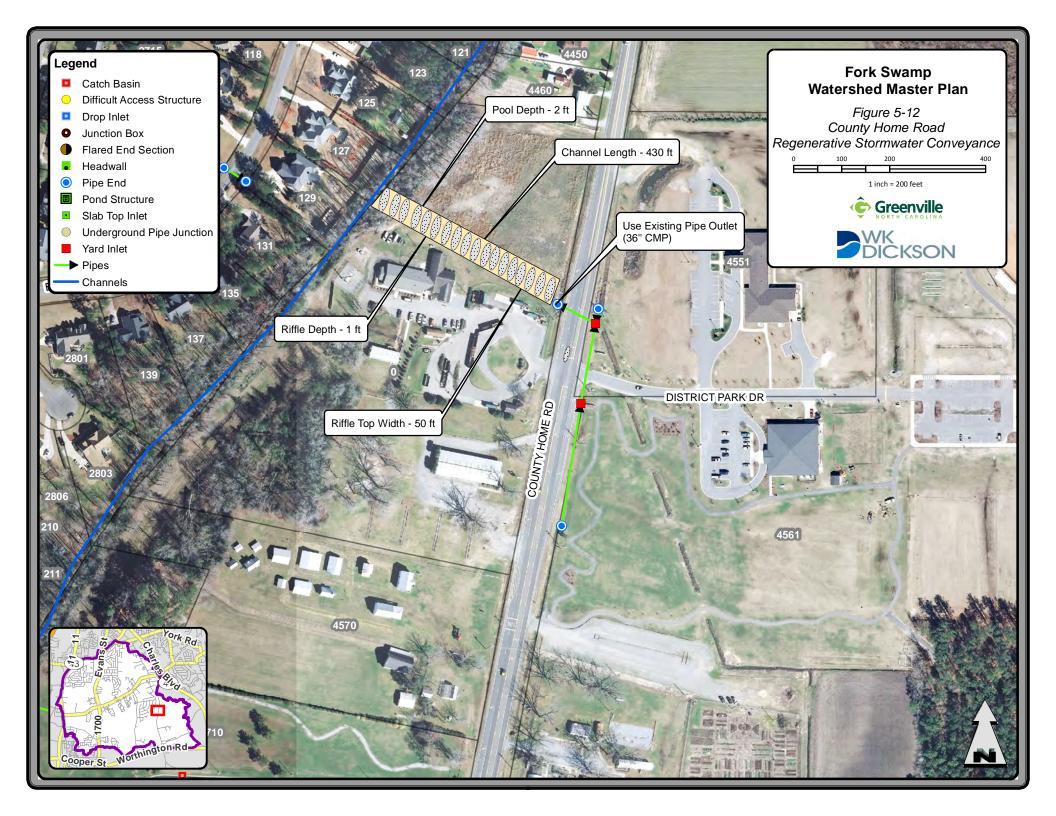
Picture 5-18. Proposed Location for County Home Road RSC

The required surface area of the RSC is approximately 24,500 square feet. A concept level plan of the proposed improvements is shown in Figure 5-12.

The proposed RSC project consists of the following improvements:

- Install RSC channel designed to treat runoff from the adjacent lots and road. The proposed impervious areas draining to the enhanced channel is approximately 4.8 acres.
- Excavate step pools and install required boulders, cobbles, and infiltration media. The quantities are specified in Appendix I.

The proposed water quality project is located on County property. The estimated construction cost for the RSC at County Home Road is \$490,000.



Fork Swamp Water Quality Project #6: Irish Creek Regenerative Stormwater Conveyance

A Regenerative Stormwater Conveyance (RSC) system is proposed at the outlet of a 30" RCP behind the Irish Creek subdivision off Slaney Loop (See Picture 5-19). This area drains low density residential lots and streets. The proposed located is on private property in a newer subdivision, but has no known utility conflicts. The RSC location is also very flat but would provide treatment to runoff that is currently untreated. The RSC will primarily provide water quality benefits by slowing and infiltrating runoff prior to its discharge into FSUT2R1.



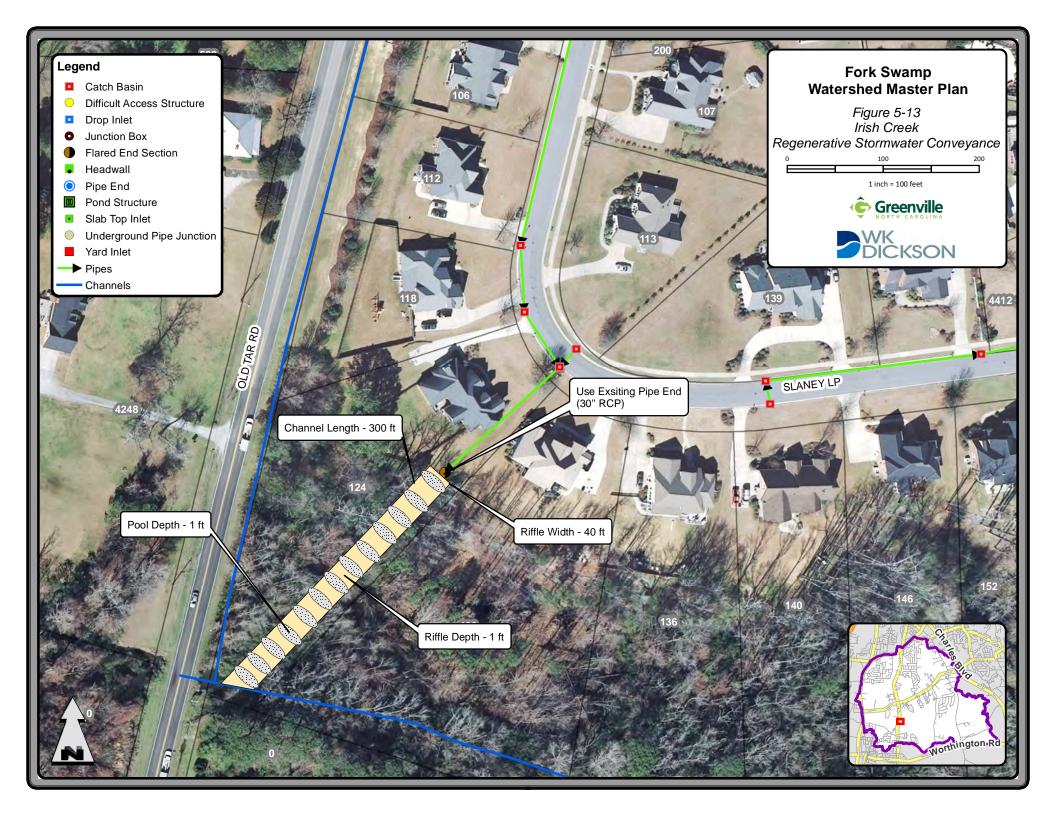
Picture 5-19. Proposed Location for Irish Creek RSC

The required surface area of the RSC is 12,000 square feet. A concept level plan of the proposed improvements is shown in Figure 5-13.

The proposed RSC project consists of the following improvements:

- Install RSC channel designed to treat runoff from the adjacent lots and road. The proposed impervious areas draining to the enhanced channel is approximately 2.6 acres.
- Excavate step pools and install required boulders, cobbles, and infiltration media. The quantities are specified in Appendix I.

The proposed water quality project is located on private property. In order to construct the RSC, an easement agreement would be required with the owner. The estimated construction cost for the RSC at Irish Creek is \$250,000.



Fork Swamp Water Quality Project #7: The Oaks Regenerative Stormwater Conveyance

A Regenerative Stormwater Conveyance (RSC) system is proposed at the outlet of a 24" RCP behind The Oaks subdivision off Treetops Circle (See Picture 5-20). This area drains low density residential lots and streets. The proposed location is on private property, but there have been complaints of flooding in the backyards of lots on Treetops Circle. The proposed location will have minimal impacts to utilities, but access will be limited by proximity of the homes. The RSC would primarily provide water quality benefits by slowing and infiltrating runoff prior to its discharge into Fork Swamp.



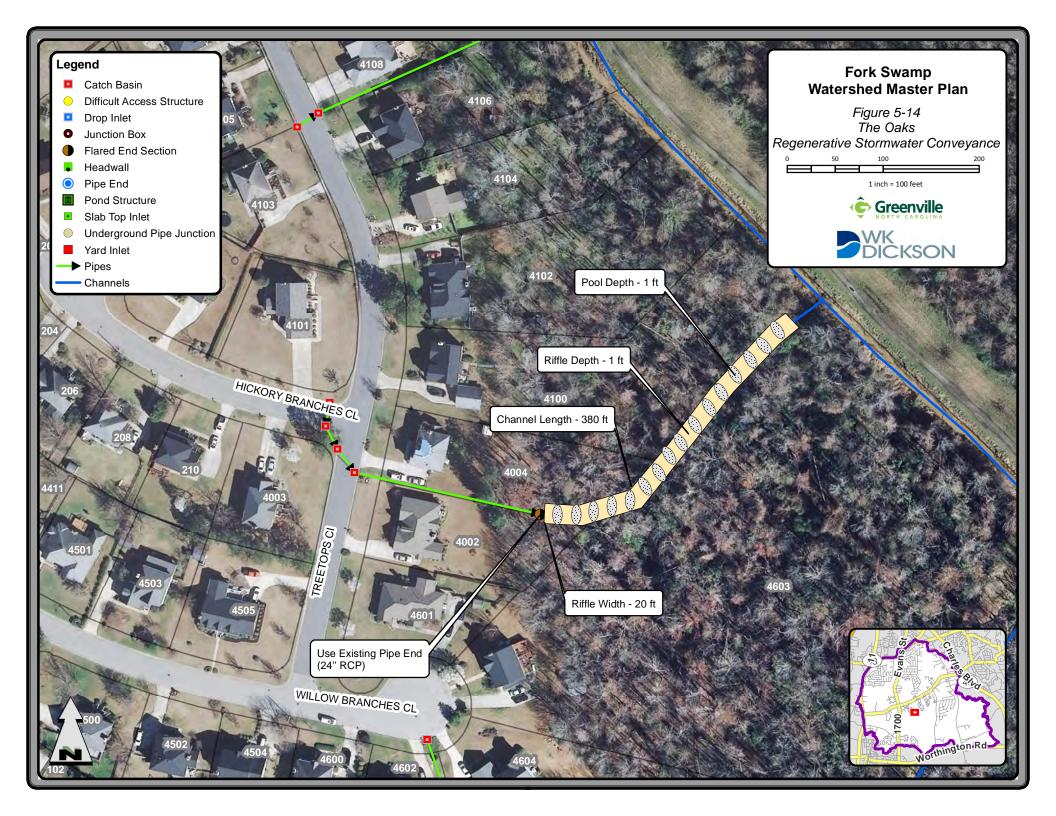
Picture 5-20. Proposed Location for The Oaks RSC

The required surface area of the RSC is 7,600 square feet. Some existing pipe may need to be removed or shortened. A concept level plan of the proposed improvements is shown in Figure 5-14.

The proposed RSC project consists of the following improvements:

- Install RSC channel designed to treat runoff from the adjacent lots and road. The proposed impervious areas draining to the enhanced channel is approximately 2.3 acres.
- Excavate step pools and install required boulders, cobbles, and infiltration media. The quantities are specified in Appendix I.

The proposed water quality project is located on private property. In order to construct the RSC, an easement agreement would be required with the owner. The estimated construction cost for the RSC at The Oaks is \$200,000.



Fork Swamp Water Quality Project #8: South Hall Bioretention

A bioretention area is proposed in the open space in the South Hall business park parking lot at West Fire Tower Road and Evans Street, near the South Hall subdivision (See Picture 5-22). This drainage area contains parking lots and several commercial buildings. The area is currently landscaped with a tree and some large shrubs, and is a focal point for the business park. A bioretention cell is an appropriate BMP choice as attractive plants and landscaping can be added to the cell. Curb cuts will need to be added to facilitate parking lot runoff into the cell to be treated. Some gas line utilities are also present near the proposed tie-in location to the existing drainage system. Since the bioretention will require an 18" RCP outlet, the pipe outlet should tie into the drainage system that exists to the south of the parking lot, and will require two 15" RCP pipes be upgraded to 18" RCP.



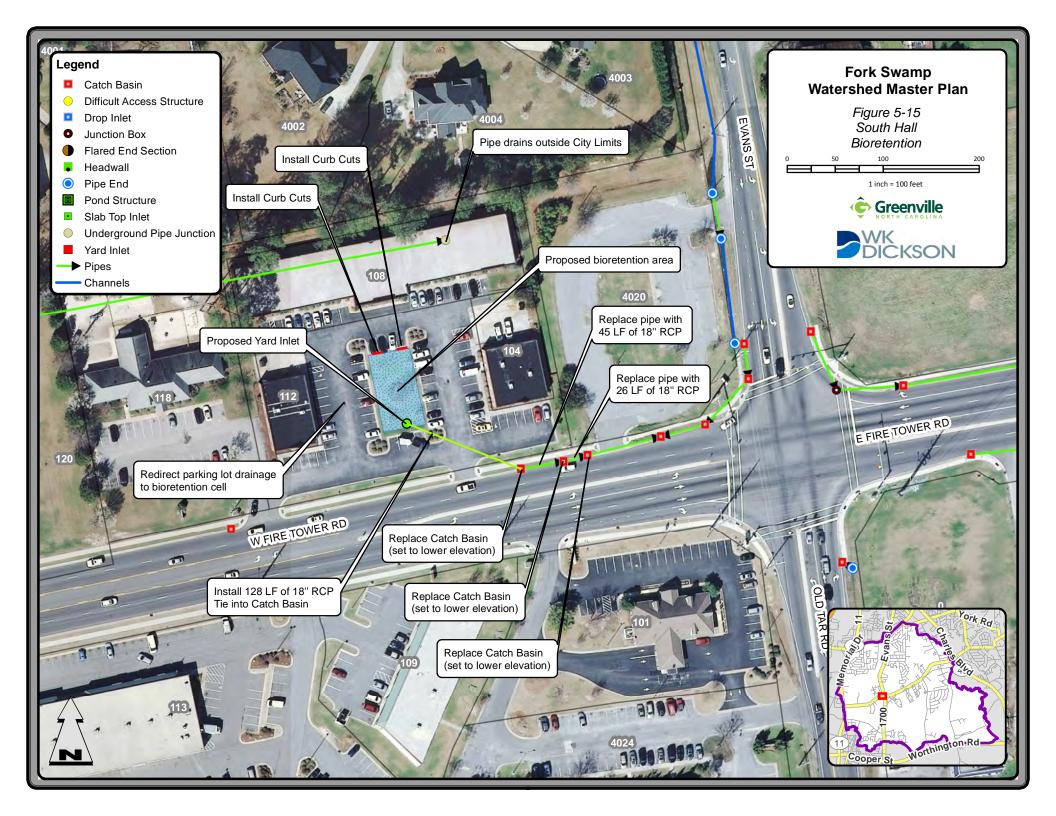
Picture 5-22. Proposed Location for South Hall Bioretention Area

The required surface area for the proposed bioretention is approximately 3,500 square feet (0.07 acres). A concept level plan of the proposed improvements is shown in Figure 5-15.

The proposed bioretention project consists of the following improvements:

- Install a bioretention pond designed to treat runoff from the adjacent lot and road. The impervious area draining to the proposed pond is approximately 1.5 acres.
- Install a yard inlet with an 18" outfall pipe directing flow into an existing conveyance system.

The proposed water quality project is located on public property. The estimated construction cost for the bioretention area at South Hall is \$240,000.



Fork Swamp Water Quality Project #9: Paramore Park Wetland

A stormwater wetland is proposed in the open area of Paramore Park behind the Sheffield subdivision near Albion Drive and East Fire Tower Road (See Picture 5-24). This area drains residential lots and streets and is located on public park property. A sewer easement runs parallel with the stream, which would provide access but the may require additional coordination with GUC. The wetland would function best by allowing flow from Fork Swamp (to the west) to be directed into the wetland for treatment and storage during larger storm events, and then be discharged back into the stream. This technique is known as 'anabranching' and ideally does not impact normal base flow limiting permanent impacts to the stream. The proposed location for the wetland may also be used as a beneficial place for habitat, education, and improved water quality.



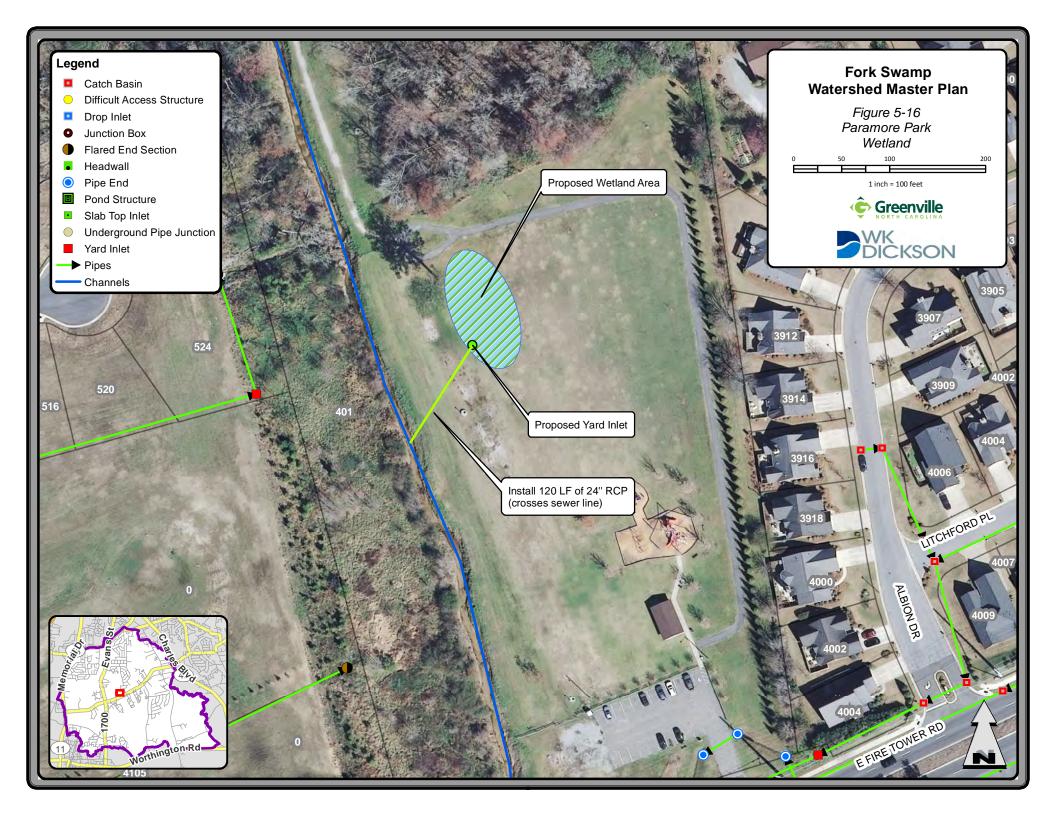
Picture 5-24. Proposed Location for Paramore Park Wetland

The required surface area for the proposed wetland is approximately 6,000 square feet (0.14 acres). A concept level plan of the proposed improvements is shown in Figure 5-16.

The proposed wetland project consists of the following improvements:

- Install a wetland designed to treat runoff from the adjacent lot and road. The proposed impervious areas draining to the proposed pond is approximately 1.6 acres.
- Install a yard inlet with a 24" outfall pipe (or natural channel design with equivalent conveyance) directing flow into an existing conveyance system (stream).

The proposed water quality project is located on City property. The estimated construction cost for the wetland at Paramore Park is \$210,000.



Fork Swamp Water Quality Project #10: WGP Properties Regenerative Stormwater Conveyance

A Regenerative Stormwater Conveyance (RSC) system is proposed at the outlet of an 18" RCP behind the Irish Creek subdivision off Slaney Loop (See Picture 5-25). This area drains a four-lane street (East Fire Tower Road), a small parking lot, and part of a large commercial parking lot. The primary constraint to this location is a sewer cleanout and line that would need to be avoided or relocated. The RSC will primarily provide water quality benefits by slowing and infiltrating runoff prior to its discharge into Fork Swamp.



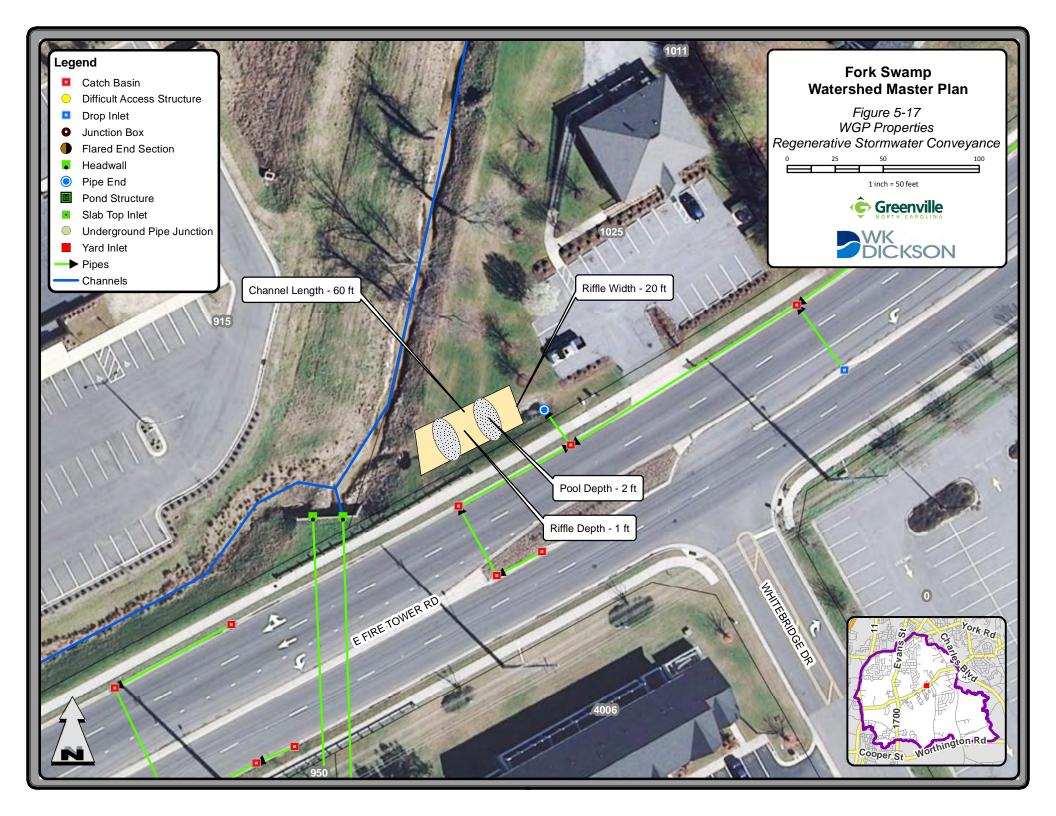
Picture 5-25. Proposed Location for WGP Properties RSC

The required surface area of the RSC is 1,200 square feet. A concept level plan of the proposed improvements is shown in Figure 5-17.

The proposed RSC project consists of the following improvements:

- Install RSC channel designed to treat runoff from the adjacent lots and road. The proposed impervious areas draining to the enhanced channel is approximately 1.8 acres.
- Excavate step pools and install required boulders, cobbles, and infiltration media. The quantities are specified in Appendix I.

The proposed water quality project is located on private property. In order to construct the RSC, an easement agreement would be required with the owner. The estimated construction cost for the RSC at WGP Properties is \$60,000.



Fork Swamp Water Quality Project #11: Wintergreen Elementary Bioretention

The following three projects are all located at Wintergreen Elementary School. Each of the BMP's have unique benefits and costs, which can be discussed with the School System and Administration to determine the most appropriate BMP for the school.

A bioretention area is proposed in the open space adjacent to the parking lot for Wintergreen Elementary on County Home Road (See Picture 5-26). This area has been graded into what appears to be an infiltration basin with a yard inlet at the lower end draining to the nearby stream. The existing drainage infrastructure has enough elevation to excavate a bioretention area and tie-in at existing elevations. The area is next to the school parking lot and main building, therefore landscaping maintenance may be necessary. Some curb cuts are included to facilitate directing parking lot runoff to the area. There are no known utility conflicts in the area. The bioretention area will primarily provide water quality benefits by attenuating runoff prior to its discharge into Fork Swamp.



Picture 5-26. Proposed Location for Wintergreen Elementary Bioretention Area

The required surface area for the proposed bioretention is approximately 6,000 square feet (0.14 acres). A concept level plan of the proposed improvements is shown in Figure 5-18.

The proposed bioretention project consists of the following improvements:

- Install a bioretention pond designed to treat runoff from the adjacent lot and road. The proposed impervious areas draining to the proposed pond is approximately 0.65 acres.
- Install a yard inlet with a 24" outfall pipe directing flow into an existing conveyance system.

The proposed water quality project is located on public property. The estimated construction cost for the bioretention area at Wintergreen Elementary is \$310,000.

Fork Swamp Water Quality Project #12: Wintergreen Elementary Regenerative Stormwater Conveyance

A Regenerative Stormwater Conveyance (RSC) system is proposed at the outlet of a 48" RCP behind Wintergreen Elementary off County Home Road (See Picture 5-27). This area drains the school parking lot, runoff from school buildings, athletic fields, and County Home Road. The proposed location will cross a sanitary sewer line, which may present a conflict when daylighting the existing pipe. The proposed design will remove 135 LF of 48" RCP and grade the RSC channel in its place. The yard inlet will be removed and replaced with the appropriate 48" pipe end and headwall. Located on school property, this installation may be an opportunity for water quality education. The RSC will primarily provide water quality benefits by slowing and infiltrating runoff prior to its discharge into Fork Swamp.



Picture 5-27. Proposed Location for Wintergreen Elementary RSC

The required surface area of the RSC is 4,200 square feet. Some existing pipe segments may need to be shortened or removed. A concept level plan of the proposed improvements is shown in Figure 5-18.

The proposed RSC project consists of the following improvements:

- Install RSC channel designed to treat runoff from the adjacent lots and road. The proposed impervious areas draining to the enhanced channel is approximately 9.3 acres.
- Excavate step pools and install required boulders, cobbles, and infiltration media. The quantities are specified in Appendix I.

The proposed water quality project is located on County property. The estimated construction cost for the RSC at Wintergreen Elementary is \$180,000.

Fork Swamp Water Quality Project #13: Wintergreen Elementary Rainwater Harvesting

A Rainwater Harvesting (RWH) system is proposed for the front office building of Wintergreen Elementary (See Picture 5-28). There are six downspouts on the far left building that would drain into the proposed system. Some retrofits may be required to facilitate drainage into the cistern. Additional considerations for the design phase would be the intended use of the reclaimed water, which has a large impact on sizing. Located on school property and near the front of the building, this location would be ideal for water quality education. This system will collect rooftop runoff and provide water quality benefits by capturing and reusing the runoff or allowing for a slower discharge to FSUT1.



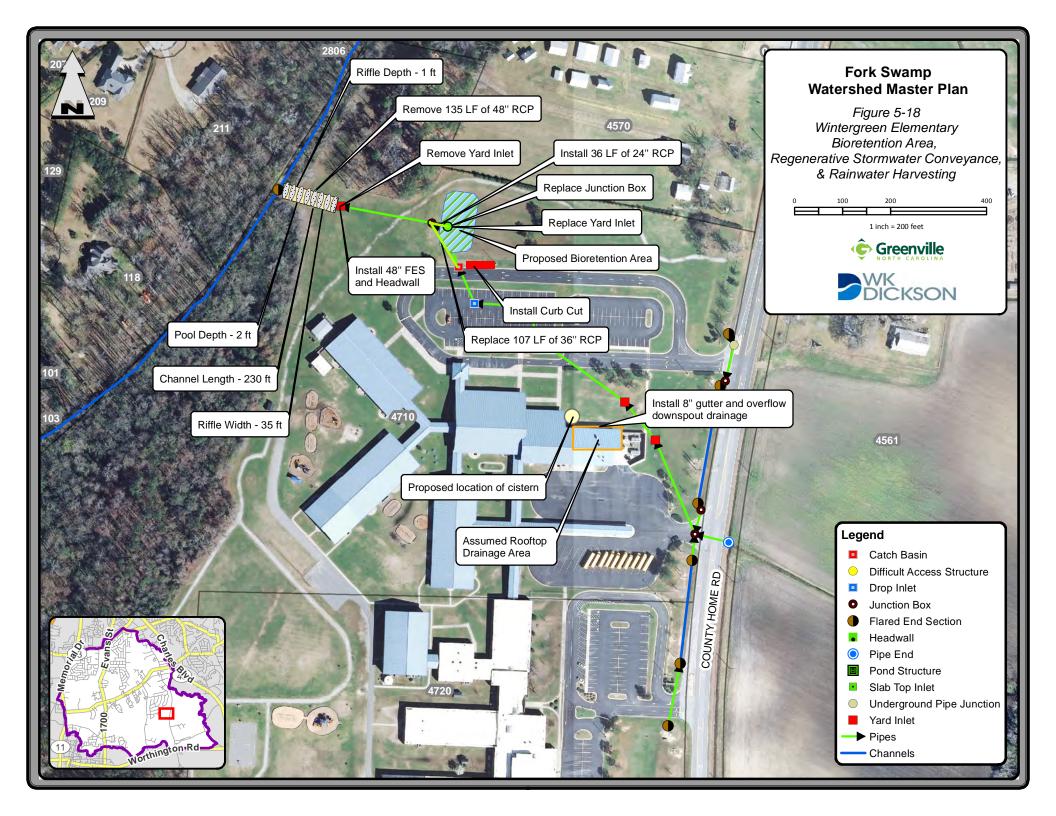
Picture 5-28. Proposed Location for Wintergreen Elementary Rainwater Harvesting

The required volume of the RWH cistern is approximately 3,000 gallons. This estimate will vary depending on the intended use of the stored rainwater. A concept level plan of the proposed improvements is shown in Figure 5-19.

The proposed RWH project consists of the following improvements:

- Install RWH cistern at building location shown in Figure 5-18. The contributing rooftop area is approximately 4,800 square feet (0.11 acres).
- Install gutter system according to Appendix I calculations.

The proposed water quality project is located on County property. The estimated construction cost for the RWH at Wintergreen Elementary is \$20,000.



Fork Swamp Water Quality Project #14: Belle Meade Apartments Wetland

A stormwater wetland is proposed in the open area behind the Belle Meade Apartments near Shadowood Court and East Fire Tower Road (See Picture 5-29). This area drains apartment buildings and parking lots, residential lots, and streets. The proposed location is very flat, and includes a channel for private drainage from the apartment parking lot to Fork Swamp. The project could be combined with the proposed floodplain benching on FSUT3 to maximize water quality and quantity benefits. The existing city infrastructure can be reconfigured to direct flow into the wetland for treatment very easily. The site has fairly good access via the Belle Meade parking lot and there do not appear to be any utility conflicts. The wetland will primarily provide water quality benefits by attenuating runoff prior to its discharge into Fork Swamp.



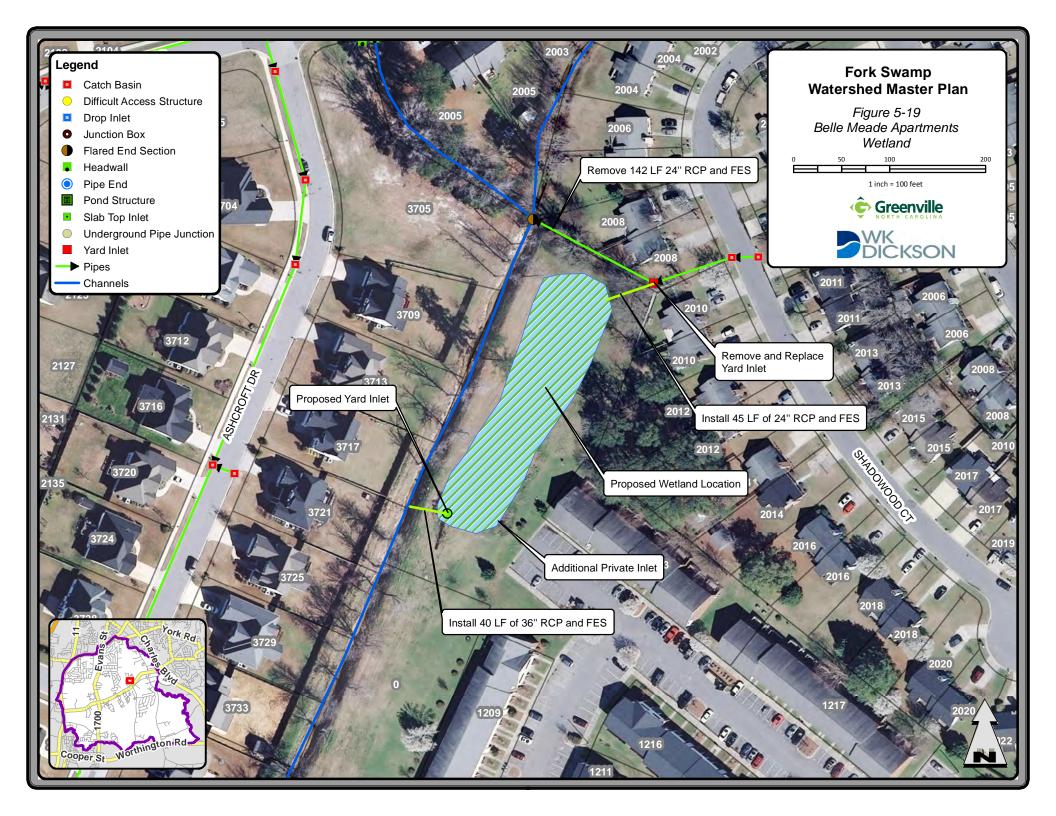
Picture 5-29. Proposed Location for Belle Meade Apartments Wetland

The required surface area for the proposed wetland is approximately 17,700 square feet (0.41 acres). A concept level plan of the proposed improvements is shown in Figure 5-19.

The proposed wetland project consists of the following improvements:

- Install a wetland designed to treat runoff from the adjacent lot and road. The proposed impervious areas draining to the proposed pond is approximately 6.1 acres.
- Remove 24" existing storm sewer pipe and FES and install 45 LF of 24" RCP and FES positioned to drain into the proposed wetland.
- Install a yard inlet with a 36" outfall pipe directing flow into an existing conveyance system.

The proposed water quality project is located on City property. The estimated construction cost for the wetland at Belle Meade Apartments is \$570,000.



Fork Swamp Water Quality Project #15: Greenville Convention Center Permeable Pavement

A permeable pavement system is proposed in the open area behind the Greenville Convention Center on SW Greenville Boulevard (See Picture 5-30). This area drains the parking lots and some rooftop runoff from the building. If the City has plans to expand the parking area, permeable pavement should be considered as the most appropriate BMP to treat parking lot run-off. To further enhance this area, there is also the option to include bioretention in parking lot islands (not included in this concept plan). The permeable pavement system will primarily provide water quality benefits by attenuating runoff prior to its discharge into Fork Swamp.



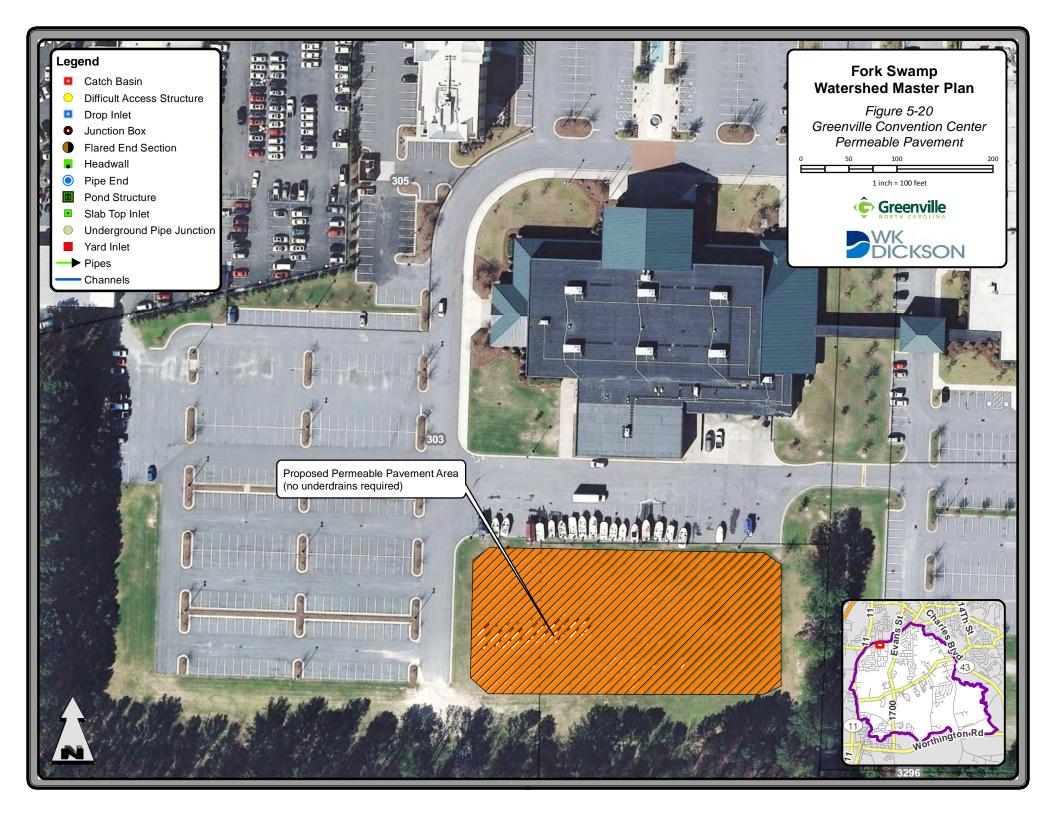
Picture 5-30. Proposed Location for Greenville Convention Center Permeable Pavement

The required surface area for the proposed parking lot is approximately 47,400 square feet (1.1 acres). A concept level plan of the proposed improvements is shown in Figure 5-20.

The proposed permeable pavement project consists of the following improvements:

- Install 3.5-inch-thick permeable pavers over 2 inches of bedding layer, 4 inches of base aggregate, and 6 inches of gravel casing. Underdrains are not required for this design.
- The impervious area draining to the proposed pond is approximately 2.9 acres.

The proposed water quality project is located on City property. The estimated construction cost for the permeable pavement system at the convention center is \$2,870,000. While the cost of this BMP is substantial, the actual additional cost for permeable pavement would be reduced if the City intends on adding parking. These BMPs are only recommended as part of a parking add-on and not an independent retrofit.



Fork Swamp Water Quality Project #16: Lynndale Court Bioretention

A bioretention area is proposed in the common area in the landscaped portion of the Gaylord office park on Lynndale Court (See Picture 5-31). The existing drainage infrastructure has enough elevation to excavate a bioretention area and tie in at existing elevations. The area is the entrance to an office park, therefore landscaping maintenance may be necessary. Curb cuts are included to facilitate directing parking lot runoff to the area. There are some utility conflicts in the area to be avoided such as a fire hydrant and sewer cleanouts. There are two water meter boxes that can be relocated. The bioretention area will primarily provide water quality benefits by attenuating runoff prior to its discharge into FSUT3.



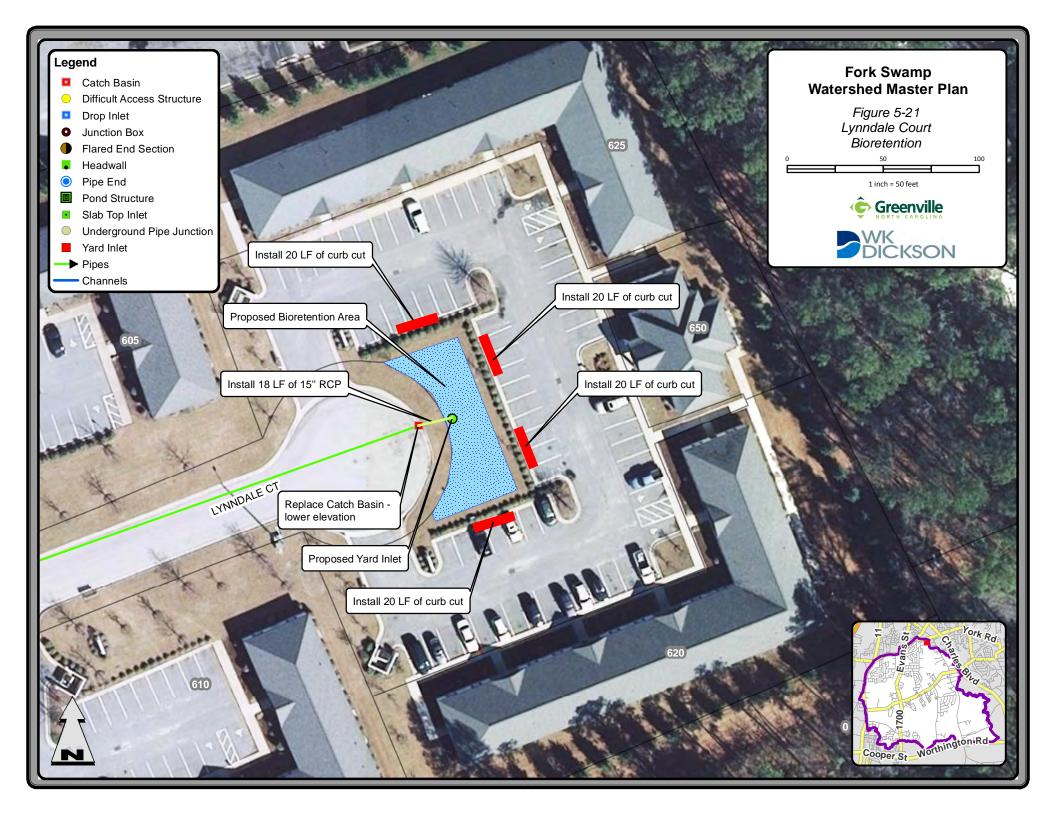
Picture 5-31. Proposed Location for Lynndale Court Bioretention Area

The required surface area for the proposed bioretention is approximately 2,500 square feet (0.06 acres). A concept level plan of the proposed improvements is shown in Figure 5-21.

The proposed bioretention project consists of the following improvements:

- Install a bioretention pond designed to treat runoff from the adjacent lot and road. The proposed impervious areas draining to the proposed pond is approximately 1.05 acres.
- Install a yard inlet with a 15" outfall pipe directing flow into an existing conveyance system.

The proposed water quality project is located on public property. The estimated construction cost for the bioretention area at Lynndale Court is \$150,000.



Fork Swamp Water Quality Project #17: Westhaven South Wetland

A water quality wetland is proposed in the open area south of Cedarhurst Road in the Westhaven subdivision (See Picture 5-32). This area drains several residential lots and some street runoff from Cedarhurst Road. The proposed location is currently used as a community park, but can be enhanced with the addition of the wetland, concrete walkway, and educational signage. There are no known utility conflicts, and the site is accessible through either Cedarhurst Road or Loudon Court. A large wet pond is located upstream of the proposed location, which may present an opportunity to retrofit or treat in series. For concept level design, the wetland has been evaluated as a stand-alone treatment system. The wetland will primarily provide water quality benefits by attenuating runoff prior to its discharge into Fork Swamp.



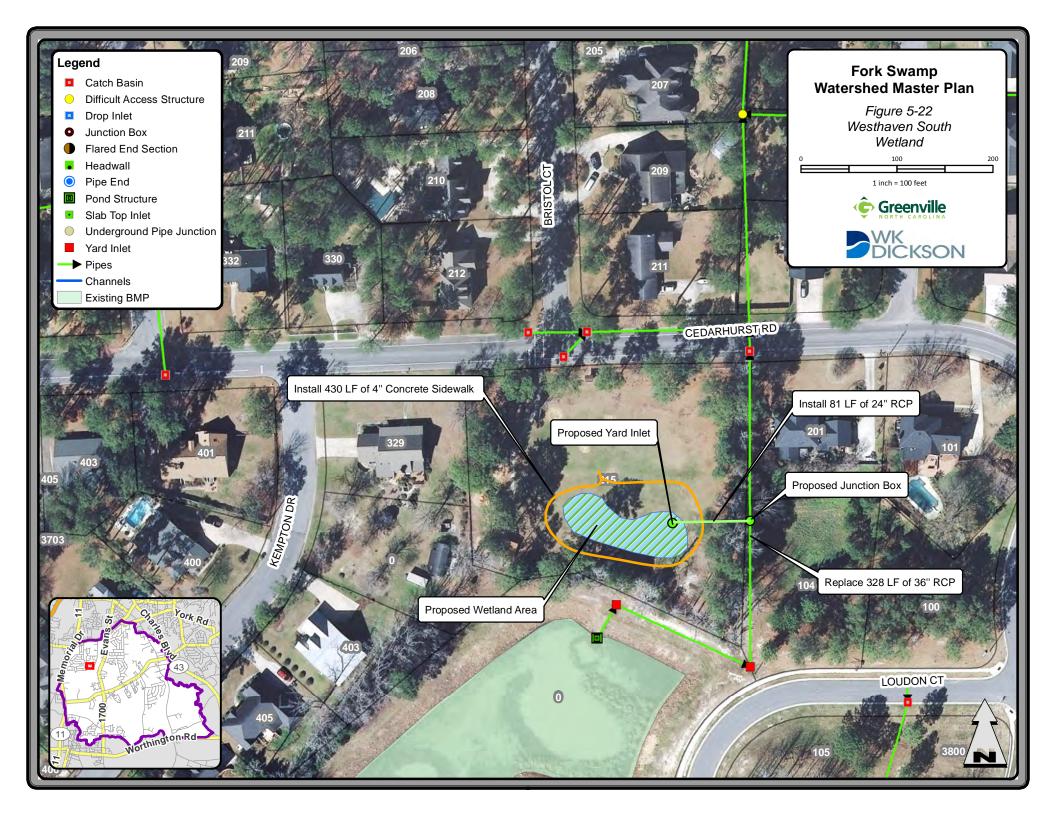
Picture 5-32. Proposed Location for Westhaven South Wetland

The required surface area for the proposed wetland is approximately 4,500 square feet (0.10 acres). A concept level plan of the proposed improvements is shown in Figure 5-22.

The proposed wetland project consists of the following improvements:

- Install a wetland designed to treat runoff from the adjacent lot and road. The impervious areas draining to the proposed pond is approximately 1.5 acres.
- Install a yard inlet with a 24" outfall pipe directing flow into an existing conveyance system.

The proposed water quality project is located on City property. The estimated construction cost for the wetland at Westhaven South is \$820,000.



Fork Swamp Water Quality Project #18: Shamrock Regenerative Stormwater Conveyance

A Regenerative Stormwater Conveyance (RSC) system is proposed at the outlet of a 42" RCP behind the Shamrock subdivision of Evans Street (See Picture 5-33). This area drains high density residential lots and streets. An existing buried 42" RCP will be daylighted for the last 70 LF to incorporate the RSC. This new system will no longer require the yard inlet or 15 LF of 42" RCP downstream and thus should be removed. The slope at the proposed location is more flat than an RSC generally is used for, however water quality benefits will be realized from the series of infiltration beds. There are no known utility conflicts. The RSC will primarily provide water quality benefits by slowing and infiltrating runoff prior to its discharge into FSUT2.



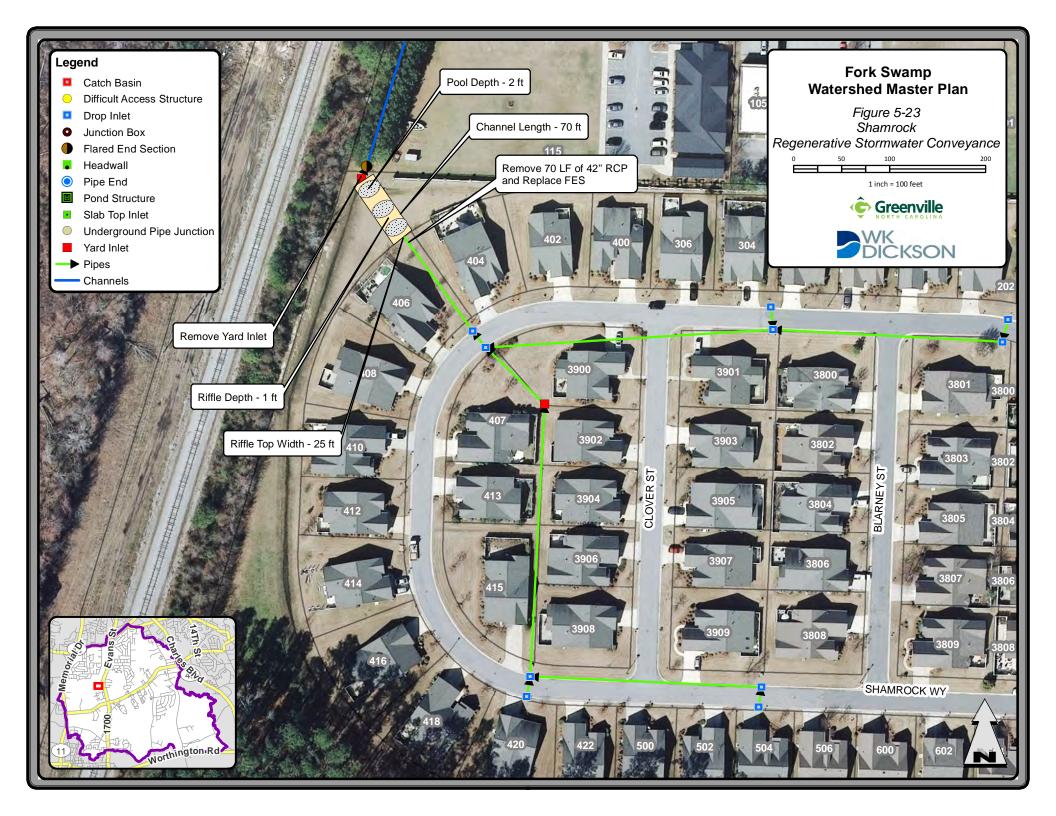
Picture 5-33. Proposed Location for Shamrock RSC

The required surface area of the RSC is 1,750 square feet. Some existing pipe may need to be removed or shortened. A concept level plan of the proposed improvements is shown in Figure 5-23.

The proposed RSC project consists of the following improvements:

- Install RSC channel designed to treat runoff from the adjacent lots and road. The proposed impervious areas draining to the enhanced channel is approximately 6.0 acres.
- Excavate step pools and install required boulders, cobbles, and infiltration media. The quantities are specified in Appendix I.

The proposed water quality project is located on public property. The estimated construction cost for the RSC at Shamrock is \$130,000.



5.4 NUTRIENT REMOVAL CAPACITIES

Along with determining the size and other design parameters for the proposed BMPs, nutrient removal efficiencies were calculated. Total Nitrogen (TN) and Total Phosphorous (TP) were computed based on the removal efficiencies provided in Jordan Lake Nutrient Loading Accounting Tool, version 2.0. While the Jordan Lake tool was developed specifically to address the Jordan Lake and Falls Lake Rules, the tool can apply throughout the State provided the appropriate physiographic location is used. For Greenville and Pitt County the Coastal Plain loading rates are recommended. Benefits of BMP retrofits should be revisited prior to implementation to utilize the most current research as these tools are frequently refined based on updated monitoring results and innovative technologies. The tool is available on NCDEQ website (http://portal.ncdenr.org/web/jordanlake/implementation-guidance-archive).

The tool provided the nutrient effluent concentrations and removal efficiencies for each BMP. It should be noted that the tool does not contain an entry for RSC systems, therefore the 'Sand Filter' option was used since RSCs function similarly to this BMP. Additionally, the RWH was not fully designed to determine a percent of volume reduction as this is highly dependent on the intended use of the reclaimed water. Thus, a volume reduction of 90% was assumed for the system as an intended use has not yet been determined. The percent reduction has a direct effect on the concentration of nutrients in runoff. The calculated removal efficiencies are provided in the table below.

Table 5-1: Proposed BMP Pollutant Removal Efficiency

Project	TN Removed	TP Removed
	(lb/ac/yr)	(lb/ac/yr)
Project #1 – Cromwell Drive Bioretention	3.61	1.19
Project #2 – H. Boyd Lee Park Bioretention	4.46	1.60
Project #3 – H. Boyd Lee Park Permeable Pavement	8.62	3.79
Project #4 – Faith Assembly Church Pond Retrofit	1.86	0.99
Project #5 – County Home Road Regenerative Stormwater Conveyance	1.68	0.89
Project #6 – Irish Creek Regenerative Stormwater Conveyance	1.98	1.21
Project #7 – The Oaks Regenerative Stormwater Conveyance	2.70	1.89
Project #8 – South Hall Bioretention	9.97	3.87
Project #9 – Paramore Park Wetland	2.34	1.38
Project #10 – WGP Properties Regenerative Stormwater Conveyance	4.13	2.95
Project #11 – Wintergreen Elementary Bioretention	4.65	1.63
Project #12 – Wintergreen Elementary Regenerative Stormwater Conveyance	2.63	1.59
Project #13 – Wintergreen Elementary Rainwater Harvesting	10.18	1.41
Project #14 – Belle Meade Apartments Wetland	3.22	2.15
Project #15 – Greenville Convention Center Permeable Pavement	1.73	0.79
Project #16 – Lynndale Court Bioretention	7.63	3.35
Project #17 – Westhaven South Wetland	4.11	1.61
Project #18 – Shamrock Regenerative Stormwater Conveyance	3.02	1.94

PUBLIC EDUCATION AND OUTREACH

Successful implementation of the Fork Swamp Watershed Master Plan and stormwater as a whole requires extensive public education and outreach. The City has taken important steps in public outreach within the Fork Swamp watershed through the use of direct mail questionnaires, web-based applications, and public meetings. Questionnaires were mailed to residents throughout the watershed in August of 2014 requesting feedback on flood-prone areas and any water quality concerns. Compiled results of the questionnaires can be found in Appendix D.

A public meeting was held on November 4, 2014, to introduce the project and facilitate further feedback from the public. The initial public feedback is critical to identifying flood-prone areas and validating model results. A follow-up was held on November 17, 2015 to share results of the Master Plan with the public. As selected projects proceed into design and construction continuous public outreach will be critical to the success of the projects. Additional public meeting and individual property owner meetings will help educate property owners on the benefits of the proposed projects as well as the temporary and permanent impacts from construction.

Aside from the public education and outreach completed for projects specific to the Fork Swamp Watershed Master Plan, the City has several programs dedicated to educating the public about water quality and pollution. The City's website provides information about the Stormwater Program and the development of the Stormwater Utility and associated fees. Another outreach measure that could be considered would be to target those City residents that live adjacent to streams. For this select group, quarterly newsletter could be mailed presenting information regarding the importance of not illegally discharging item (e.g. yard waste, car batteries, and other miscellaneous debris) into the stream. The newsletter should encourage the residents to keep the stream clean and report any blockage.

A different approach could be coordinating with local schools to teach the students about age appropriate stormwater issues. There are many benefits to teaching children about stormwater issues including the students relaying the information to their parents. A presentation could be done in conjunction with an afternoon spent visiting and cleaning up a nearby stream. Adding an educational BMP near a school and park would be another outreach opportunity. The projects proposed at Wintergreen Elementary School and Paramore Park would be an example. This along with the previously mentioned newsletter could be included in the Public Education section of the City's Action Report and Plan that must be completed annually to meet the requirements of the Neuse River Basin stormwater program.

ANTICIPATED PERMITTING

The proposed improvements described in Section 4 may require local, State, and/or Federal permits or approvals prior to the onset of construction. Based on the types of projects identified in the Fork Swamp watershed, permits or approvals may be required for any of the following reasons:

- Stream and/or wetland impacts;
- FEMA floodway impacts;
- Land disturbance; and
- Potable water and sewer line adjustments.

The permitting matrix shown in Table 7-1 shows the different types of permits that are anticipated for each of the proposed flood control projects. The water quality retrofits may require erosion control permits if the area of disturbance is greater than 1.0 acres, but permits or agreements from DWR, USACE, FEMA, and NCDOT are not anticipated for these projects.

The types of 404/401 permits are described below and may vary based on the length of stream impacts and/or acreage of wetland impacts. Wetlands will need to be delineated to determine the acreage of impacts. Permit requirements for a given project may change based on the final design and any changes to the existing regulations. The appropriate permitting agencies should be contacted during the design process to determine if permits will be required for the proposed project.

7.1 NORTH CAROLINA DIVISION OF WATER RESOURCES 401 WATER QUALITY CERTIFICATION AND US ARMY CORPS 404 PERMIT

Proposed improvements within the City of Greenville must adhere to the requirements set forth in Section 401 and 404 of the Clean Water Act. Required permitting can range from activities that are pre-authorized to those requiring pre-construction notification (PCN) for a Nationwide Permit (NWP) to those requiring an Individual Permit (IP). Individual permits may be required for projects with stream impacts greater than 300 feet and wetland impacts greater than 0.5 acres. It is anticipated that NWP #3 (Maintenance) and NWP #13 (Bank Stabilization) may be required to support the projects that include work within channels that are claimed jurisdictional by the US Army Corps of Engineers (USACE). Individual permits may be required for floodplain benches where significant wetland impacts may be encountered. More detailed explanations of the types of 404 permits are provided below.

NWP#3 - Maintenance

This permit authorizes the repair, replacement, or rehabilitation of any previously permitted or currently serviceable structure. A PCN is not required for minor deviations in the structure's configuration or filled area that occur as a result of changes in materials, construction techniques, or safety standards necessary to make repair or replacement, provided environmental impacts are minimal. A PCN to the USACE is required if a significant amount

of sediment is excavated/filled within the channel. NC Division of Water Resources (DWR) does not typically require a PCN for NWP #3 but usually receives one as a courtesy.

Other provisions imposed by the State of North Carolina require that culvert inverts must be buried a minimum of 1-foot below the streambed for culverts greater than or equal to 48 inches in diameter to allow low flow passage of water and aquatic life. Culverts less than 48 inches in should be buried to a depth of 20 percent or greater of the culvert's diameter.

7.2 INDIVIDUAL PERMITS

Individual permits are required when stream or wetland impacts do not meet the conditions of a nationwide permit. Permit applications may be reviewed by multiple agencies including but not limited to USACE, DWR, EPA, SHPO, NCWRC, and USFWS. The application is also made available for public review. There is no defined timeline for review of the application for an IP; therefore, the permitting process for an IP is typically significantly longer that the review time for a NWP. Typically, 404 and 401 Individual Permits are applied for jointly and their review is concurrent.

7.3 FEDERAL EMERGENCY MANAGEMENT AGENCY (FEMA)

Streams with a drainage area greater than one square mile are typically modeled and mapped by FEMA for flood insurance purposes. The 100-year floodway and floodplain has been mapped for the following segments of stream:

- Fork Swamp from approximately 0.4 mile upstream of East Fire Tower Road to its confluence with the Swift Creek;
- FSUT1 from Corey Road to its confluence with Fork Swamp;
- FSUT2R1 from Old Tar Road to its confluence with Fork Swamp; and
- FSUT23 from approximately 0.2 miles downstream of East Fire Tower Road D/S to its confluence with Fork Swamp.

Any proposed projects that will include grading within a FEMA defined floodway will require a Conditional Letter of Map Revision (CLOMR) submitted to FEMA for pre-approval purposes and a Letter of Map Revision (LOMR) upon completion of construction. Table 7-1 identifies projects where FEMA permitting is expected.

7.4 Erosion and Sedimentation Control

North Carolina Department of Environmental Quality (NCDEQ) is another agency that requires notification before proposed activities are constructed. NCDEQ requires that an erosion and sedimentation control plan be submitted to the Land Quality Section for approval before the start of construction for any disturbance greater than one acres. Erosion and Sedimentation permits are anticipated for most of the proposed projects as shown in Table 7-1.

Table 7-1: Permitting Matrix for Proposed Projects						
	FEMA	NCDEQ	404/401	404/401	NCDOT	RAILROAD
		/NPDES	(NWP)	(IP)	110201	THILLIAM
PRIMARY SYSTEM PROJECTS						
Railroad Floodplain Benching and		x	X			
Stream Stabilization (Fork Swamp)						
Evans Street Culvert Replacement						
and Floodplain Benching (Fork		X	X		X	
Swamp)						
East Fire Tower Road Floodplain	3/	•	3/			
Benching and Stream Stabilization	X	X	X			
(Fork Swamp)						
Fork Swamp Main Branch	X	X	X			
Floodplain Benching (Fork Swamp)						
Trafalgar Drive – South Floodplain		X	X			
Culvert (FSUT1)						
Trafalgar Drive – North Culvert		X	X			
Replacement (FSUT1)						
Corey Road Floodplain Culverts and	X	X	X		X	
Benching (FSUT1)						
Culverts and Ronghing (FSLIT2)		X	X		X	
Culverts and Benching (FSUT3) East Fire Tower Road – U/S						
Floodplain Culvert (FSUT3)		X	X		X	
Wimbledon Drive Culvert						
Replacement and Floodplain		x	X			
Benching (FSUT3)						
Tower Place Culvert Replacement						
(FSUT3)		X	X			
Summerhaven Drive Culvert						
Replacement and Floodplain		X	X			
Benching (FSUT3)						
East Fire Tower Road – D/S						
Floodplain Benching and Stream	X	X	X		X	
Stabilization (FSUT3)						
SECONDARY SYSTEM PROJECTS						
Corey Road		X			X	
Lynndale Closed System Phase I		X				
Lynndale Closed System Phase II		X				
Lynndale Closed System Phase III X						
STREAM STABILIZATION PROJECTS						
Project #1 – Live Oak Lane	X	X	X			
Project #2 – Corey Road	X	X	X			
Project #3 – East Fire Tower Road		Х	X			
Project #4 – Tower Place		X	X			

SECTION 7: ANTICIPATED PERMITTING

	FEMA	NCDEQ /NPDES	404/401 (NWP)	404/401 (IP)	NCDOT	RAILROAD
Project #5 – Charles Boulevard		X	X			
Project #6 – Queen Annes Road		Х	Х			
Project #7 – Evans Street		Х	Х			
V	VATER Q	UALITY PI	ROJECTS			
Project #1 – Cromwell Drive		v				
Bioretention		X				
Project #2 – H. Boyd Lee Park		v				
Bioretention		X				
Project #3 – H. Boyd Lee Park		v				
Permeable Pavement		X				
Project #4 – Faith Assembly Church		v				
Pond Retrofit		X				
Project #5 – County Home Road RSC		X				
Project #6 – Irish Creek RSC		X				
Project #7 – The Oaks RSC		Х				
Project #8 – South Hall Bioretention		Х				
Project #9 – Paramore Park Wetland		X				
Project #10 – WGP Properties RSC		х				
Project #11 – Wintergreen		х				
Elementary Bioretention		Λ				
Project #12 – Wintergreen		X				
Elementary RSC		Λ.				
Project #13 – Wintergreen		X				
Elementary Rainwater Harvesting		Λ				
Project #14 – Belle Meade		X				
Apartments Wetland		Λ				
Project #15 – Greenville Convention		X				
Center Permeable Pavement		Λ				
Project #16 – Lynndale Court		X				
Bioretention	, A					
Project #17 – Westhaven South	X					
Wetland		Λ				
Project #18 – Shamrock RSC		X				

FUNDING OPPORTUNITIES

8.1 WATER QUALITY IMPROVEMENT FUNDING

As the final designs of the proposed improvements are evaluated, the City is encouraged to investigate the potential funding mechanisms that are available for water quality projects. There are wide range of funding mechanisms that may be available to the City. Sources include the Clean Water Act Part 319 funds administered by the US EPA and North Carolina Cleanwater Management Trust Fund (CWMTF). CWMTF funding can include land acquisition costs, design fees, and construction costs to help finance projects that improve and protect water quality. In 2014, \$24.8 million to fund projects throughout North Carolina (www.cwmtf.net).

The Clean Water State Revolving Fund (CWSRF) is another option. It offers low-interest loans that can be used to find stormwater projects with water quality components. It should be noted that typically, grants require some type of match funding. The matching requirements vary for each different type of grant. For example, the CWSRF requires a 20 percent match from the State based on the amount of Federal dollars awarded while the CWMTF does not have a specified match requirement.

The NCDEQ Division of Water Resources has a Water Resources Development Project Grant Program. The program provides cost-share grants and technical assistance. The grants are offered for the following purposes: general navigation, recreational navigation, water management, stream restoration, beach protection, land acquisition, and facility development for water-based recreation and aquatic weed control. Spring 2014, the program awarded grants ranging from \$1,500 to \$450,000. The total awarded across thirty-seven projects/recipients was \$2,240,000 (www.ncwater.org).

8.2 FLOOD MITIGATION FUNDING

FEMA's Flood Mitigation Assistance (FMA) is a pre-disaster grant program designed to provide funding to Stated and communities in their efforts to reduce or eliminate the risk of repetitive flood damage to building and structures insured under the National Flood Insurance Program (NFIP). In order to be eligible, communities must have completed and approved Flood Mitigation Plans that assess the flood risk and identify actions to reduce that risk. Any State agency, participating NFIP community, or local agency is eligible to participate and should contact community officials.

Additional project grant eligibility criteria include a project that is:

- Cost effective;
- Cost beneficial to the National Flood Insurance Fund;
- Technically feasible; and

 Physically located in participating NFIP community or reduce future flood damages in an NFIP community.

A project must also comply with (1) the minimum standards of the NFIP Floodplain Management Regulations, (2) the applicant's Flood Mitigation Plan, and (3) all applicable laws and regulations. The State is the grantee and program administrator for FMA. FEMA distributes FMA funds to States that in turn provide funds to communities. FEMA may provide up to 75% of the total eligible costs. The remaining costs must be provided by a non-Federal source of which no more than half can be provided as in-kind contributions from third parties.

8.3 REVENUE AND GENERAL OBLIGATION BONDS

Municipalities in North Carolina have the authority to use binding for capital improvement projects under the State's General Statues. There are two types of bonds available for use – general obligation and revenue bonds. General obligation bonds are funds received after voter approval of bond referendum. A vote is required because general obligation bonds are secured using the City's taxing power. All revenues, including different taxes, can be used to pay off a general obligation debt. Revenue bonds, on the other hands, are backed by income generated by the City through fees collected (e.g., various utility fees including stormwater). Because their security is not as great as that of general obligation bonds, revenue bonds may carry a slightly higher interest rate.

8.4 UTILITY RATE STUDY

The City should consider completing a utility rate study to determine if the current rate is appropriate for funding the required operation of the Stormwater Division as well as capital projects. The enterprise fund was originally established in 2001 with collections beginning in 2003. In May 2013, City staff requested a fee increase of \$0.50/ERU each year for the next five years to support capital projects and completion of the City-wide master plan. Currently as of July 1, 2015 the fee is \$4.35 per ERU. Once planning is concluded the City should complete a detailed rate study based on the capital needs identified during the planning process.

COST ESTIMATES

The cost estimates provided as part of the Fork Swamp Watershed Master Plan were prepared to assist City staff in making planning level decisions and prioritizing improvements. These cost estimates are not final design cost estimates. These costs were developed using recent bid tabulations from other communities and NCDOT projects within North Carolina. They include easement acquisitions, surveying, engineering, legal, and administrative costs. A detailed breakdown of the costs for the projects listed below in Table 9-1 is included in Appendix G. Projects are not listed based on priority. See Section 10 for a prioritization list. The cost estimates are approximate and are subject to change due to local costs, materials, delivery, construction, and other factors. BMP costs are based on the size of the BMP, the estimated excavation requires, and any associated structure of planting costs.

The stormwater drainage systems evaluated in this report are composed of a series of culverts, closed drainage systems, open channels, floodplain grading, and BMPs. For these drainage systems to function as designed, they must be properly maintained.

Table 9-1: Preliminary Project Cost Estimates

Projects	Preliminary Project Cost			
PRIMARY SYSTEM PROJECTS				
Railroad Floodplain Benching and Stream Stabilization (Fork Swamp)	\$1,000,000			
Evans Street Culvert Replacement and Floodplain Benching (Fork Swamp)	\$1,920,000			
East Fire Tower Road Floodplain Benching and Stream Stabilization (Fork Swamp)	\$1,740,000			
Fork Swamp Main Branch Floodplain Benching (Fork Swamp)	\$5,240,000			
Trafalgar Drive – South Floodplain Culvert (FSUT1)	\$180,000			
Trafalgar Drive – North Culvert Replacement (FSUT1)	\$440,000			
Corey Road Floodplain Culverts and Benching (FSUT1)	\$6,870,000			
Corey Road Regional Detention (FSUT1)	\$9,500,000			
County Home Road Floodplain Culverts and Benching (FSUT3)	\$210,000			
East Fire Tower Road – U/S Floodplain Culvert (FSUT3)	\$680,000			
Wimbledon Drive Culvert Replacement and Floodplain Benching (FSUT3)	\$610,000			
Tower Place Culvert Replacement (FSUT3)	\$640,000			
Summerhaven Drive Culvert Replacement and Floodplain Benching (FSUT3)	\$650,000			
East Fire Tower Road – D/S Floodplain Benching and Stream Stabilization (FSUT3)	\$4,000,000			
SECONDARY SYSTEM PROJECTS				
Corey Road	\$370,000			

Lynndale Closed System Phase I	\$1,010,000
Lynndale Closed System Phase II	\$3,420,000
Lynndale Closed System Phase III	\$2,750,000
STREAM STABILIZATION	ON PROJECTS
Project #1 – Live Oak Lane	\$280,000
Project #2 – Corey Road	\$590,000
Project #3 – East Fire Tower Road	\$230,000
Project #4 – Tower Place	\$140,000
Project #5 – Charles Boulevard	\$90,000
Project #6 – Queen Annes Road	\$220,000
Project #7 – Evans Street	\$130,000
WATER QUALITY F	PROJECTS
Project #1 – Cromwell Drive Bioretention	\$350,000
Project #2 – H. Boyd Lee Park Bioretention	\$340,000
Project #3 – H. Boyd Lee Park Permeable Pavement	\$970,000
Project #4 – Faith Assembly Church Pond Retrofit	\$270,000
Project #5 – County Home Road Regenerative	\$490,000
Stormwater Conveyance	
Project #6 – Irish Creek Regenerative Stormwater	¢250,000
Conveyance	\$250,000
Project #7 – The Oaks Regenerative Stormwater	\$200,000
Conveyance	φ200,000
Project #8 – South Hall Bioretention	\$240,000
Project #9 – Paramore Park Wetland	\$210,000
Project #10 – WGP Properties Regenerative Stormwater	\$60,000
Conveyance	ψου,ουο
Project #11 – Wintergreen Elementary Bioretention	\$310,000
Project #12 – Wintergreen Elementary Regenerative	\$180,000
Stormwater Conveyance	Ψ100,000
Project #13 – Wintergreen Elementary Rainwater	\$20,000
Harvesting	Ψ20,000
Project #14 – Belle Meade Apartments Wetland	\$570,000
Project #15 – Greenville Convention Center Permeable	\$2,870,000
Pavement	
Project #16 – Lynndale Court Bioretention	\$150,000
Project #17 – Westhaven South Wetland	\$820,000
Project #18 – Shamrock Regenerative Stormwater	\$130,000
Conveyance	

PRIORITIZATION AND RECOMMENDATIONS

As previously noted, the primary goal of this study is to make improvement recommendations to reduce flooding within the Fork Swamp Watershed. Currently, several conveyance systems do not meet the City hydraulic design requirements. WK Dickson has provided recommendations that help to reduce or eliminate the identified problems. Success criteria goals used to measure the proposed flood control project included the following:

- Providing improved level of service for roadways and structures;
- Economic feasibility;
- Minimizing stream and wetland impacts;
- Confirming physical feasibility using available GIS and survey data; and
- Minimizing easement acquisition.

Two different prioritization lists were developed for the proposed projects identified in Section 4 and 5; Flood Control Improvements and Water Quality/Stream Stabilization Improvements. Projects were prioritized using the Prioritization Matric provided in Appendix L. The improvements were prioritized based on the following factors:

- Public health and safety;
- Severity of street flooding;
- Cost effectiveness;
- Effects of improvements;
- Water quality BMP;
- Open channel –erosion control;
- Implementation constraints;
- Grant funding; and
- Constructability.

In some instances, project prioritization will be impacted by the required sequencing of projects to provide the highest possible flood reduction benefits and to reduce or negate any downstream impacts for the proposed projects. Downstream impacts are including in the scoring for Implementation Constraints, however upon completion of the scoring process, the prioritization list should be reviewed to ensure the projects are appropriately ranked based on sequencing. Table 10-1 shows the proposed prioritizations for the Flood Control Improvements. The City should re-visit the prioritization lists annually to determine if the priorities should change.

Table 10-1: Flood Control Prioritization – Primary System Projects

Prioritization	Project	
1	Railroad Crossing (Fork Swamp)	
2	Summerhaven Drive (FSUT3)	
3	Evans Street (Fork Swamp)	
4	Trafalgar Drive - South (FSUT1)	
5	County Home Road (FSUT3)	
6	Tower Place (FSUT3)	
7	East Fire Tower Road (Fork Swamp)	
8	Trafalgar Drive - North (FSUT1)	
9	Corey Road (FSUT1)	
10	Wimbledon Drive (FSUT3)	
11	Fork Swamp Main Branch Floodplain Benching	
12	East Fire Tower Road - Downstream (FSUT3)	
13	East Fire Tower Road - Upstream (FSUT3)	
N/A*	Corey Road Regional Detention (FSUT1)	

^{*}This project is located outside the City limits and does not impact the need or size for other capital projects. It is only proposed to avoid increases in flows at the City limits. However, improvements will benefit residents in the City limits.

Table 10-2: Flood Control Prioritization – Secondary System Projects

Prioritization	Project
1	Lynndale Closed System Phase I
2	Lynndale Closed System Phase II
3	Lynndale Closed System Phase III
4	Corey Road Closed System

Table 10-3: Stream Stabilization Prioritization

Prioritization	Project
1	Evans Street
2	Live Oak Lane
3	Tower Place
4	Charles Boulevard
5	East Fire Tower Road
6	Queen Annes Road
N/A*	Corey Road

^{*}This project is located in the ETJ therefore was not ranked. However, improvements will benefit residents in the City limits.

Table 10-4: Water Quality Prioritization

Prioritization	Project
1	WGP Properties Regenerative Stormwater Conveyance
2	H. Boyd Lee Park Bioretention
3	Wintergreen Elementary Rainwater Harvesting
4	Wintergreen Elementary Bioretention
5	South Hall Bioretention
6	Lynndale Court Bioretention
7	Shamrock Regenerative Stormwater Conveyance
8	Paramore Park Wetland
9	H. Boyd Lee Park Permeable Pavement
10	County Home Road Regenerative Stormwater Conveyance
11	The Oaks Regenerative Stormwater Conveyance
12	Wintergreen Elementary Regenerative Stormwater Conveyance
13	Cromwell Drive Bioretention
14	Belle Meade Apartments Wetland
15	Faith Assembly Church Pond Retrofit
16	Westhaven South Wetland
17	Irish Creek Regenerative Stormwater Conveyance
18	Greenville Convention Center Permeable Pavement

Table 10-5 shows the recommended priorities for maintenance projects in the watershed. Maintenance locations were identified based on the condition assessment completed during the stormwater inventory. Structures receiving a condition of "poor" or "repair" are listed below for maintenance. More immediate maintenance needs may present themselves if portions of a conveyance system fail. Projects were prioritized based on the consequences of flooding. Projects requiring structural improvements (i.e. in danger of failing) were given priority over those driven by sediment/vegetation removal needs. Additionally, the impact of flooding and proximity to a citizen input response were also considered in project ranking. Maintenance costs assume that City staff will complete the construction. If maintenance projects are bid to a private contractor, the City should complete a more detailed cost estimate prior to bid.

Table 10-5: Maintenance Recommendations

Prioritization	Project	Estimated Cost
1	Replace 72 LF of twin 60" CMP - squashed pipe end near 1750 Wimbledon Drive (FSUT030360 and FSUT030361)	\$64,800
2	Replace 162 LF of 15" CMP - rusted out bottom of pipe end near 400 Queen Annes Road (FSUT030769)	\$16,200
3	Replace 157 LF of 18" CMP - rusted bottom of pipe end near 113 Westhaven Road (FSMB030272) and replace 179 LF of 24" CMP - rusted bottom of pipe end near 107 Westhaven Road (FSMB030279)	\$40,800
4	Replace 154 LF of 18" CMP - rusted bottom of pipe end near 114 Woodstock Drive (FSMB030118) and Replace 194 LF of 15" CMP - rusted bottom of pipe end near 100 S Baywood Lane (FSMB030121)	\$26,600
5	Replace 208 LF of 15" CMP (sinkholes) near 3906 Southampton Court (CB FSUT020148)	\$20,800
6	Repair bent wing wall; replace eroded rip-rap at FES FSMB020543 near 3400 Evans Street; and replace 23 LF of 42" CMP - crushed pipe end near 101 Sara Lane (FSMB020547)	\$18,900
7	Replace box/repair 1' deep hole at bottom of drop inlet box at 3901 Clover Street (FSMB020182)	\$6,000
8	Replace 236 LF of 42" CMP - squashed pipe end near 608 Cedarhurst Road (FSMB030223)	\$70,800
9	Replace/repair minor damage and exposed rebar at pipe end near 3702 Evans Street (FSMB020200)	\$4,000
10	Repair broken hood/replace catch basin FSUT030560 near 3741 Charles Boulevard	\$6,000
11	Repair/replace FES near 508 Chesapeake Place separated from pipe, water is flowing underneath pipe end (FSUT030641)	\$4,000
12	Repair/replace FES separating from pipe near 3400 Baywood Lane (FSMB030001)	\$6,000
13	Repair/replace FES separating from pipe near 201 Bristol Drive (FSMB030063)	\$2,000
14	Replace 48 LF of 18" RCP eroding around pipe end at 2074 Old Fire Tower Road (FSUT030517)	\$5,300
15	Replace catch basin (sinkhole) near 3308 Landmark Street (FSMB030036)	\$6,000
16	Replace catch basin (sinkhole) near 2002 Tower Place(FSUT030325)	\$6,000
17	Replace catch basin (sinkhole) near 2085 E Fire Tower Road (FSUT030550)	\$6,000
18	Replace yard inlets (sinkhole) near 144 Blackwater Drive (FSUT020090) and near 327 West Meath Drive (FSUT020085)	\$12,000

Prioritization	Project	Estimated Cost
19	Replace yard inlet (sinkhole) near 3615 Memorial Drive (FSMB030176)	\$6,000
20	Replace yard inlet (sinkhole) near 403 Bremerton Drive (FSMB020481)	\$6,000
21	Replace catch basin near 209 Pin Oak Court (FSMB020135) sink holes around box	\$6,000
22	Replace 134 LF of 15" CMP - rusted bottom of pipe end near 110 Hearthside Drive (FSMB030269)	\$13,400
23	Replace 12 LF of 36" CMP - squashed pipe end near 301 Crestline Boulevard (FSMB030180) and Replace 19 LF of 36" CMP - squashed pipe end near 217 Crestline Boulevard (FSMB030186)	\$7,400
24	Replace yard inlet (sinkhole) near 120 Fire Tower Road (FSUT020442)	\$6,000
25	Replace yard inlets (sinkhole) near 1017 Van Gert Drive (FSMB010070 and FSMB010071)	\$12,000
26	Replace yard inlet (sinkhole) near 4222 Dunhagan Road (FSMB020276)	\$6,000
27	Replace pipe end, perched outfall recessed approximately 5' under bank near 1108 Holden Drive(FSUT030617)	\$4,000
28	Repair loose lid ring and cracked lid at junction box FSMB020506 near 604 Queen Annes Road	\$4,000
29	Repair loose lid ring at junction box FSMB020346 near 3505 Huntington Road	\$2,000
30	Repair/replace FES separating from pipe near 3104 Amhurst Lane (FSUT030573)	\$6,000
31	Replace yard inlet (sinkhole) near 4009 Lucerne Court (FSUT020327)	\$6,000
32	Replace catch basin FSMB020356 near 3514 Wallingford Road, bottom eroding away	\$6,000
33	Replace broken grate at catch basin FSMB010081 near 949 Van Gert Drive	\$6,000
34	Replace yard inlet (sinkhole) near 3614 Gosford Gate (FSMB020410)	\$6,000
35	Replace yard inlet (sinkhole) near 913 Chesapeake Place (FSMB020306)	\$6,000
36	Replace catch basin (sinkhole) near 127 Greenwood Drive (FSMB030163)	\$6,000
37	Replace yard inlet (sinkhole) near 4117 Bridge Court (FSUT030078)	\$6,000
38	Repair channel - major erosion of bank nearing road at pipe end near 161 Keys Court (FSMB020197)	\$15,000
39	Replace yard inlet near 1801 Arlington Boulevard (FSUT030531) major erosion around box	\$6,000

Prioritization	Project	Estimated Cost
40	Replace missing lid at junction box near 1604 Fire Tower Road (FSUT030466)	\$6,000
41	Replace missing grate at drop inlet FSUT030825, FSUT030826, FSUT030827, and FSUT030828 near 4112 Bridge Court	\$24,000
42	Replace fallen grate at yard inlet near 108 Loudon Court (FSMB030085)	\$3,000
43	Replace missing grate for pond structure FSMB020383 near 3870 Dunhagen Road	\$7,000
44	Replace broken grate at catch basin FSMB030164 near 1604 Stone Wood Drive	\$6,000
45	Replace missing lid at junction box near 1908 Exchange Drive (FSUT030434)	\$6,000
46	Maintain channel near pipe end at 4410 County Home Road - fully submerged (FSUT010081 and FSUT010082)	\$6,500
47	Maintain channel near pipe end at 1900 Rosemont Drive - fully submerged (FSUT030213)	\$6,500
48	Dredge pipe end outlet at 401 Fire Tower Road (FSMB020242)	\$2,000
49	Dredge buried pipe end at 301 Guiness Drive (FSUT020457)	\$2,000
50	Clear dense vegetation in channel, obstructing pipe end of FSUT020095 near 100 Poplar Branches Circle	\$1,000
51	Clear dense vegetation in channel, obstructing pipe end of FSUT020228 and FSUT020241 near 740 W Fire Tower Road	\$1,000
52	Remove tree growing on top of pipe end FSMB030139 near 301 Greenwood Drive	\$1,000
53	Repair water line dumping into catch basin near 3032 Rolston Road (FSUT030599)	\$10,000
54	Repair waterline conflict/obstruction at junction box near 107 Pinewood Road (FSMB020527)	\$10,000

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